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Piezoelectric, ferroelectric and pyroelectric properties of (100−*x***)Pb(Mg1/3Nb2/3)O3−***x***PbTiO3 ceramics**

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A series of $(100-x)Pb(Mg_{1/3}Nb_{2/3}O_3-xDbTiO_3$ (PMN−*xPT*, $x = 24, 25, 26$) ceramics were prepared by solid-state reaction technique using $MgNb₂O₆$ precursor. The results of the detailed characterizations reveal that the content of PT has negligible influence on the grain size, and all samples possess the perovskite structure. As the PT content increases, the samples changed from the normal ferroelectric phase to the ergodic relaxor state at room temperature. As a result, PMN–*x*PT ceramics are endowed with electro-strain of 0.08% at a relatively low electric field of 2 kV/mm, and effective piezoelectric coefficient of 320 pm/V was obtained. Simultaneously, the PMN–*x*PT ceramics have exceptional pyroelectric performance, exhibiting a high pyroelectric coefficient *p*~5.5 – 6.3 × 10−8 C·cm−2·K−1. This study demonstrates the great potential of PMN–*x*PT for piezoelectric and pyroelectric device applications.

Keywords: Perovskite; PMN–PT; electro-strain; ferroelectric phase.

1. Introduction

Lead-based relaxor ferroelectric materials are generally binary or ternary solid solutions of $PbTiO₃$, represented by $PbZrO_3-PbTiO_3$ (PZT), $Pb(In_{1/2}Nb_{1/2})O_3-Pb(Mg_{1/3}Nb_{2/3})$ $-PbTiO_3$ (PIN–PMN–PT) and $Pb(Mg_{1/3}Nb_{2/3})O_3-PbTiO_3$ (PMN–PT).¹⁻³ They have typical ABO₃ perovskite structure, and the general formula of their composite perovskite structure is A (B'B") O_3 or A'A"(B'B") O_3 , which is characterized by more than one ion at the same lattice position. Their excellent ferroelectricity, high dielectric properties, strong piezoelectric performance and good pyroelectric, photoelectric properties render them widely used in ferroelectric memory, actuators, sensors, dielectric resonators and transducers.⁴⁻⁷ $(100-x)Pb(Mg_{1/3}Nb_{2/3})O_3-xPbTiO_3$, (where *x* varies from 0 to 100), where the A-site ion is Pb^{2+} , the B-site ions are composite ions (B' is Mg^{2+} and B" is Nb⁵⁺).^{8,9} It displays a broader dielectric dispersion around Curie temperature (T_C) , a higher dielectric constant, and a relatively small dielectric temperature coefficient. Therefore, this material can be widely used in consumer electronic products, pulse power applications and energy harvesting systems.10–12

For the binary solid solution systems with different PT contents in PMN–PT, due to different phase structure, the

corresponding structures and properties are also different. On both sides of the MPB phase boundary component, one side with low PT content shows strong dielectric relaxation characteristics, while the other side shows typical ferroelectric characteristics.13–15 However, PMN–PT binary system also undergoes different types of phase transition, which depends on the value of *x*, and its crystal structure will change significantly with temperature. At low temperature (below Curie temperature), when the PT content is less than 27, PMN–PT system shows a rhombohedral structure (R), and when the PT concentration was higher $(x > 34)$, it showed a tetragonal structure (T). Therefore, in the MPB component region (27 $\langle x \rangle$ 34), PMN–PT system is the coexistence of rhombohedral and tetragonal phases. Above the Curie temperature, no matter what the PT content is, the crystal structure of the PMN–PT system is a cubic phase without the piezoelectric effect.16–18

It is well known that PMN–PT has excellent piezoelectric properties in rhombohedral phase region, tetragonal phase region and MPB region. Especially, PMN–PT ceramics near MPB have very high piezoelectric coefficient, extremely high electro-strain and excellent electromechanical coupling factors, which are far greater than those of PZT-based

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ceramics. PMN–PT ceramics can be used to fabricate high sensitivity ultrasonic transducers, large displacement actuators and sensors. PMN–PT ceramics have good application prospects in ultrasonic imaging and sonar positioning systems.^{19–21} Therefore, in this work, $(100-x)$ PMN–*x*PT (*x* = 24, 25, 26, these component are close to MPB) was selected and prepared by solid-state reaction. $MgNb₂O₆$ precursor route was used for synthesis to reduce the possible formation of pyrochlore phase. The dielectric, piezoelectric, ferroelectric and pyroelectric properties of (100−*x*)PMN–*x*PT ceramics were systematically studied.

2. Experimental Procedure

The $(100-x)PbMg_{1/3}Nb_{2/3}O_3-xPbTiO_3$ (designated as PMN–*x*PT, with $x = 24$, 25, and 26) ceramics were prepared using the traditional solid-state reaction method. The Pb_3O_4 (99.95%), $C_4H_6MgO_4.4H_2O$ (99%), Nb_2O_5 (99.9%), TiO₂ (99%) were used as raw materials. All the raw materials are purchased from Aladdin reagent. First, $C_4H_6MgO_4.4H_2O$ and $Nb₂O₅$ were weighed according to the chemical reaction of Eq. (1). The powder mixtures were ball-milled for 24 h, then dried and heated to 1000°C at a rate of 5°C/min, and held for 6 h. The MgNb₂O₆ precursor was obtained. Second, according to the stoichiometric ratio, the synthesized $MgNb₂O₆$ was mixed with Pb_3O_4 and TiO₂, and ball-milled for using alcohol as solvent for 24 h. 10 mol.% Pb_3O_4 and 5 mol.% $C_4H_6MgO_4 \cdot 4H_2O$ was additionally added to compensate for the possible volatilization of Pb and Mg element during heat treatment. The mixed power was dried, and then calcined at 800°C for 2 h, Afterwards, the calcined powder went through a second ball milling for 24 h. Then, the resultant powder was mixed with 7% concentration of polyvinyl alcohol (PVA). The powder was pressed into green pellets with a diameter of 10 mm and a thickness of 1.5 mm by isostatic pressing. Finally, these samples were sintered at 1220°C for 2 h.

$$
C_4H_6MgO_4.4H_2O + Nb_2O_5 + 4O_2 \rightarrow MgNb_2O_6 + 7H_2O + 4CO_2.
$$
 (1)

The crystal structure of the PMN–*x*PT was analyzed by X-ray diffractometer (XRD; D8 ADVANCE, Bruker, Germany) using Cu K α radiation ($\lambda = 0.15418$ nm) at a scanning speed of 0.2°/s, a step size of 0.02° and a scanning range of 20°– 80°. The morphology and grain size of the ceramics were characterized by field emission scanning electron microscope (FESEM; SU8220, Hitachi, Japan). The density of the sample was measured by water immersion technique using Archimedes' principle. The instrument used to collect the dielectric property data was Agilent E4981A capacitance meter, which was tested at 1 kHz. The instrument used to obtain the dielectric temperature spectrum data was TH 2816 A digital bridge. The piezoelectric constant d_{33} of the sample was measured with a quasi-static d_{33} measuring instrument (JZ-3AN, Institute of Acoustics Academic, China). The polarization hysteresis loops (*P*–*E*), strain-electric field (*S*–*E*), d_{33} -electric field (d_{33} –*E*) and ε _{*r*}-electric field (ε _{*r*}–*E*) curves of the ceramics were measured using a ferroelectric analyzer TF-1000 (Aixacct, Germany).

3. Result and Discussion

Figure 1 shows the XRD patterns of as-received PMN–*x*PT ceramics with different PT contents. The diffraction profiles reveal that PMN-25PT has a single perovskite structure, but

Fig. 1. XRD patterns of PMN–*x*PT ceramics sintered at 1220°C for 2 h: (a) 20°–80° and (b) 65°–75°.

Fig. 2. SEM micrographs of PMN–*x*PT ceramics sintered at 1220°C for 2 h: (a) PMN–24PT, (b) PMN–25PT and (c) PMN–26PT.

a trace amount of pyrochlore phase (marked as *) is present in PMN-24PT and PMN-26PT. It suggests that for the case of PMN-25PT, the PT can form a complete solid solution with the PMN matrix. In order to analyze the process of structural change further in detail, three characteristic reflection peaks, ${220}$, ${221}$ and ${301}$ in the range from 65° to 75° are chosen, as shown in Fig. 1(b). With increasing PT concentration, they are split into {220}, {221} and {301} peaks for all the ceramics, which suggests that rhombohedral and tetragonal phases coexist in all these components. In addition, {202}, {212} and {103} peaks shift towards lower angle, implying the expansion of lattice due to the incorporation of PT. Therefore, the addition of PT changes the phase structure, which would have an impact on the piezoelectric, dielectric and pyroelectric properties of materials.

In order to analyze the morphology of the PMN–*x*PT ceramics, field emission scanning electron microscopy (FESEM) was used. Figure 2 presents the microstructure of PMN–*x*PT ceramics. All of the samples have dense microstructure with well-defined grains and very small amount of pores with a high relative density (>95%). However, compared with other samples, PMN-25PT has good grain development, full crystal shape and clear grain boundary contour (the average grain size of 5.53 *μ*m), indicating that PMN-25PT ceramic has the highest crystallization degree. With the increase of PT content, it is found that the average grain size increases, the grain distribution gets uniform and the grain gradually becomes round. According to the existing research results,22–25 the grain size will affect the piezoelectric and dielectric properties of ceramics. Under a certain grain size, it increases with the increase of grain size. If it exceeds this critical value, it will decrease with the increase of grain size.

Figures 3(a)–3(c) show the temperature-dependent dielectric permittivity and loss tangent of PMN–*x*PT ceramics measured from 30°C to 140°C at 1 kHz, 10 kHz and 100 kHz, respectively. All the samples display obvious frequency dispersion, suggesting the nature of the relaxor state. However, two anomalies are observed in the dielectric permittivity curves. The one at the lower temperature region $({\sim}80^{\circ}C)$ could be attributed to the process of thermal evolution of

Fig. 3. Temperature dependence of dielectric permittivity and tangent loss at different measuring frequencies for (a) PMN–24PT, (b) PMN–25PT and (c) PMN–26PT.

discrete tetragonal polar nanoregions (PNRs).²⁶ The other one at the higher temperature region (~110°C) can be designated as T_m with the maximum value of the dielectric permittivity, corresponding to the PNRs relaxation emerged from rhombohedral PNRs.^{27,28} As the frequency decreases, T_m moves to lower temperature, indicating that all samples are relaxor ferroelectrics. Moreover, with the increase of PT content, *ε^r* of the sample first decreases and then increases, and tan*δ* also shows the same trend. The overall dielectric frequency dispersion decreases and T_m increases linearly.

Figure 4(a) displays the polarization hysteresis loops (*P*-*E*) for PMN–*x*PT measured under 2 kV/mm. It is observed that the remnant polarization P_r of the ceramics decreases with the increase of PT content. On the one hand, this can be attributed to the change of crystal structure. Through the above analysis of permittivity results, it can be seen that with the increase of PT content, the relaxation characteristics increase, which will seriously damage the long-range order of the original oxygen octahedron, thereby reducing the stability of the ferroelectric unit and damaging the inherent ferroelectricity.²⁹ On the other hand, the introduction of PT destroys long-range ordered ferroelectric domains and weakens the stability of coupling between charged defective dipoles and domains. Figure 4(b) presents the electric field-induced strains at room temperature for PMN–*x*PT ceramics. With the increase of PT content, the strain increases, while the overall strain remains a relatively high value (>0.08%, at 2 kV/mm). Symmetric butterfly-shaped loop, a characteristic of good piezoelectric system, is observed, which establishes the utility of PMN– *x*PT ceramics for actuator applications. The effective piezoelectric coefficient d_{33} of PMN–*x*PT ceramics as a function of electric field d_{33} -*E* curves is shown in Fig. 4(c). It can be seen that the d_{33} -*E* curve of the sample follows the standard ferroelectric hysteresis loop shape. The maximum piezoelectric

Fig. 4. The (a) *P–E* loops, (b) *S–E* loops, (c) d_{33} –*E* loops and (d) ε_r –*E* loops of PMN–*xPT* ceramics.

Fig. 5. Pyroelectric constant and F_v as a function of temperature for PMN–*x*PT ceramics.

coefficient reaches 320 pm/V, and with the increase of PT content, its value increases, due to the increase of relaxation, being consistent with the previous *P*-*E* diagram. It can be seen from Fig. 4(d) that the dielectric constant decreases with the PT content at zero bias voltage, and the dielectric response is the largest when the PT content is 25. With the increase of bias field, the difference of dielectric response decreases gradually, which is analogous to the changing trend of the C–V characteristics of the PZT system with composition in the literatures $30,31$ (the dielectric response is the largest at zero bias field, and the difference decreases gradually with the increase of bias field). According to the maximum dielectric response at the low bias field of PMN–25PT, this component has the largest contribution of domain wall motion. However, the domain wall motion will be frozen by the bias field. When the bias field increases, the contribution of the domain wall motion to the dielectric response decreases gradually. The dielectric response also decreases with the change of composition.

The pyroelectric coefficient and voltage response F_v of PMN–*x*PT ceramics are investigated, as shown in Figs. 5(a) and 5(b), respectively. It can be seen from Fig. 5(a) that the pyroelectric coefficient decreases slightly with the increase of PT content at room temperature. However, the pyroelectric coefficient of the ceramic system remains in the range of 5.5–6.3 × 10⁻⁸ C·cm⁻²·K⁻¹, indicating that the pyroelectric coefficient of the ceramic system can be maintained in a stable range. At the same time, the peak p_{max} of the pyroelectric coefficient also shows similar changes at the $F_{RL} - F_{RH}$ phase transition temperature. However, it can be seen that the position of p_{max} peak of PMN–26PT ceramics is obviously different from that of other components. Because the composition of PMN–26PT ceramic was very close to the MPB region, so it has a high $F_{RL} - F_{RH}$ phase transition temperature, which

is also consistent with the results of the dielectric spectrum. The curve in Fig. 5(b) shows the variation of the optimal voltage response value F_v of the sample with temperature, which is consistent with the variation of pyroelectric coefficient. At room temperature, the voltage response F_v of the ceramic system is between $2.1-2.5 \times 10^{-8}$ C·cm·J⁻¹.

4. Conclusion

The phase structure, microstructure and electrical properties of PMN–*x*PT ceramics were systematically investigated in this study. Well-shaped and saturated *P*–*E* hysteresis loops with high room temperature remnant polarization, a high electro-strain of 0.08% at 2 kV/mm, and effective piezoelectric coefficient of 320 pm/V could be obtained. The PMN– *x*PT ceramics are found to have a very high pyroelectric coefficient of 5.5–6.3 × 10⁻⁸ C·cm⁻²·K⁻¹ and F_v of 2.1–2.5 × 10−8 C·cm·J−1 at room temperature. The results suggest that PMN–*x*PT ceramics are promising candidates for piezoelectric and pyroelectric applications.

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