

RF characterization of InP double heterojunction bipolar transistors on a flexible substrate under bending conditions

Lishu Wu^{1,2}, Jiayun Dai², Yuechan Kong², Tangsheng Chen², and Tong Zhang^{1,3,†}

¹Joint International Research Laboratory of Information Display and Visualization, School of Electronic Science and Engineering, Southeast University, Nanjing 210096, China

²Science and Technology on Monolithic Integrated Circuits and Modules Laboratory, Nanjing Electronic Devices Institute, Nanjing 210016, China

³Key Laboratory of Micro-Inertial Instrument and Advanced Navigation Technology, Ministry of Education, School of Instrument Science and Engineering, Southeast University, Nanjing 210096, China

Abstract: This letter presents the fabrication of InP double heterojunction bipolar transistors (DHBTs) on a 3-inch flexible substrate with various thickness values of the benzocyclobutene (BCB) adhesive bonding layer, the corresponding thermal resistance of the InP DHBT on flexible substrate is also measured and calculated. InP DHBT on a flexible substrate with 100 nm BCB obtains cut-off frequency $f_T = 358$ GHz and maximum oscillation frequency $f_{MAX} = 530$ GHz. Moreover, the frequency performance of the InP DHBT on flexible substrates at different bending radii are compared. It is shown that the bending strain has little effect on the frequency characteristics (less than 8.5%), and these bending tests prove that InP DHBT has feasible flexibility.

Key words: InP DHBT; thermal resistance; radio frequency; bending

Citation: L S Wu, J Y Dai, Y C Kong, T S Chen, and T Zhang, RF characterization of InP double heterojunction bipolar transistors on a flexible substrate under bending conditions[J]. *J. Semicond.*, 2022, 43(9), 092601. <https://doi.org/10.1088/1674-4926/43/9/092601>

1. Introduction

Flexible electronics have unique advantages of flexibility, ductility and portability, which have wide application prospects in communication information, energy, medical and other fields^[1–6]. However, the future application of high frequency communication and wireless internet of things puts forward higher requirements on the frequency of flexible electronics. The current traditional flexible electronic devices and circuits cannot meet the requirements of larger bandwidth and higher speed, because these flexible electronic devices have low carrier mobility and saturation speed in a higher frequency range^[7–9]. As a result, high performance RF transistors and circuits with higher speeds and frequencies are in great demand.

At present, various types of flexible electronic materials and devices have been developed and applied, such as graphene/carbon transistor, GaAs HBT/HEMT, Si MOSFET, etc., all of which have their own unique advantages and application fields^[10–17]. We have reported a fabrication method for transferring InP DHBTs onto a flexible substrate using benzocyclobutene (BCB) bonding technology lately. The flexible substrate InP DHBT device has the cut off frequency $f_T = 337$ GHz and oscillation frequency $f_{MAX} = 485$ GHz^[18]. In this paper, we continue to present an optimized process of the BCB adhesive layer between InP DHBT and the flexible substrate, which can operate at higher cut off frequency $f_T = 358$ GHz and oscillation

frequency $f_{MAX} = 530$ GHz, the thermal resistance (R_{th}) of InP DHBT on flexible substrate is estimated. In addition, the RF performance under different bending radii is also compared.

2. Fabrication process

The process of fabricating InP DHBT devices on flexible substrate has been reported in previous work with identical device geometry^[18], while the standard 0.5 μm process is used for InP DHBT devices. Fig. 1 shows a schematic diagram of InP DHBT devices on flexible substrate.

The BCB adhesive layer is sandwiched between InP DHBTs layers and flexible substrate, the thermal conductivity of BCB is 0.3, and InP is 68 W/(m·K), the flexible substrate material used in this letter is boron nitride (BN) composite polymer material, which has a thermal conductivity greater than 8 W/(m·K). Considering the BCB having low thermal conductivity, it is necessary to evaluate the different thickness of BCB adhesive layer which affect the RF and I - V performances of InP DHBT.

The BCB adhesive layer is spun onto two groups of 3-

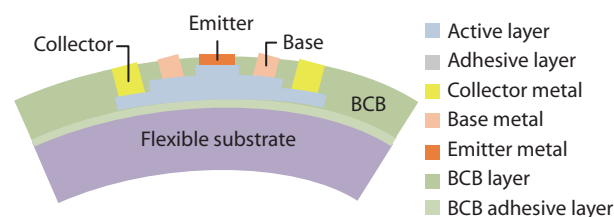


Fig. 1. (Color online) The schematic diagram of InP DHBT device on flexible substrate.

Correspondence to: T Zhang, tzhang@seu.edu.cn

Received 20 MARCH 2022; Revised 19 APRIL 2022.

©2022 Chinese Institute of Electronics

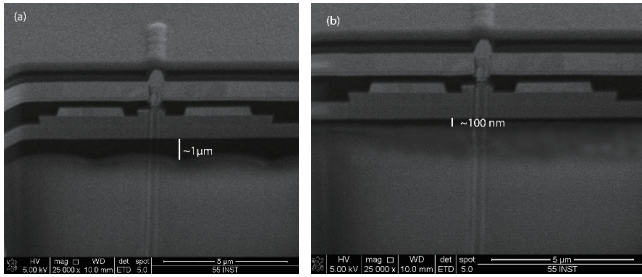


Fig. 2. (a) FIB cross-sectional image of InP DHBT device on flexible substrate with 1 μm BCB. (b) FIB cross-sectional image of InP DHBT device on flexible substrate with 100 nm BCB.

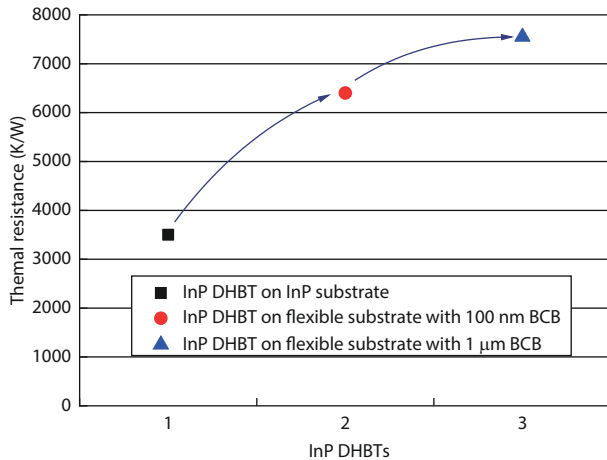


Fig. 3. (Color online) Experimental and calculated R_{th} for InP DHBT and flexible substrate InP DHBT.

inch flexible substrates with BCB thickness of 100 nm and 1 μm , respectively. After the InP DHBT device is bonded to the flexible substrate, the BCB thickness under the InP DHBT device is measured by the focused ion beam (FIB), as shown in Figs. 2(a) and 2(b), which shows the FIB image of InP DHBT on the flexible substrate, the thickness of BCB can be measured separately.

3. Results and discussions

To make a heat dissipation evaluation of InP DHBT device on flexible substrate, thermal resistance (R_{th}) of InP DHBT was measured. A large output current leads to an increasing amount of self-heating. Fig. 3 shows the calculated and experimental R_{th} of fabricated InP DHBT with the emitter area of $A_{\text{E}} = 0.5 \times 5 \mu\text{m}^2$. The current gain and emitter-base voltage vary with temperature to evaluate thermal resistance of the device, R_{th} is expressed by the following relation^[19]:

$$R_{\text{th}} = \frac{1}{\phi} \frac{\Delta V_{\text{be}}}{P_{\text{diss}}}. \quad (1)$$

The ϕ is a thermo-electrical coefficient expressed from Gummel plots with different testing temperatures, V_{be} is the base-emitter voltage for a constant collector current, the ϕ can be expressed as $\Delta V_{\text{be}} = \phi \cdot \Delta T$, the ΔT in junction temperature versus the backplate temperature for a certain power P_{diss} dissipated in the InP DHBT. And the P_{diss} dissipated power variation with $P_{\text{diss}} = \Delta V_{\text{ce}} \cdot I_{\text{c}}$. The measured ϕ is about 0.84 mV/K of InP DHBT device. The measured R_{th} of a conventional InP DHBT device on the InP substrate is 3505 K/W, while the InP

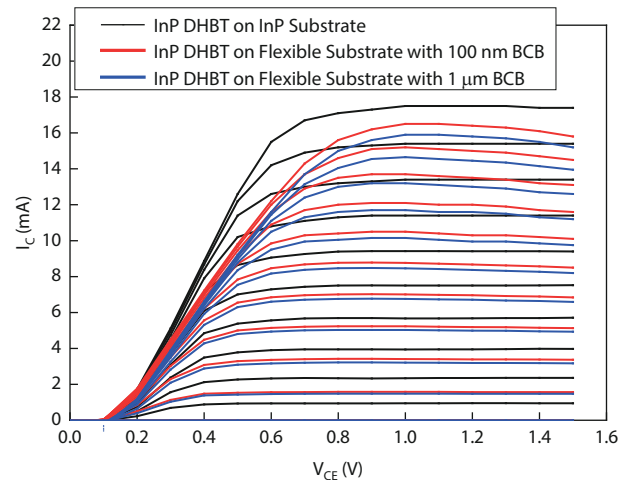


Fig. 4. (Color online) The corresponding $I_{\text{c}}-V_{\text{CE}}$ of InP DHBT and flexible substrate InP DHBT.

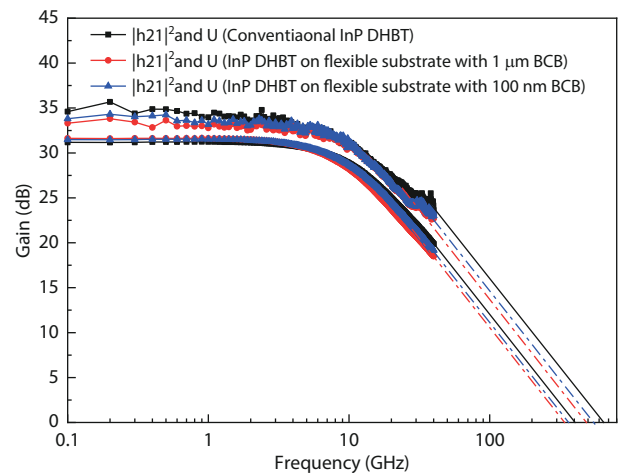


Fig. 5. (Color online) Mason's unilateral gain U and $|h_{21}|^2$ as a function of frequency measured the InP DHBT and flexible substrate InP DHBT.

DHBT device on a flexible substrate with 100 nm BCB exhibits R_{th} of 6410 K/W, which is about an 82.8% increase. And the InP DHBT device on a flexible substrate with 1 μm BCB exhibits R_{th} of 7550 K/W, which is attributed to the low thermal conductivity of flexible substrate and BCB.

$I-V$ measurements of flexible substrate InP DHBT devices were performed on a semiconductor wafer probe, Fig. 4 shows the common emitter $I_{\text{c}}-V_{\text{CE}}$ characteristics of flexible substrate InP DHBT devices with two different thickness of BCB. It can be confirmed that the $I_{\text{c}}-V_{\text{CE}}$ characteristics of InP DHBT devices with different BCB thicknesses are degraded to a certain extent, and the BCB with the thickness of 1 μm is degraded more seriously, this result corresponds to an increase in thermal resistance.

The RF performance of flexible substrate InP DHBTs are measured by vector network analyzer, which using off-wafer line-line-reflect-match calibration, at the same time, the device pads are de-embedded with open/short calibration structures^[20-23]. Fig. 5 shows the InP DHBT short-circuit current gain $|h_{21}|^2$ and Mason's unilateral gain U on frequency function, when the $V_{\text{CE}} = 1.5 \text{ V}$ and collector current $I_{\text{c}} = 15 \text{ mA}$. Using extrapolation of U and $|h_{21}|^2$ with a -20 dB/dec roll-off yields method, which shows the cut off frequency $f_{\text{T}} = 395 \text{ GHz}$, the maximum oscillation frequency $f_{\text{MAX}} = 630 \text{ GHz}$

Table 1. Comparison of the f_T and f_{MAX} with other previous reported flexible transistors.

Device	f_T (GHz)	f_{MAX} (GHz)	Ref.
Graphene transistor	198	28.2	[13]
InAs MOSFET	105	22.9	[15]
InGaAs/InAlAs HEMT	160	290	[17]
GaAs HBT	37.5	6.9	[24]
GaN HEMT	60	115	[25]
SOI CMOS	150	160	[26]
Si MOFET	5	38	[27]
InP DHBT	337	485	[18]
InP DHBT	358	530	This Work

of the InP DHBT on InP substrate. For the flexible substrate InP DHBT with 100 nm BCB, the cut off frequency f_T and maximum oscillation f_{MAX} are 358 and 530 GHz respectively.

The RF performance f_T and f_{MAX} of the flexible substrate InP DHBT device in this paper are compared with the performance of other flexible transistors reported previously in Refs. [13, 15, 17, 18, 24–27], as shown in Table 1. Our work shows the highest RF frequency performance of flexible devices to date, besides confirms the potential of flexible substrate InP DHBT for high frequency applications.

At the same time, in order to explore the influence of flexible substrate bending on the high-frequency performance of InP DHBT devices, the 3-inch flexible substrate InP DHBT is pasted on curved glass with a certain bending radius^[28–30]. The bending degree of flexible substrate depends on the bending radius of curved glass, as shown in Fig. 6(a). Three different bending radii of 70, 30 and 15 mm are set to measure the high frequency performance of the flexible substrate InP DHBT. Figs. 6(b) and 6(c) show a comparison of the frequency characteristics of InP DHBT at these three bending radii. It is observed that a decrease in the bending radii leads to a slight degradation of the device's high-frequency performance, although in a case there is a small increase in f_T as the bending increases. The f_T and f_{MAX} of the device in the bent state are reduced by about 8.5% compared with that in the flat state. The performance of InP DHBT devices decreases slightly under different bending states, which may be related to strain, it affects the carrier mobility and other properties of InP DHBT.

4. Conclusion

A standard 0.5 μm process of InP DHBT is fabricated on 3-inch flexible substrate using epitaxial lift-off and BCB adhesive bonding techniques. Different thickness values of BCB adhesive bonding layer and the corresponding thermal resistance are investigated, besides high cut-off frequency $f_T = 358$ GHz and maximum oscillation $f_{MAX} = 530$ GHz are obtained. Moreover, the RF performance under different bending radii is also compared, and the results show that the RF performance of the flexible InP DHBT is less affected by bending strain. These results further confirm the possibility that flexible InP DHBT will be used in flexible RF circuits.

Acknowledgments

This work was supported in part by National Natural Science Foundation of China under Grants 61875241.

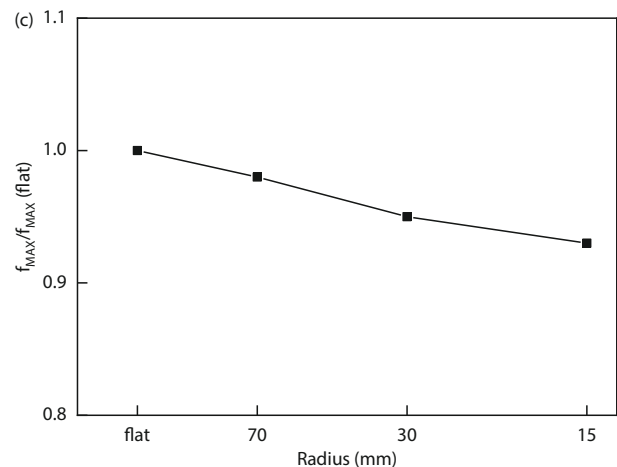
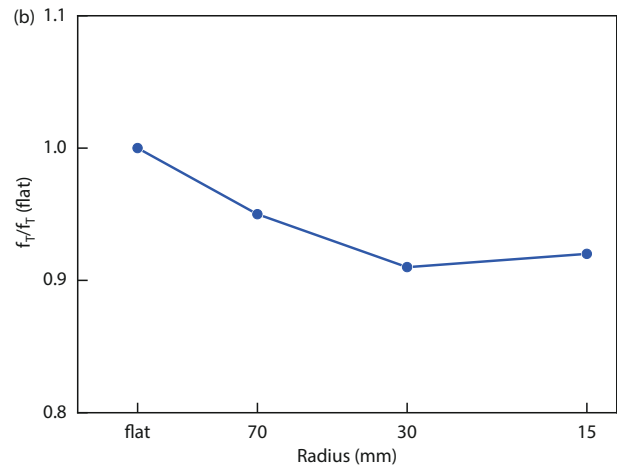


Fig. 6. (Color online) (a) Photographs of InP DHBT on flexible substrate under bending conditions on test bench. The InP DHBT frequency performance under different bending radii: (b) $f_T/f_T(\text{flat})$, (c) $f_{MAX}/f_{MAX}(\text{flat})$.

References

- [1] Cherenack K H, Kattamis A Z, Hekmatshoar B, et al. Amorphous-silicon thin-film transistors fabricated at 300 °C on a free-standing foil substrate of clear plastic. *IEEE Electron Device Lett*, 2007, 28, 1004
- [2] Saxena S, Kim D C, Park J H, et al. Polycrystalline silicon thin-film transistor using Xe flash-lamp annealing. *IEEE Electron Device Lett*, 2010, 31, 1242
- [3] Crone B, Dodabalapur A, Lin Y Y, et al. Large-scale complementary integrated circuits based on organic transistors. *Nature*, 2000, 403, 521
- [4] Haas U, Gold H, Haase A, et al. Submicron pentacene-based organ-

- ic thin film transistors on flexible substrates. *Appl Phys Lett*, 2007, 91, 043511
- [5] Takahashi T, Takei K, Adabi E, et al. Parallel array InAs nanowire transistors for mechanically bendable, ultrahigh frequency electronics. *ACS Nano*, 2010, 4, 5855
- [6] Menard E, Nuzzo R G, Rogers J A. Bendable single crystal silicon thin film transistors formed by printing on plastic substrates. *Appl Phys Lett*, 2005, 86, 093507
- [7] Ahn J H, Kim H S, Lee K J, et al. High-speed mechanically flexible single-crystal silicon thin-film transistors on plastic substrates. *IEEE Electron Device Lett*, 2006, 27, 460
- [8] Lin Y M, Dimitrakopoulos C, Jenkins K A, et al. 100-GHz transistors from wafer-scale epitaxial graphene. *Science*, 2010, 327, 662
- [9] Cao Y, Brady G J, Gui H, et al. Radio frequency transistors using aligned semiconducting carbon nanotubes with current-gain cutoff frequency and maximum oscillation frequency simultaneously greater than 70 GHz. *ACS Nano*, 2016, 10, 6782
- [10] Sun Y G, Menard E, Rogers J A, et al. Gigahertz operation in flexible transistors on plastic substrates. *Appl Phys Lett*, 2006, 88, 183509
- [11] Akinwande D, Petrone N, Hone J. Two-dimensional flexible nanoelectronics. *Nat Commun*, 2014, 5, 5678
- [12] Lee K J, Meitl M A, Ahn J H, et al. Bendable GaN high electron mobility transistors on plastic substrates. *J Appl Phys*, 2006, 100, 124507
- [13] Petrone N, Meric I, Chari T R, et al. Graphene field-effect transistors for radio-frequency flexible electronics. *IEEE J Electron Devices Soc*, 2015, 3, 44
- [14] Lee J, Ha T J, Li H F, et al. 25 GHz embedded-gate graphene transistors with high-K dielectrics on extremely flexible plastic sheets. *ACS Nano*, 2013, 7, 7744
- [15] Wang C, Chien J C, Fang H, et al. Self-aligned, extremely high frequency III-V metal-oxide-semiconductor field-effect transistors on rigid and flexible substrates. *Nano Lett*, 2012, 12, 4140
- [16] Shi J, Wichmann N, Roelens Y, et al. Microwave performance of 100 nm-gate $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}/\text{In}_{0.52}\text{Al}_{0.48}\text{As}$ high electron mobility transistors on plastic flexible substrate. *Appl Phys Lett*, 2011, 99, 203505
- [17] Shi J, Wichmann N, Roelens Y, et al. Electrical characterization of $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}/\text{In}_{0.52}\text{Al}_{0.48}\text{As}$ high electron mobility transistors on plastic flexible substrate under mechanical bending conditions. *Appl Phys Lett*, 2013, 102, 243503
- [18] Wu L S, Dai J Y, Wang Y, et al. High performance wafer scale flexible InP double heterogeneous bipolar transistors. *Semicond Sci Technol*, 2021, 36, 03LT02
- [19] Liu W. Thermal-electrical properties. In: Handbook III-V Heterojunction Bipolar Transistors. New York: Wiley, 1998
- [20] Ruiz-Palmero J M, Hammer U, Jäckel H, et al. Comparative technology assessment of future InP HBT ultrahigh-speed digital circuits. *Solid State Electron*, 2007, 51, 842
- [21] Niu B, Wang Y, Cheng W, et al. Common base four-finger InGaAs/InP double heterojunction bipolar transistor with maximum oscillation frequency 535 GHz. *Chin Phys Lett*, 2015, 32, 172
- [22] Cheng W, Wang Y, Zhao Y, et al. A THz InGaAs/InP double heterojunction bipolar transistor with $f_{\text{max}} = 325$ GHz and $BV_{\text{CBO}} = 10.6$ V. *J Semicond*, 2013, 34, 054006
- [23] Jung Y H, Chang T H, Zhang H L, et al. High-performance green flexible electronics based on biodegradable cellulose nanofibril paper. *Nat Commun*, 2015, 6, 7170
- [24] Zeng Y P, Ostinelli O, Lövbom R, et al. 400-GHz InP/GaAsSb DHBTs with low-noise microwave performance. *IEEE Electron Device Lett*, 2010, 31, 1122
- [25] Chang T H, Xiong K L, Park S H, et al. High power fast flexible electronics: Transparent RF AlGaIn/GaN HEMTs on plastic substrates. *2015 IEEE MTT-S International Microwave Symposium*, 2015, 1
- [26] Lecavelier des Etangs-Levallois A, Dubois E, Lesecq M, et al. 150-GHz RF SOI-CMOS technology in ultrathin regime on organic substrate. *IEEE Electron Device Lett*, 2011, 32, 1510
- [27] Seo J H, Ling T, Gong S Q, et al. Fast flexible transistors with a nanotrench structure. *Sci Rep*, 2016, 6, 24771
- [28] Qin G X, Cai T H, Yuan H C, et al. Flexible radio-frequency single-crystal germanium switch on plastic substrates. *Appl Phys Lett*, 2014, 104, 163501
- [29] Cho S J, Jung Y H, Ma Z Q. X-band compatible flexible microwave inductors and capacitors on plastic substrate. *IEEE J Electron Devices Soc*, 2015, 3, 435
- [30] Sun L, Qin G X, Huang H, et al. Flexible high-frequency microwave inductors and capacitors integrated on a polyethylene terephthalate substrate. *Appl Phys Lett*, 2010, 96, 013509



Lishu Wu received the M.S. degree from Southeast University in 2010. He is currently pursuing the Ph.D. degree in electronic science and engineering from Southeast University. His research interest includes the technology of heterogeneous integration of compound semiconductor with Si CMOS and flexible substrate. He is the author of more than 10 articles, and more than 15 inventions.



Tong Zhang is a professor at Southeast University. He is engaged in micro-nano integrated devices, surface plasmons, microwave photonics and other fields. He has undertaken more than 40 major research projects of the Ministry of Science and Technology and the National Natural Science Foundation of China. He has been granted 6 American invention patents and more than 50 Chinese invention patents. He has published more than 140 papers and 5 monographs and translated books.