

# High-power non-perturbative laser delivery diagnostics at the final focus of 100-TW-class laser pulses

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## Abstract

Controlling the delivery of multi-terawatt and petawatt laser pulses to final focus, both in position and angle, is critical to many laser applications such as optical guiding, laser-plasma acceleration, and laser-produced secondary radiation. We present an online, non-destructive laser diagnostic, capable of measuring the transverse position and pointing angle at focus. The diagnostic is based on a unique double-surface-coated wedged-mirror design for the final steering optic in the laser line, producing a witness beam highly correlated with the main beam. By propagating low-power kHz pulses to focus, we observed spectra of focus position and pointing angle fluctuation dominating frequency below 70 Hz. The setup was also used to characterize the excellent position and pointing angle correlation of the 1-Hz high-power laser pulses to this low-power kHz pulse train, opening a promising path to fast non-perturbative feedback concepts even on few-Hz-class high-power laser systems.

**Keywords:** high-power lasers, laser diagnostics, laser stabilization

## 1. Introduction

High-power laser systems, targeting science at relativistic laser intensities ( $> 10^{18}$  W/cm<sup>2</sup>), are now routinely employed at laboratories all over the world, ranging from peak powers of tens of TW (teraWatt) to multi-PW (petaWatt) and beyond<sup>[1–4]</sup>. Such high peak power is enabled by concentrating Joules of laser energy into femtosecond-duration pulses via Chirped Pulse Amplification<sup>[5]</sup>. When focused to  $\mu\text{m}$ -sized spots, the peak intensity reaches a regime where matter is easily ionized and the electrons quiver at relativistic speeds. Non-linear laser-plasma processes can then be accessed, driving applications such as laser-plasma acceleration (LPA, where plasma electrons are accelerated to GeV-level energies over distances of just centimeters<sup>[6]</sup>), LPA-based light sources<sup>[7–10]</sup>, plasma-based X-ray lasers<sup>[11]</sup>, and ion acceleration from solid targets<sup>[12]</sup>, among others.

The non-linear physics at play in the high-power laser-plasma interaction makes applications highly sensitive to laser alignment. For example, transverse position jitter at focus of order 10  $\mu\text{m}$  is problematic when short-scale plasma density features are present, when colliding or overlapping multiple  $\mu\text{m}$ -sized laser foci<sup>[13–16]</sup>, or when guiding intense laser pulses in plasmas<sup>[17,18]</sup>. Similarly, the pointing

angle of the laser axis affects the coupling of the laser-plasma-produced secondary radiation (electron beams, X-rays, etc) onto downstream beam and radiation optics such as quadrupole magnets. Hence control of position, pointing angle, and other laser parameters are key to high-quality laser applications.

Over recent years, LPA-relevant pioneering work has been performed on pointing-correcting<sup>[19]</sup> and wavefront-optimizing feedback loops<sup>[20]</sup>. Traditionally, high-power transverse focal position and angle are measured by monitoring the leakage of the last optic in the beam line<sup>[21]</sup>. However, since the leakage beam is transmitted through the mirror, vibrations and thermal motion of that specific mirror are not picked up by the leakage beam. Especially with long focal-length geometries, the vibrations on this last optic can translate into large position fluctuations at focus, uncorrelated to the leakage beam. In this manuscript past limitations are overcome by the installation of a specialty final steering mirror (the last optic delivering the converging laser beam from the parabola towards focus), where its back-surface reflection of the main beam is used to provide online non-perturbative monitoring of the high-power laser focus position and angle at a two-camera setup. We refer to the beam reflected from the back surface as the “witness beam”. This witness beam is a fully correlated copy of the

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high power beam since it shares exactly the same mirror reflections.

In addition, such a witness beam diagnostic also lends itself to integration of pointing stabilization based on feedback concepts. As part of this manuscript we will present data taken to quantify the system’s focal position and pointing angle fluctuations, by using both the low-power ( $\sim 1$  mJ at focus) high-repetition-rate (1 kHz) laser pulse train, as well as the low-repetition-rate (1 Hz) high-power ( $\sim 2.5$  J at focus) laser pulses. The low-power kHz pulse train is derived from the laser front-end. Since both pulse trains are originated from the same pulse train at upstream, with moderate thermal lensing of the amplifier crystals and kHz pulse having enough energy to be propagated, they have roughly the same beam size and the divergence through the whole system. This makes the low-power kHz pulse train well suited as the alignment beam. It carries same vibrations as the high power beam, from the source through the entire laser system, all the way to focus, which is not possible if the alignment beam is injected after amplifiers<sup>[19]</sup>. By propagating the low-power kHz pulses to focus, we observed focus position and pointing angle fluctuation dominated by frequency below 70 Hz (consistent with spectra of equipment vibrations, air turbulence, among other effects). This encouraging finding supports the vision that if high-power laser systems were to become available at kHz repetition rates (which is currently being pursued by various groups<sup>[22,23]</sup>), fast feedback mechanisms using the witness beam technique demonstrated in this paper could be able to correct for the  $<70$  Hz motion.

While awaiting such high-power kHz laser systems, we study the option of using the non-amplified kHz background pulse train to correct beam misalignments for the 1 Hz amplified high-power pulses. By simultaneously using two laser diagnostics (the witness beam diagnostic as well as a down-stream mode-imager diagnostic), we measured the position and pointing angle correlation between the 1 Hz amplified pulses and the 1 kHz non-amplified pulse train. One key question we aimed to answer is if the 1 Hz amplified pulses have a decreased correlation to temporally-adjacent kHz background pulses due to the 1 Hz amplification process (*i.e.*, does the pump laser and amplification process impart a temporary uncorrelated positional and angular kick to the 1 Hz amplified laser pulse?). If that were the case, it would critically limit the option for fast feedback at few-Hz laser systems by using the non-amplified background laser. However, it will be presented that full-power measurements confirmed that the amplification process did not add a measurable uncorrelated contribution to the 1 Hz amplified pulses.

The work presented here demonstrates a very accurate non-perturbative high-power laser diagnostic, allowing shot-tagged laser delivery information on position and angle. The demonstrated correlation of the high-power laser pulse

train to the non-amplified background pulse train highlights the option for feedback integration at bandwidths larger than the  $<70$  Hz environmental fluctuations. This would allow significant improvements in stability, quality, and applicability of high-power laser systems.

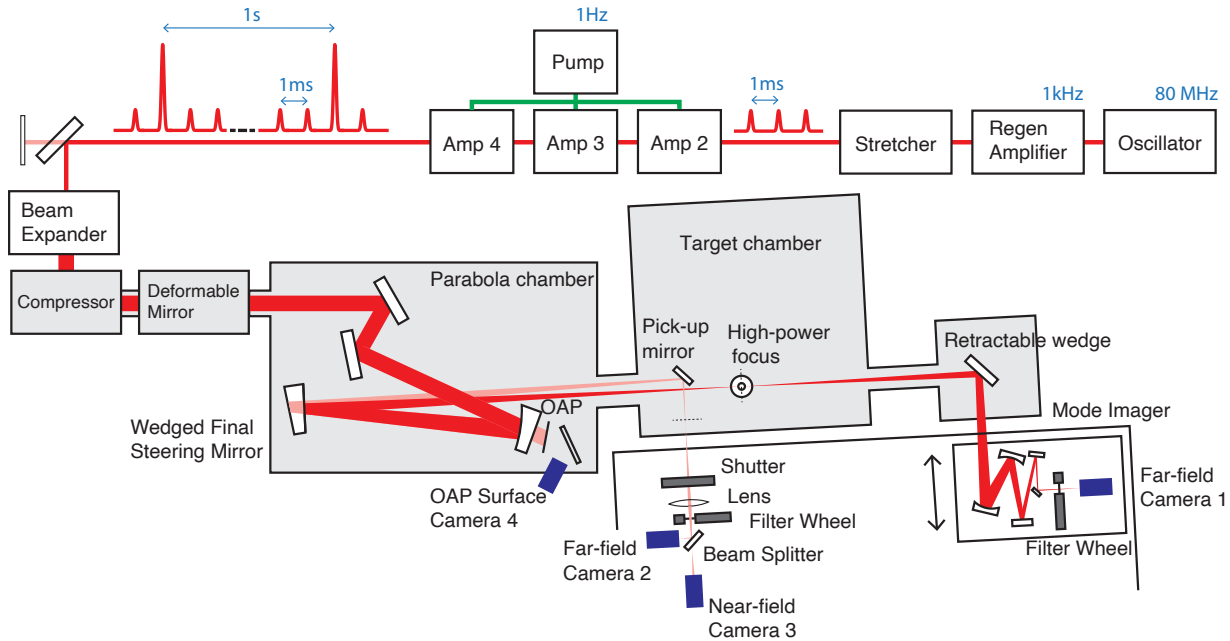
## 2. Experimental Setup

A schematic of the 100-TW-class laser system and online target chamber monitoring setup is shown in Fig. 1. The titanium-sapphire-based chirped-pulsed-amplification laser system was built to serve the LPA-based Free Electron Laser project at the BELLA Center<sup>[24]</sup>. It has the capability to approach 100 TW-class peak power based on  $\simeq 2.5$  J energy on target (3.8 J before the compressor) and 35 fs FWHM (full width at half maximum) pulse duration.

The commercial 1 kHz, 800 nm front-end laser is based on Vitara oscillator from Coherent<sup>[25]</sup> coupled with the Legend Elite regenerative amplifier. The laser pulses contain 3 mJ and are stretched from 25 fs to 290 ps at the stretcher to prevent damage to optics during amplification. The pulse train is then propagated to amplifier 2 (a 4-pass bow-tie amplifier), amplifier 3 (a 3-pass bow-tie amplifier), and to amplifier 4 (a 3-pass bow-tie amplifier). All three amplifier crystals are pumped by the same 16 J/shot 5 Hz pump laser (GAIA from Thales<sup>[26]</sup>, 532 nm,  $\sim 16$  ns pulse duration). The amplified pulse energy reaches 100 mJ after amplifier 2, 1 J after amplifier 3, and 4 J after amplifier 4, while its size increases from 6mm FWHM to 12 mm before amplifier 3, and to 23mm before amplifier 4. All titanium-sapphire crystals are water cooled.

While the repetition rate (as set by the pump lasers) can operate up to 5 Hz, in this manuscript we have operated the pump laser at 1 Hz repetition rate. In this mode the pulse train coming out of the amplifiers consists of amplified pulses separated in time by 1 second, and a train of unamplified background pulses separated by 1 ms. With the pump laser blocked, the remnant 1 kHz pulse train leaving the front-end system will be labeled as the “1 kHz non-amplified beam”. Following the three amplifiers, the laser pulses are spatially expanded from 23 to 81 mm FWHM using the reflective-curved-mirror telescope with magnification of 3.5. After being routed into the vacuum system, the pulses are compressed to 35 fs (FWHM) with a grating compressor, and focused into the target chamber using an off axis parabolic mirror (OAP) with focal length of 3 m. As shown in Fig. 1, one meter downstream of the OAP a final steering mirror directs the converging beam to final focus.

The laser mode on target is measured by inserting an uncoated retractable wedge downstream of focus (hence “destructive” to the path of electron beam propagating downstream), and routing the beam through a Mode Imager setup consisting of curved reflective mirrors and two more uncoated wedge reflections for appropriate attenuation onto



**Figure 1.** Experimental setup of the 100-TW-class laser system. A 1 kHz, 800 nm, 25 fs laser pulse train is produced in the regenerative amplifier (Regen), stretched to 300 ps, then every one in a thousand pulses is amplified in three successive multi-pass bow-tie amplifiers (Amp 2, 3, and 4). Single commercial pump laser (532 nm,  $\sim 16$  ns pulse duration) is routed to all three amplifier Ti:Sapphire crystals with 1 Hz repetition rate. The laser pulses are then compressed to 35 fs and focused into the target chamber, where a gas jet is placed for Laser Plasma Accelerator (LPA) experiments. The laser mode at focus is measured with two diagnostics: (1) a common Mode Imager (after insertion of the retractable wedge) with Camera 1 recording the far-field laser profile by imaging the target chamber focus plane, and (2) a correlated witness beam setup, where a back-surface-reflected final steering mirror is routing a correlated copy of the main beam to a setup measuring the laser's far-field (Camera 2, imaging the target chamber focus plane) and quasi-near-field (Camera 3, imaging a plane 44 mm downstream of the target chamber focus). The near-field beam profile at the off-axis parabolic mirror (OAP) surface is recorded by Camera 4. Grey boxes represent vacuum chambers.

far-field CCD Camera 1 (Basler acA1300-22gm, 1.3 MP resolution, pixel size  $6.9 \mu\text{m} \times 6.9 \mu\text{m}$ , pixel bit depth 12 bits). Camera 1 is thus imaging the plane of the focused beam in the target chamber at magnification  $\times 2.8$ .

Besides the Mode Imager setup, an alternative laser delivery monitor was developed. The copy of the high-power main beam was generated by the main beam reflecting at the rear surface of the final steering mirror, which is wedged at an angle of 0.25 degrees, has a 98% surface reflectivity on the front surface, and 80% reflectivity on the rear surface. Thus  $2\% \times 80\% \times 2\% = 0.032\%$  of the main beam was reflected from the rear surface of the wedge. This copy of the main beam will be labeled as “witness beam”. The transmission of this mirror was used for laser alignment and the measurement of its energy. At the front surface of the wedge, the reflected witness beam was separated from the main beam by 1.0 mm and 0.76 degrees. These parameters depend on the angle of incidence onto the wedge (4.4 degrees), the thickness (9.5 mm), and the material (fused silica). The witness beam  $B$ -integral, which is a measure of the nonlinear phase shift of light as it propagates through the final steering mirror was calculated to be 0.41 rad, which is low enough to keep unwanted effects such as self-phase modulation and self-focusing at acceptable levels (for a thicker optic and/or increased laser

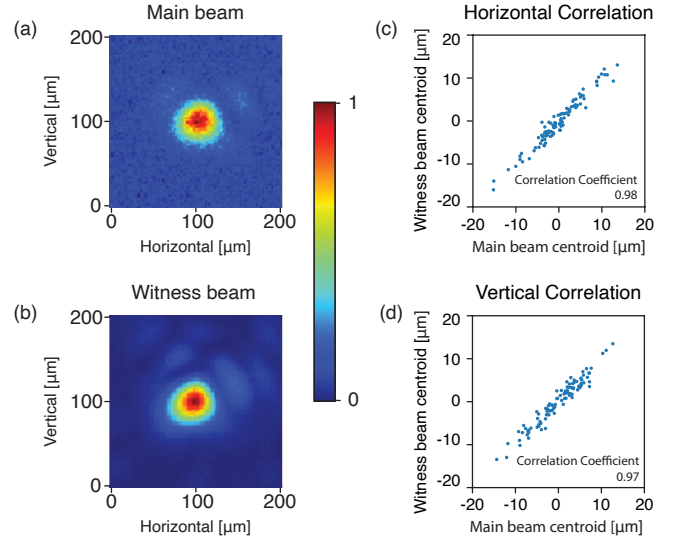
energy this effect should be re-evaluated). The aberrations introduced to the converging witness beam by the double-pass through the wedged mirror is expected to be minor due to the small wedge angle, its sub-cm thickness, and the near-normal angle of incident of the incoming laser. This assumption is supported by the fact that the main beam and the witness beam have similar beam sizes at focus, with no sign of significant aberrations, as shown in Figs. 2(a)-(b) and accompanied text in Sec. 3. The transverse position separation between the main beam and witness beam at the target chamber focal plane was 27 mm. The witness beam was reflected by a rigidly-mounted reflective mirror positioned 8 cm upstream of the witness beam focus. Thus the additional fluctuations of the witness beam picked up by this mirror is small compared to the last optic shared by the main beam and the witness beam. A vacuum window 11 cm after the witness beam focus transmitted the beam onto an achromatic lens and a beamsplitter. The reflected beam was captured by far-field Camera 2 (imaging the witness beam focus plane), while the transmitted beam was sent onto quasi-near-field Camera 3 (imaging a plane 44 mm downstream of the witness beam focal plane). CMOS Cameras 2 & 3 (Basler acA720-290gm, 0.4 MP resolution, pixel size  $3.75 \mu\text{m} \times 3.75 \mu\text{m}$ ) were operated in 1 kHz frame rate by reducing the ROI (region of interest) to 100

$\times 1000$  pixels. The magnification of this imaging system was  $\times 1.1$ . Pixel bit depth of all four cameras presented here were set to 12 bits. When recording images, the signal level was typically set to a factor of  $\times 1000$  above the noise, which was  $\sim 3$  counts. We typically threshold the image right above the background which varied between 20  $\sim$  200 counts depending on cameras and the laser power. It was verified that changing the threshold conditions above the background did not make a noticeable impact on the correlation studies presented in this manuscript. Since the witness beam setup can monitor both the position of the transverse focus (centroid on Camera 2) as well as the angle of the focal line (centroid difference between Cameras 2 and 3 divided by separation), this setup was capable of measuring the laser delivery non-destructively without interfering with the high-power laser focus and the LPA electron beam transport line. Filter wheels containing thin pellicle attenuators were installed in front of the Mode Imager and witness beam cameras. Both systems were mounted on an optical table isolated from the vacuum chambers for better stability.

### 3. Witness beam validation in high-power mode

To measure the correlation between the two diagnostics and to compare the main beam and the witness beam, synchronized far-field (focus) images on Camera 1 (Mode Imager) and Camera 2 (witness beam) were captured. Figure 2(a) shows a far-field mode of the main beam captured with Camera 1, while (b) shows a far-field mode of a witness beam captured with Camera 2. The beam size measured with Camera 1 was  $46 \mu\text{m}$  FWHM. The Mode Imager point spread function (PSF), arising from a limited collected angle, was measured by temporarily placing a single-mode fiber tip at the target chamber focal plane (mode size  $< 5 \mu\text{m}$ , see Fig. 1). This measured PSF indicates a resolution limit of  $25 \mu\text{m}$  FWHM, thus yielding a PSF-deconvolved target chamber focus beam size of  $\sqrt{46^2 - 25^2} = 39 \mu\text{m}$  FWHM. In the witness beam diagnostic (not constrained by a limited collection angle), the size of the witness beam measured with Camera 2 was  $40 \mu\text{m}$  FWHM, providing agreement with the Mode Imager setup.

Figures 2(c) and (d) show the centroid correlations of 100 consecutive shots (with each shot  $n$  yielding a centroid  $c_n$ ) of the amplified main and witness beams, in the horizontal and vertical planes, respectively. Note that each camera was calibrated to incorporate the transverse magnification at the imaged plane (the focal plane inside the target chamber). The standard deviation of 100 collected centroid measurements  $\sigma_c$  on the centroids on the Mode Imager is  $5.4 \mu\text{m}$  (rms) in horizontal direction and  $5.3 \mu\text{m}$  in vertical direction, corresponding approximately to an angle-of-incidence fluctuation of the beam onto the fixed point on the OAP of  $1.8 \mu\text{rad}$  in horizontal direction and  $1.9 \mu\text{rad}$  in vertical direction (not to be confused with the pointing angle fluctuations of the post-



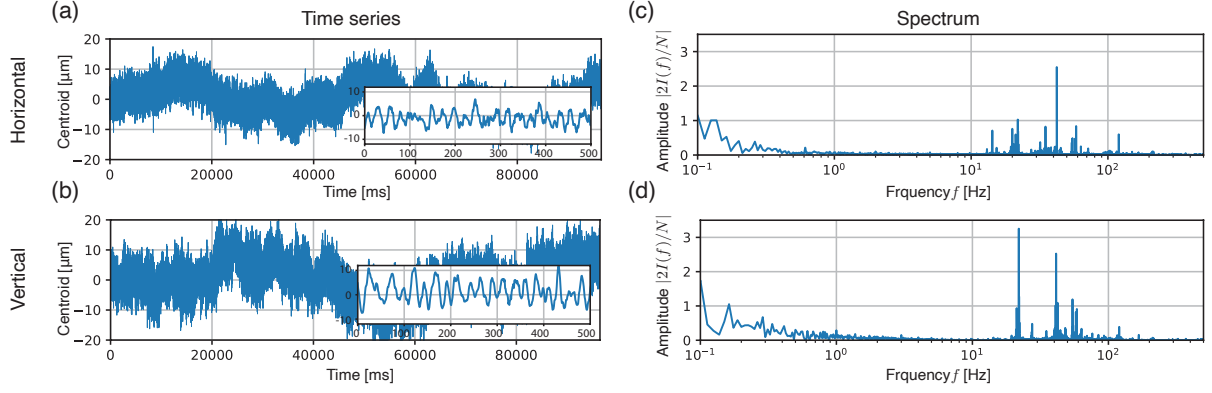
**Figure 2.** A single-shot transverse mode profile of the amplified beam captured by (a) Camera 1 (Mode Imager) and (b) Camera 2 (witness beam). (c-d) Correlation of 100 consecutive high-power shots (at 1 Hz) of the main beam and witness beam centroids in horizontal and vertical direction, respectively.

OAP target-line laser axis where the target position is fixed).

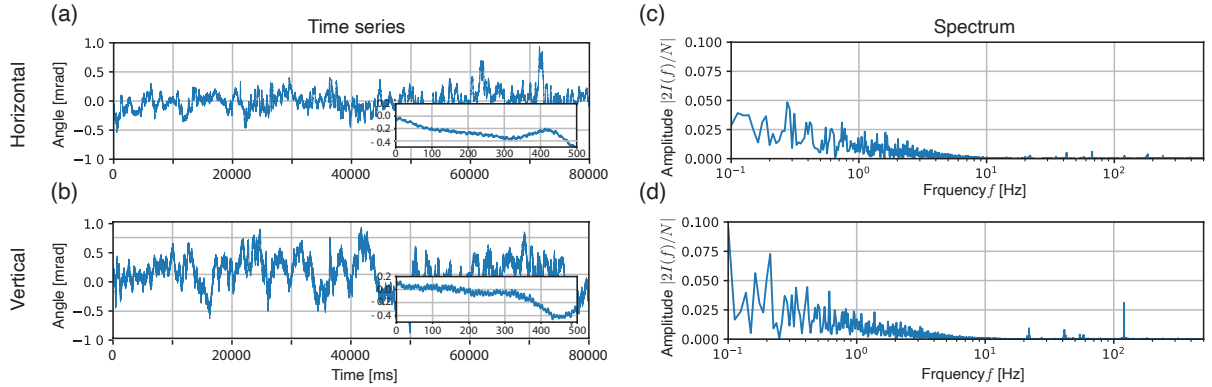
The witness-to-main beam Pearson's correlation coefficient (measuring the degree of correlation) for these 100 shots (100 seconds of 1 Hz acquisition), as shown in Figs. 2(c-d) was 0.98 and 0.97 in horizontal and vertical direction, respectively. Here, the Pearson's correlation coefficient is defined as

$$\rho = \frac{\text{cov}(c_{n1}, c_{n2})}{\sigma_{c1}\sigma_{c2}}, \quad (1)$$

with  $\text{cov}(c_{n1}, c_{n2})$  being the covariance of the two centroid measurements  $c_{n1}$  (Mode Imager Camera 1) and  $c_{n2}$  (witness Camera 2), and  $\sigma_{c1}$  and  $\sigma_{c2}$  their respective standard deviations. The standard deviation of the residual centroid fluctuations (uncorrelated)  $\sigma_{\text{res}}$  was found to be  $1.2 \mu\text{m}$  in horizontal direction and  $1.3 \mu\text{m}$  in vertical direction. Note that both main and witness beams share exactly the same mirror reflections all the way to the final steering mirror, limiting sources of uncorrelated factors. Camera 2 was imaging a plane 8 cm downstream of the reflecting mirror inside the target chamber, thus making it relatively insensitive to vibrations of this optic. Most residual fluctuation can be attributed to the fact that the Mode Imager has a series of post-focus reflective optics. We studied this post-focus by placing a rigidly-mounted single-mode fiber tip at the target chamber focus location, which was also used to measure the PSF. We found the centroid fluctuation  $\sigma_c$  to be  $0.84 \mu\text{m}$  in horizontal direction and  $1.2 \mu\text{m}$  in vertical direction, thus accounting for most of the witness-to-main beam residual fluctuation  $\sigma_{\text{res}}$ .



**Figure 3.** (a-b) Time series of 1 kHz non-amplified beam centroids in horizontal and vertical direction measured with far-field witness beam Camera 2. The inset displays a zoomed-in sub-set of the first 500 shots. (c-d) The amplitude  $|2I(f)/N|$  of the discrete Fourier transform  $I(f)$  of the time series (a) and (b), respectively, with  $N = 100000$  the number of samples. Besides sub-Hz drifts, several peaks in the fluctuation spectrum can be observed between 10 and 100 Hz.



**Figure 4.** (a-b) Time series of 1 kHz non-amplified beam pointing angle at focus in horizontal and vertical direction, derived from the far-field mode captured by Camera 2 and the near-field mode captured by Camera 3. (c-d) The amplitude  $|2I(f)/N|$  of the discrete Fourier transform  $I(f)$  of the time series (a) and (b), respectively, highlights the dominant components below 10 Hz.

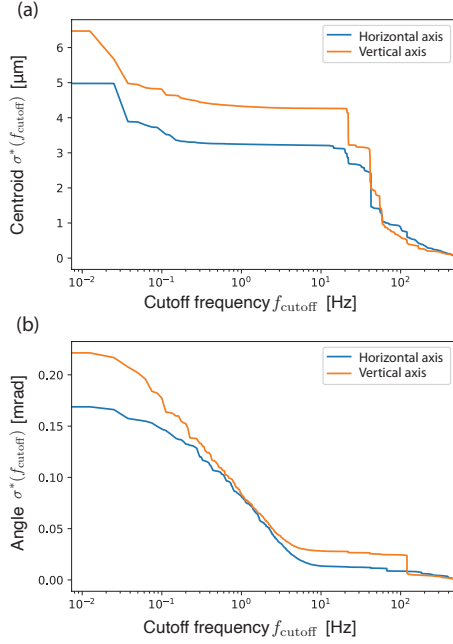
#### 4. Non-amplified kHz beam focus position and pointing angle fluctuations

To investigate the source of pointing fluctuations in the 1 Hz amplified beam, we blocked the pump laser to the main amplifiers, and studied the non-amplified kHz pulse train focus position and pointing angle fluctuations. The far-field mode of the witness beam was recorded on Camera 2 for 100 seconds at 1 kHz frame rate ( $N = 100000$  shots in total), with the centroids plotted in Figs. 3(a-b). The standard deviation was  $5.0 \mu\text{m}$  in horizontal direction and  $6.5 \mu\text{m}$  in vertical direction, which is similar to the high-power fluctuations in Fig. 2. This indicates amplifying the beam does not increase fluctuation. Hence within the resolution of our measurements, observed pointing fluctuations in the amplified 1 Hz beam can likely be corrected by steering mirrors based on fluctuations of non-amplified pulse train. Figures 3(c) and (d) show the intensity  $|2I(f)/N|$  of the discrete Fourier transform  $I(f)$  of centroids  $c_n$ , with is calculated together with the power spectral density  $S(f)$  following

$$S(f) = \frac{\Delta t^2}{T} |I(f)|^2 = \frac{\Delta t^2}{T} \left| \sum_{n=1}^N c_n e^{-2i\pi f n \Delta t} \right|^2, \quad (2)$$

with  $N$  total number of shots,  $\Delta t = 1$  ms the time between centroid acquisitions, and  $T = N\Delta t$  the total acquisition period. The bulk of the frequency components of the fluctuations are below 100 Hz, which we predict could be eliminated by an active control stabilization system using the 1 kHz non-amplified beam.

Similarly to Fig. 3, we recorded the optical axis angle  $\theta_n$  near final focus, by calculating the difference between the beam centroids as measured by Camera 2 and Camera 3, and by dividing it by the longitudinal separation in imaged planes. Figures 4(a) and (b) show the time series of the optical axis angle of the witness beam. The standard deviation was  $\sigma_\theta = 0.17$  mrad in horizontal direction and 0.22 mrad in vertical direction. Note that these values are significantly higher than the angle-of-incidence fluctuations



**Figure 5.** The standard deviation  $\sigma^*$  of (a) the centroid fluctuations and (b) the angle fluctuations, with only frequencies above  $f_{\text{cutoff}}$  included in the standard deviation calculation. This representation of the spectral content is a complementary way to interpreting the Fourier transforms of the time series in Fig. 3 and 4.

of the beams onto the OAP (position fluctuations on target translated into angle fluctuations assuming position on the OAP is fixed), and this difference is a direct result of the fact that optical axis of the focused laser beam is mainly dictated by position offset on the OAP surface (for example, a 0.3 mm position offset with no angle offset on the surface of the OAP with 3 m focal length results in a 0.1 mrad delivered pointing angle). It turns out there is high degree of correlation between the beam centroid on the OAP surface (Camera 4) and pointing angle determined from the witness beam diagnostic, which will be discussed in Sec. 6. Interestingly, compared to the time series of the beam centroids in Fig. 3, the pointing angle fluctuations in Fig. 4 are dominated by much lower frequencies, as is apparent in the zoomed-in insets of Figs. 4(a-b). The discrete Fourier transform of the time series of the pointing angle fluctuations, calculated by replacing  $c_n$  with  $\theta_n$  in Eq. (2), is shown in Figs. 4(c)-(d). One can observe that the frequencies below 10 Hz are dominating the fluctuations of the pointing angles.

Another method of interpreting the Fourier spectra of the centroid and pointing angle fluctuations is by computing the cutoff-integrated power spectral density<sup>[27]</sup>. The relation between the time-series standard deviation  $\sigma$  and the power spectral density  $S(f)$  is

$$\sigma = \sqrt{\int_0^{\infty} 2 S(f) df}. \quad (3)$$

Thus the standard deviation of the fluctuations  $\sigma^*$  for  $f$  less than  $f_{\text{cutoff}}$  (for example, because the lower frequencies were eliminated with an active feedback system), can be calculated as

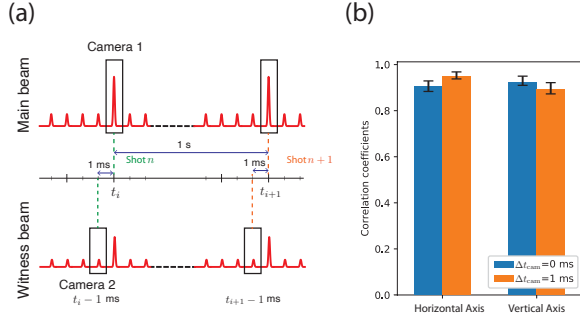
$$\sigma^*(f_{\text{cutoff}}) = \sqrt{\int_{f_{\text{cutoff}}}^{\infty} 2 S(f) df}. \quad (4)$$

Note that for  $f_{\text{cutoff}} = 0$ , we retrieve  $\sigma^*(0) = \sigma$ . Using Eq. (4), we calculated the cutoff-corrected standard deviation  $\sigma^*$  for the centroid and angular time-series of Figs. 3(a-b) and Figs. 4 (a-b). Figure 5(a) shows the centroid standard deviation  $\sigma^*$  as a function of cut-off frequency  $f_{\text{cutoff}}$ . The unfiltered standard deviation  $\sigma^*(0)$  in horizontal and vertical directions was  $5.0 \mu\text{m}$  and  $6.5 \mu\text{m}$ , respectively, but drops as  $f_{\text{cutoff}}$  is increased. As is evident, the standard deviation has strong contributions at  $<1$  Hz, around 20 Hz, 40 Hz, and 50-70 Hz. If frequency components below 70 Hz were filtered out ( $f_{\text{cutoff}} = 70$  Hz), the remaining standard deviation of the beam centroids would reduce to  $1.0 \mu\text{m}$  and  $0.81 \mu\text{m}$ , respectively, i.e.,  $\sim \times 5$ . In Fig. 5(b), addressing the focal axis pointing angle, the unfiltered standard deviation  $\sigma^*(0)$  in the horizontal and vertical direction was 0.17 mrad and 0.22 mrad, respectively. One can observe the dominant contributions to be below  $<10$  Hz. Choosing  $f_{\text{cutoff}} = 10$  Hz would reduce the standard deviation to 0.010 mrad and 0.026 mrad, respectively. Note that these are the hypothetical examples and in reality the measured fluctuations cannot become zero when all the oscillations are eliminated by the active feedback system. To measure the limit of the position and angle fluctuations of the witness beam, a rigidly-mounted single-mode fiber tip was placed at the witness beam focus location. Its position and angle fluctuations, which are the fluctuations of the diagnostics, were found to be  $0.56 \mu\text{m}$  in horizontal and  $0.67 \mu\text{m}$  in vertical direction, and 0.02 mrad in horizontal and 0.03 mrad in vertical direction respectively.

## 5. Main beam and witness beam centroid correlations

If the 1 Hz amplified beam were to receive a transient position and angle perturbation, for example during the sub-ms pumping process in the titanium-sapphire crystals, it would simply not be appropriate to use the non-amplified pulse train as an active feedback driver. In the previous sections we characterized the correlation of the amplified 1 Hz high-power pulse on the Mode Imager (the main beam) and the witness beam setup (witness beam), and we used the non-amplified 1 kHz pulse train to study the dominant spectral terms in the fluctuating position and angle at focus. Section 3 confirmed the witness beam as a correlated measurement of the main beam and Sec. 4 highlighted that most fluctuations are well below  $<70$  Hz. This opens a promising path to using the kHz pulse train for fast active





**Figure 6.** (a) Illustration of the main beam and the witness beam timing with respect to the camera capture exposure. The example shows the  $\Delta t_{\text{cam}} = 1$  ms case when Camera 1 (Mode Imager) captures the 1 Hz amplified main beam, while Camera 2 captures the non-amplified pulse 1 ms earlier. (b) Correlation coefficients  $\rho$  derived from the beam centroids measured with Camera 1 and Camera 2, both for  $\Delta t_{\text{cam}} = 0$  ms (blue bars) and  $\Delta t_{\text{cam}} = 1$  ms (orange bars). We observe no significant degradation in  $\rho$  at  $\Delta t_{\text{cam}} = 1$  ms, indicating that the main pulse has not picked-up a random centroid fluctuation during the amplification process.

feedback laser delivery stabilization. A further requirement is the correlation between the 1 Hz amplified pulse properties to the kHz pulse train.

To measure the correlation of the amplified beam to the non-amplified beam, we took advantage of the fact that the trigger timing for the witness beam cameras can be selected. For example, for a given acquisition of the main amplified beam on Camera 1, we triggered Cameras 2 and 3 to record the non-amplified pulse 1 ms earlier. Note that in order not to damage the witness beam cameras while recording the non-amplified pulse, all attenuators were removed and a mechanical shutter with sub-ms close time was used to block the 1 Hz amplified beam. A schematic of the camera capture timings is shown in Fig. 6(a). The Pearson's correlation coefficients  $\rho$  for  $N = 100$  consecutive shots are shown in Fig. 6(b), both in horizontal (left bars) and vertical direction (right bars). Two data sets are compared. The blue bars show  $\rho$  when both Camera 1 (Mode Imager) and Camera 2 (witness beam) are timed to record the main (high-power) pulse (there was no delay on the Camera 2 trigger, such that  $\Delta t_{\text{cam}} = 0$  ms). The orange bars show the case where  $\Delta t_{\text{cam}} = 1$  ms, referring to the situation where Camera 1 (Mode Imager) is recording the main (high-power) pulse, but Camera 2 is recording the non-amplified pulse 1ms earlier. The error bars show the standard error of the Pearson's correlation coefficient,  $\sqrt{(1 - \rho^2)/(N - 2)}$ <sup>[28]</sup>. Note that for this dataset, the laser mode was not optimized as for the centroid data in Fig. 2, which appears to manifest itself as a slightly reduced Pearson coefficient  $\rho$  (small fluctuations in the wings of the laser mode will affect the centroid calculation).

Noteworthy from Fig. 6(b) is the observation that there is no significant difference in the correlation coefficient  $\rho$  for (a)  $\Delta t_{\text{cam}} = 0$  ms and (b)  $\Delta t_{\text{cam}} = 1$  ms. This indicates that there is no significant random term in the transverse

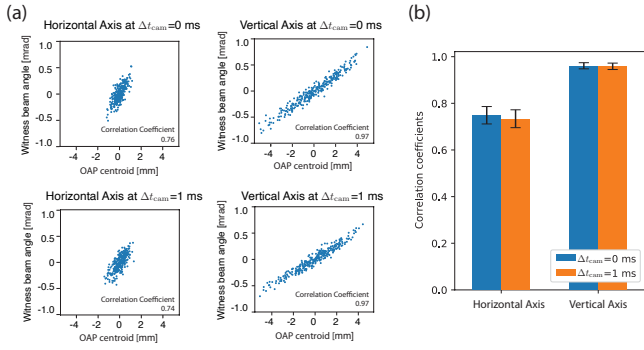
centroids as introduced by the amplification progress. This is a promising result when considering active feedback systems driven by the kHz non-amplified pulse train.

We also simulated how the Pearson coefficient  $\rho$  would drop if we added to the data a deliberate centroid fluctuation only on the main (high-power) pulse. If a fluctuation following a Gaussian statistical distribution with  $0.5 \mu\text{m}$  standard deviation was added to mimic added centroid fluctuations in the amplified beam, the correlation  $\rho$  at  $\Delta t_{\text{cam}} = 1$  ms was found to drop by 0.1 (from 0.9 to 0.8) in both horizontal and vertical directions. The value further drops to 0.6-0.7 when the standard deviation is increased to  $1.0 \mu\text{m}$ . Since our experimental results in Fig. 6(b) did not record a drop in  $\rho$  exceeding the  $\sim 0.05$  error bar, we can conclude that the additional focus position fluctuation during the amplification process is well below the error-bar-related upper bound of  $< 0.5 \mu\text{m}$ , which in turn is  $\sim 10\%$  of the fluctuation of the main beam.

## 6. Main beam and witness beam pointing angle correlations

When addressing pointing angle, unfortunately, unlike the Camera 2 and 3 witness diagnostic, the Mode Imager setup did not have the ability to measure the pointing angle of the main beam at focus. However, we can still use the beam centroid location at the OAP surface, as measured by CCD Camera 4 (Basler acA1300-22gm) in Fig. 1, to estimate the amplified laser pointing angle near focus. Indeed, as the top plots in Fig. 7(a) show, there is high degree of correlation between the beam centroid on the OAP surface (Camera 4) and pointing angle determined from the witness beam diagnostic. The Pearson correlation coefficient  $\rho$  is plotted as blue bars in Fig. 7(b), for the case of  $\Delta t_{\text{cam}} = 0$  ms (both diagnostics recording the high-power main pulse). The standard deviation of the witness beam angle at  $\Delta t_{\text{cam}} = 0$  was 0.16 mrad in horizontal direction and 0.30 mrad in transverse direction. The standard deviation of the centroid of the main beam at the OAP surface at  $\Delta t_{\text{cam}} = 0$  was 0.43 mm in horizontal direction and 2.0 mm in vertical direction. Offset of 0.43 mm in the OAP surface is equivalent to the angle offset of 0.14 mrad at focus assuming no angle offset on the surface of the OAP with 3 m focal length. Note that the difference of the slope of the correlation between the horizontal axis and the vertical axis in Fig. 7 is probably due to the existence of the non-symmetric high order near-field modes, and the investigation of this high-order content is beyond the coverage of this paper.

To study the potential impact of the transient amplification process, we also executed a scan where the witness beam angle diagnostic recorded the pointing angle of the non-amplified pulse 1 ms earlier (at  $\Delta t_{\text{cam}} = 1$  ms), with the scatter plots shown at the bottom in Fig. 7(a) and the correlation coefficient shown as orange bars in Fig. 7(b). Just like with the centroid scans in Fig. 6, there was no significant



**Figure 7.** (a) Correlations of the main beam centroid at the Off-Axis Parabola (OAP) surface as captured with Camera 4, and the pointing angle at focus captured with Cameras 2 and 3 (witness beam diagnostic). Camera 4 always captured the main (high-power) 1 Hz pulses, while Cameras 2 and 3 captured either the same pulse at  $\Delta t_{\text{cam}} = 0$  ms or the non-amplified pulse 1 ms earlier at  $\Delta t_{\text{cam}} = 1$  ms. (b) Correlation coefficients  $\rho$  for the plots in (a), showing that there are no significant differences in  $\rho$  between  $\Delta t_{\text{cam}} = 0$  ms and  $\Delta t_{\text{cam}} = 1$  ms, supporting the claim that the amplification process does not impart significant random fluctuations in target-chamber laser axis angle.

difference in Fig. 7 between the correlation coefficients at  $\Delta t_{\text{cam}} = 0$  ms and  $\Delta t_{\text{cam}} = 1$  ms. If a fluctuation following a Gaussian statistical distribution with 0.01 mrad standard deviation was added to mimic the angle fluctuations in the amplified beam, the correlation coefficient  $\rho$  drops below the standard error of the measured value. This suggests that pointing angle at focus is degraded by no more than  $< 0.01$  mrad of additional pointing angle fluctuation from the amplification process, i.e.,  $\sim 5\%$  of the main beam pointing angle fluctuation.

## 7. Conclusion

An online non-perturbative monitor of the high-power laser delivery was installed on a 1-Hz 100-TW-class laser system, measuring both the transverse focus position and the pointing angle at focus. The diagnostic was based on a unique double-surface-coated wedged-mirror used as a final steering mirror, generating a highly correlated witness beam. Correlation at high-power operation was verified with a Mode Imager far-field camera.

In addition to 1 Hz high-power pulses, the 1 kHz non-amplified pulse train was also sent to the witness beam cameras. The 1 kHz non-amplified witness beam is well suited as an alignment laser, since it propagates with the amplified beam from the oscillator all the way up to the last reflection at the final steering mirror, with its beam size and the divergence matched with the amplified beam. By performing a Fourier analysis on the centroid and pointing angle time series, the spectra of the position and the angle fluctuations were characterized. While the pointing angle fluctuations were dominated by  $< 10$  Hz environmental factors, the centroid fluctuations consisted both of low-frequency  $< 1$  Hz variations and various discrete contributions around 20,

40, and 50-70 Hz. By varying the camera trigger timing, it was verified that the amplified 1 Hz laser pulses did not accumulate random position and angle fluctuations during the amplification process by more than  $0.5 \mu\text{m}$  and  $0.01$  mrad respectively.

The various observations presented in this manuscript support the future concept that a  $< 70$ -Hz-bandwidth active feedback system, using the kHz non-amplified pulse train as sampling source, is sufficient to non-perturbatively stabilize the position and pointing angle of the 1-Hz-class high-power laser pulses by  $\sim \times 5$ . This would present a significant advance in the stability and tunability of high-power laser applications such as laser-plasma accelerators, among others.

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