

Optimization of energy storage properties in $(1-x)\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3-x\text{Sr}_{0.7}\text{La}_{0.2}\text{TiO}_3$ -relaxed ferroelectric ceramics

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Ferroelectric materials are considered to be the most competitive energy storage materials for applications in pulsed power electronics due to excellent charge–discharge properties. However, the low energy storage density is the primary problem limiting their practical application. In this study, $(1-x)\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3-x\text{Sr}_{0.7}\text{La}_{0.2}\text{TiO}_3$ [(1-x)NBT–xSLT] ferroelectric ceramics are found to exhibit excellent energy storage performances through a synergistic strategy. As the SLT concentration increases, the relaxation characteristic increases significantly and the breakdown strength increases dramatically from 150 kV/cm to 220 kV/cm. The recoverable energy storage density of the 0.55NBT–0.45SLT ceramic is 2.86 J/cm³ with an energy storage efficiency of 88% under an electric field of 220 kV/cm. Furthermore, the ceramic with $x = 0.45$ mol exhibited excellent energy storage stability in the ranges of 20–180°C (temperature) and 1–125 Hz (frequency). These excellent properties demonstrate the potential of (1-x) NBT–xSLT ceramics when used as dielectric capacitors in pulsed power systems.

Keywords: Energy storage; ferroelectric; lead-free ceramics; dielectric; microstructure.

1. Introduction

With the growing requirement for energy storage devices for pulsed power systems, ceramic-based dielectric materials are becoming a focus of interest due to their high power density and excellent stability.^{1–11} Basically, total energy storage (W_{tot}), recoverable energy storage (W_{rec}) and energy storage efficiency (η) of dielectric ceramic material can be assessed by the following equations^{11–13}:

$$W_{\text{tot}} = \int_0^{P_{\text{max}}} E dp, \quad (1)$$

$$W_{\text{rec}} = \int_{P_r}^{P_{\text{max}}} E dp, \quad (2)$$

$$\eta = \frac{W_{\text{rec}}}{W_{\text{tot}}} \times 100\%, \quad (3)$$

where E , P_{max} and P_r are the applied electric field, maximum polarization and remnant polarization, respectively.

Therefore, to obtain excellent energy storage performance, large P_{max} , low P_r and high breakdown strength (BDS) need to be satisfied.^{15–17}

Currently, four types of dielectric ceramics are widely used for energy storage applications, namely linear dielectrics (LDs), ferroelectrics (FEs), relaxed ferroelectrics (RFEs) and antiferroelectrics (AFE).^{18–21} Compared to LDs with low P_{max} and FEs with high P_r ,^{22,23} AFEs with double hysteresis loops and RFEs with slender polarization–electric field (P – E) hysteresis loops are considered to be promising materials for energy storage.^{15,24} However, RFEs are considered to be the most desirable ceramic dielectric capacitor material at present due to their environmental advantages. Due to the generation of random electric field (RFS), which disrupts the long-range ordered structure of the relaxation material, polar nanoregions (PNRs) are formed and thus excellent energy storage properties are achieved.²⁵

Among the relaxation ferroelectric ceramics, $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3$ (NBT)-based ceramic is considered to be the

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most competitive lead-free energy storage material by virtue of its excellent P_{\max} ($>40 \mu\text{C}/\text{cm}^2$). However, the small BDS and large P_r of pure NBT-based ceramic materials lead to low W_{rec} .¹⁵ Therefore, researchers have tried to improve the energy storage behavior of NBT-relaxed ferroelectric ceramics through component optimization.^{12,14,26} Qiao *et al.* introduced $\text{Sr}_{0.7}\text{Sm}_{0.2}\text{TiO}_3$ (SST) in NBT ceramics for replacing Bi^{3+} and Na^+ to avoid oxygen vacancies and to inhibit grain growth. The energy storage properties of $(1-x)\text{Bi}_{0.5}\text{Na}_{0.5}\text{TiO}_3-x\text{Sr}_{0.7}\text{Sm}_{0.2}\text{TiO}_3$ $[(1-x)\text{NBT}-x\text{SST}]$ RFE ceramics were increased via reducing the tolerance factor (t) to increase the relaxation ferroelectric phase and decreasing the grain size to exhibit large BDS of 283 kV/cm.²⁷ Lin *et al.* prepared $(1-x)(\text{Na}_{0.5}\text{Bi}_{0.5})_{0.7}\text{Sr}_{0.3}\text{TiO}_3-x\text{Bi}(\text{Mg}_{2/3}\text{Nb}_{1/3})\text{O}_3$ $[(1-x)\text{NBT}-x\text{BMN}]$ RFE ceramics. Sr^{2+} ions were introduced into the NBT ceramics to disrupt the long-range ordering of the ferroelectrics and attract PNRs generation, while BMN was introduced to suppress P_r .²³ This achieves a synergistic increase in energy storage density and η . The above studies demonstrate that combining fine grain and high densities is important for enhancing the BDS and relaxation behavior of NBT-based RFEs, thus further improving their performance in practical applications.^{18,28,29}

In this study, exceptional energy storage density and efficiency were achieved in $(1-x)\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3-x\text{Sr}_{0.7}\text{La}_{0.2}\text{TiO}_3$ $[(1-x)\text{NBT}-x\text{SLT}]$ ceramics. SLT has a significant effect on the reduction of the grain size, which leads to enhanced BDS and relaxation behavior. Moreover, $(1-x)\text{NBT}-x\text{SLT}$ ceramics are fabricated by tape-casting method, which improves the microstructure and densification of the ceramics. This preparation method effectively increases the BDS of the ceramics and contributes to the desired energy storage performance.^{30,31} Further, the results show that excellent energy storage properties are achieved at high electric fields. The potential of NBT-based ceramics when used as dielectric capacitors in pulsed power systems is confirmed by these excellent properties.

2. Experimental Details

The $(1-x)\text{NBT}-x\text{SLT}$ ($x = 0.2, 0.3, 0.4$ and 0.5) RFE ceramics were obtained via tape-casting technique and conventional solid-state sintering method. The weighed drugs were placed in ethanol and ball milled for 24 h to obtain the original powder. The virgin powder was dried and calcined at 850°C for 4 h. The calcined powder was subjected to secondary ball milling. Subsequently, ethanol, tributyl phosphate, polyvinyl butyral (PVB) binder and plasticizer (polyethylene glycol, phthalate) were added to the ceramic powder and then the mixture was ball milled for 18 h to obtain the cast slurry. Air bubbles were removed from the cast slurry by a vacuum defoamer (TP-08, Beijing Oriental Sun Technology Co., Ltd., China). The slurry was cast onto the film strip substrate by a cast machine (LY-150, Beijing Orient Suntech Co., Ltd., China). The obtained thick films

were stacked together (DY-30, Tianjin Technology Co., Ltd., China) and further densified green samples were obtained by cold isostatic pressing technique (U150, Shanxi Jinkaiyuan Co., Ltd.) under high pressure. The samples were calcined at 500°C to burn out the binder and then sintered in a crucible at 1170°C for 3 h. To avoid the volatilization of Na^+ and Bi^{3+} during high-temperature sintering, the samples were encapsulated in calcined powder of the same composition. Finally, the ceramic samples were polished to $100 \mu\text{m}$ and sputtered with an electrode area of 3.14 mm^2 , followed by electrical properties testing.

The phase structures of $(1-x)\text{NBT}-x\text{SLT}$ ceramics were analyzed by an X-ray diffractometer (Bruker D8 Advanced Diffractometer, Germany). The surface morphology of the ceramics was observed by scanning electron microscopy (FE-SEM; ZEISS Supra 55, Germany). Temperature dependence of the dielectric constant (ϵ_r) and dielectric loss ($\tan\delta$) was detected via a computer-controlled LCR meter (TH2828, Tonghui, China). The P - E hysteresis loops at the frequency of 10 Hz were measured by a ferroelectric test system (Radiant Technologies, Inc., Albuquerque, USA).

3. Results and Discussion

The room-temperature X-ray diffraction (XRD) patterns of the $(1-x)\text{NBT}-x\text{SLT}$ ceramics in Fig. 1(a) demonstrate that all ceramics exhibit a pure perovskite structure, and no second phase was observed. The enlarged view of the (200) diffraction peak is shown in Fig. 1(b). No splitting of the (200) diffraction peak was observed for all ceramics, which indicates that the ceramics have a typical pseudo-cubic structure. Additionally, the (200) peak shifts to the lower angle as the SLT content increases, which indicates the expansion of the lattice constant.^{18,31}

Figure 2 shows the SEM images and grain size distribution of $(1-x)\text{NBT}-x\text{SLT}$ ceramics. It can be observed that all ceramics have a dense structure and no obvious defects are produced. In addition, the average grain sizes of the different components of the ceramics are 2.54, 2.43 and $2.29 \mu\text{m}$,

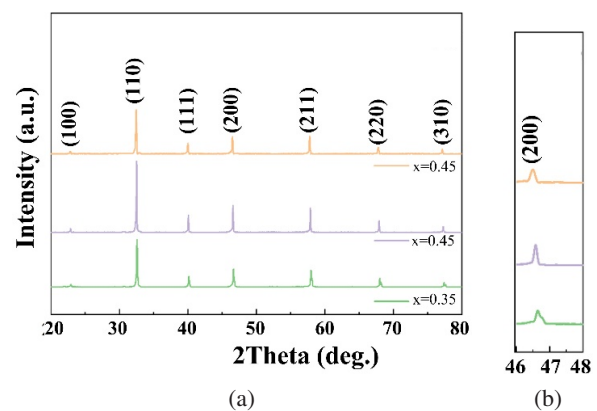


Fig. 1. (a) X-ray diffraction patterns of $(1-x)\text{NBT}-x\text{SLT}$ ceramics in the range of 20 – 80° . (b) The magnified spectra at (200) peak.

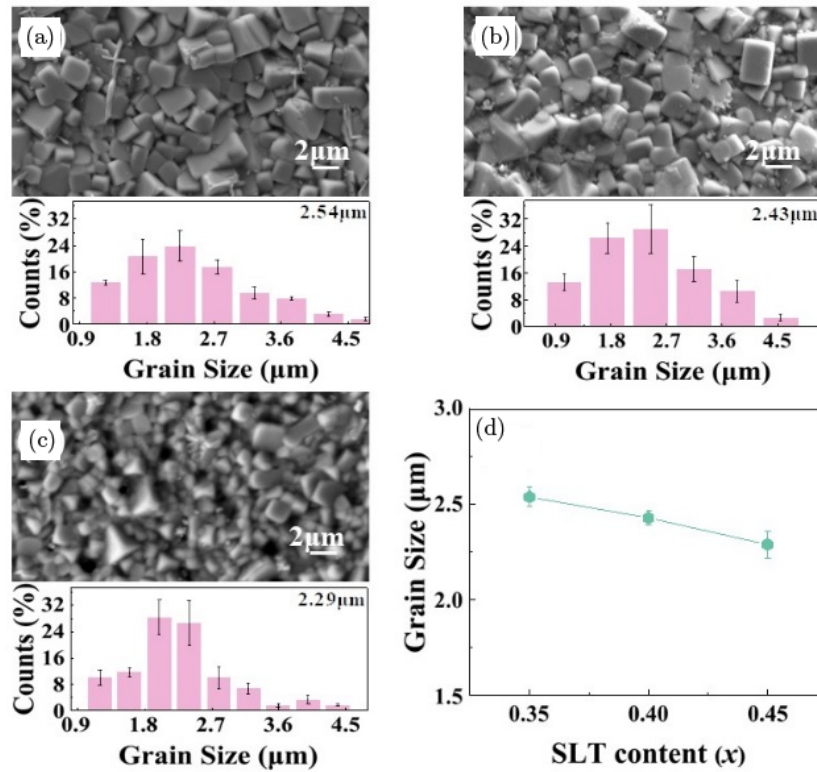


Fig. 2. (a)–(c) SEM images and grain size distribution of $(1-x)\text{NBT}-x\text{SLT}$ ceramics ($x = 0.35, 0.4$ and 0.45). (d) The average grain size of $(1-x)\text{NBT}-x\text{SLT}$ ceramics.

respectively, as can be seen in the grain size plot at the bottom of Fig. 2. This means that SLT doping can reduce the grain size of the ceramics and the defects, thus increasing the BDS.

As can be seen from Figs. 3(a)–3(c), the ε_r of all ceramics shows a tendency to increase and then decrease with increasing temperature, producing a peak in ε_r . This indicates that at this temperature, the ceramics changed from the ferroelectric phase to the paraelectric phase. As the SLT content increases, the ε_r of the ceramics gradually decreases. A reduced ε_r is beneficial to the increase in energy storage performance, which is due to the decrease in ε_r caused by increased relaxation. As the SLT content increases, local lattice deformation and disruption of ferroelectric long-range ordering produce RFS. RFS leads to a gradual increase in dynamic PNRs and hence enhanced relaxation behavior.^{3,32,33} The ε_r and $\tan\delta$ gradually move toward higher temperatures as the test frequency increases, producing frequency dispersion, which is a manifestation of ceramic relaxation properties.^{33,34} Figure 3(d) shows the frequency dependence of the $(1-x)\text{NBT}-x\text{SLT}$ ceramics. As the SLT content increases, ε_r gradually decreases. This is also an indication of progressive strengthening of the relaxation properties of the ceramics due to the increasing SLT content. The overall decrease in ε_r with increasing frequency implies that frequency affects the stability of the ceramics. Of the three components, the 0.45SLT component has the best overall stability.

The Weibull distribution of the ceramic dielectric BDS is shown in Fig. 4(a). The Weibull distribution can be calculated by the equation³⁵

$$X_i = \ln(E_i), \quad (4)$$

where E_i represent the values of specimens of test ceramics. The results for the Weibull distribution of $(1-x)\text{NBT}-x\text{SLT}$ ceramics are shown in Fig. 4(a). The graph shows a good fit of the data points, and all shape parameters (β) are higher than 50 for each composition. Good agreement with the Weibull distribution was found for all test ceramics in the decomposition data. It can be seen that the BDS of the ceramics increases gradually with the increase of SLT content, which is due to the reduction of grain size, which makes the ceramics dense, and these factors make the BDS to have a great improvement.³⁶ Figure 4(b) shows the $P-E$ loops of the ceramics at the same NBT/SLT ratio. With the increase of SLT, P_{\max} decreases, and the ceramics retain the slender shape in general, which is one of the manifestations of the relaxation property. As shown in Fig. 4(c), W_{rec} of $(1-x)\text{NBT}-x\text{SLT}$ ceramics increases significantly from 1.81 J/cm^3 to 2.52 J/cm^3 when the SLT content increases from 0.35 to 0.45. In particular, the 0.55NBT–0.45SLT ceramic has the highest W_{tot} (2.83 J/cm^3) and W_{rec} (2.52 J/cm^3), and maintained a high η (88%). To further elucidate the energy storage performance of the 0.55NBT–0.45SLT ceramic, the $P-E$ loops under the

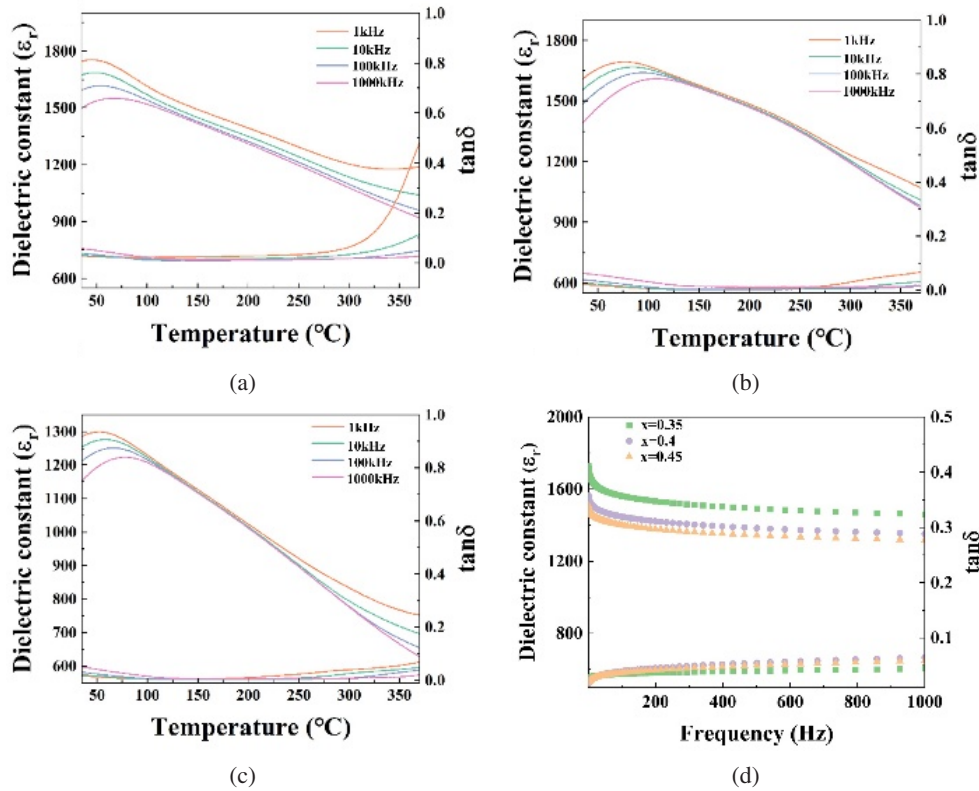


Fig. 3. Dielectric constants and dielectric losses of $(1-x)\text{NBT}-x\text{SLT}$ ceramics ($x = 0.35, 0.4$ and 0.45): (a)–(c) temperature dependence and (d) frequency dependence.

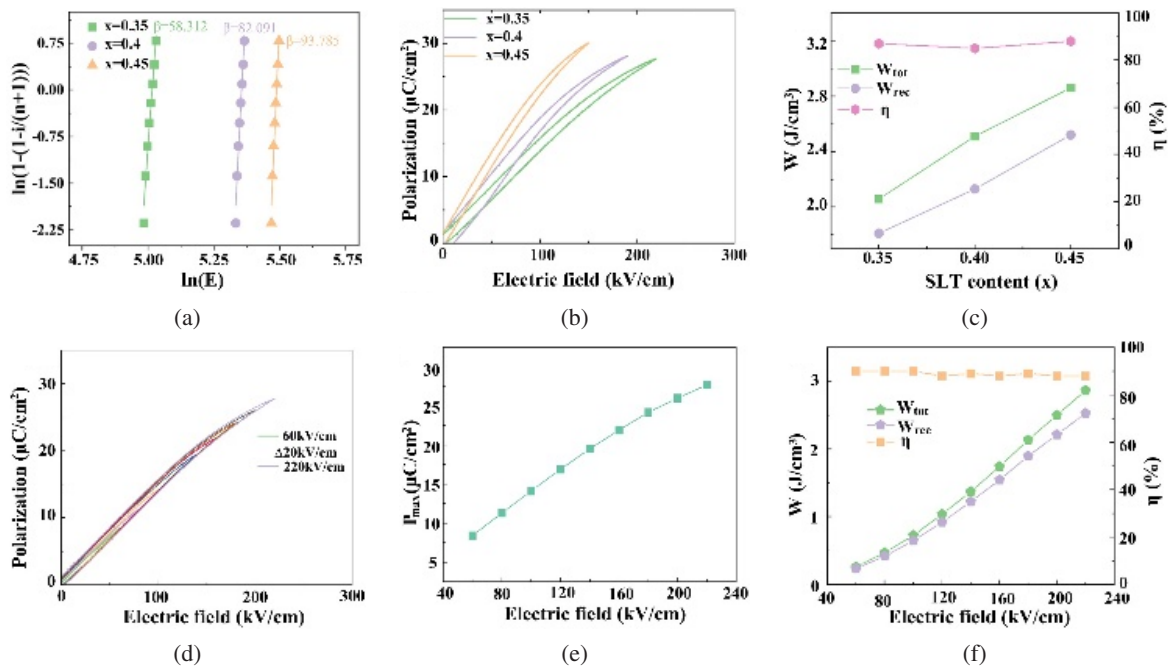


Fig. 4. (a) Weibull distribution function of BDS; (b) P - E loops of $(1-x)\text{NBT}-x\text{SLT}$ ceramics ($x=0.35, 0.4$ and 0.45); (c) W_{tot} , W_{rec} and η variations with respect to x content; (d) P - E loops of $0.55\text{NBT}-0.45\text{SLT}$ ceramic under varying electric field; (e) P_{max} of $0.55\text{NBT}-0.45\text{SLT}$ ceramic under different applied electric fields; and (f) W_{tot} , W_{rec} and η as a function of electric field for $0.55\text{NBT}-0.45\text{SLT}$ ceramic.

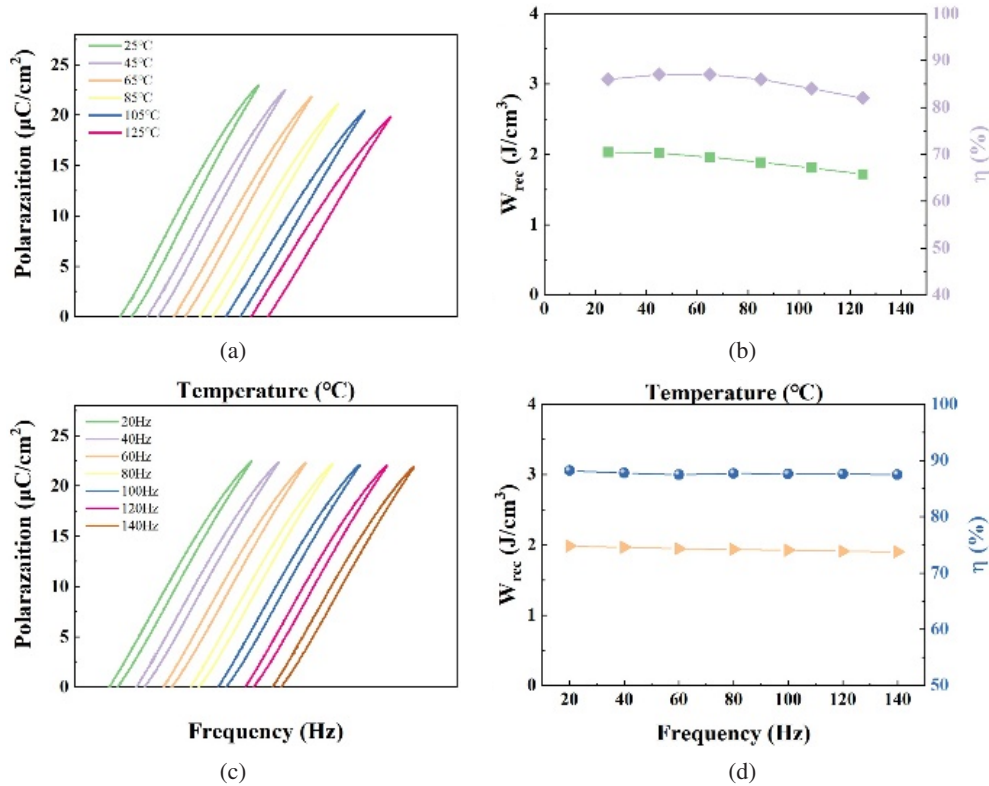


Fig. 5. The 0.55NBT–0.45SLT ceramic results corresponding to the temperature stability and frequency stability under the test conditions.

varying electric field at room temperature (RT) are shown in Figs. 4(d) and 4(e). Both the polarization and energy storage of the ceramics increase gradually with the increase of electric field. The performance of the ceramic is stable under the electric field without polarization or with the sudden change of electric field, which indicates that the ceramic has good stability under low electric field. The rate of increase of P_{max} decreases as the electric field increases from 60 kV/cm to 220 kV/cm. This indicates that as the test electric field increases and gradually approaches the BDS of the ceramic, the polarization of the ceramic also gradually approaches the optimal saturation state. The enhanced P_{max} and BDS are favorable to achieve large W_{rec} in 0.55NBT – 0.45SLT ceramic. The W_{tot} , W_{rec} and η of 0.55NBT – 0.45SLT ceramic under different applied electric fields are shown in Fig. 4(f), respectively. It can be observed that W_{tot} and W_{rec} increase from 0.28 J/cm^3 and 0.25 J/cm^3 to 2.86 J/cm^3 and 2.52 J/cm^3 , respectively. η decreases slightly from 90% to 88% with increasing BDS due to enhanced conductivity.

Figure 5 shows the P – E curves and energy storage performances of the 0.55NBT–0.45SLT ceramic at different test temperatures and frequencies. The W_{rec} of the ceramic decreases from 2.03 J/cm^3 to 1.72 J/cm^3 in the temperature range of 25–125 $^{\circ}\text{C}$ under 200-kV/cm electric field and there is a recoverable energy storage density from 1.98 J/cm^3 to 1.90 J/cm^3 in the frequency range of 20–140 Hz.

The slight but insignificant decrease in efficiency in both ranges also shows the high stability of the ceramic.

4. Conclusions

In a nutshell, $(1 - x)\text{NBT} - x\text{SLT}$ lead-free ceramics were prepared by the flow-delay method and the energy storage properties were investigated. A pure perovskite structure and a dense structure were exhibited by the $(1 - x)\text{NBT} - x\text{SLT}$ ceramics. A key role in the reduction of grain size and domain size can be attributed to SLT, which leads to enhanced BDS and relaxation properties. A maximum W_{rec} of 2.86 J/cm^3 and a high η of 88% are obtained for the 0.55NBT – 0.45SLT ceramic. Besides, the 0.55NBT – 0.45SLT ceramic exhibited good temperature and frequency stability. These excellent properties demonstrate the promising potential of the studied dielectric capacitor ceramics for the development of pulsed power systems.

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