

A 10 × 10 deep ultraviolet light-emitting micro-LED array

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Abstract: In this work, we design and fabricate a deep ultraviolet (DUV) light-emitting array consisting of 10 × 10 micro-LEDs (μ -LEDs) with each device having 20 μm in diameter. Strikingly, the array demonstrates a significant enhancement of total light output power by nearly 52% at the injection current of 100 mA, in comparison to a conventional large LED chip whose emitting area is the same as the array. A much higher (~22%) peak external quantum efficiency, as well as a smaller efficiency droop for μ -LED array, was also achieved. The numerical calculation reveals that the performance boost can be attributed to the higher light extraction efficiency at the edge of each μ -LED. Additionally, the far-field pattern measurement shows that the μ -LED array possesses a better forward directionality of emission. These findings shed light on the enhancement of the DUV LEDs performance and provide new insights in controlling the light behavior of the μ -LEDs.

Key words: AlGaIn; deep ultraviolet; micro-LED array; light extraction efficiency

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1. Introduction

AlGaIn-based deep ultraviolet light-emitting diodes (LEDs) have been identified as the next-generation DUV light source owing to the narrow emission wavelength band, non-toxicity, lower power consumption, and compact size with a long lifetime^[1, 2]. Up to now, they have attracted significant research interest owing to potential applications, including non-light-of-sight optical communication, sensing systems, sterilization, and medical phototherapy^[3]. However, the implementation of DUV LEDs in those industrial applications is restrained from their limited wall-plug efficiency (WPE), poor external quantum efficiency (EQE), and low light output power (LOP)^[4]. One of the main limiting factors of the poor optical performance for the DUV LED is the extremely low light extraction efficiency (LEE), which is less than 10%^[2]. Such low LEE is mainly owing to three reasons. Firstly, a large number of the upward-traveling DUV photons can be absorbed by the p-type GaIn-based hole-injection layer or can be blocked by the p-contact metals^[5]. Secondly, most of the downward-traveling DUV photons are constantly reflected due to the excessive difference in the refractive index by the multiple nitride epilayers, AlGaIn/sapphire, and sapphire/air interfaces^[6]. Thirdly, unlike the visible LEDs, the DUV LEDs are based on the AlGaIn materials with high aluminum content, leading to the increased transverse magnetic/transverse electric (TM/TE) polarization ratio^[7]. Since the propagation direction is perpendicular to the *c*-axis, the in-plane TM photons are extremely hard to be extracted to the external space^[8].

To enlarge the LEEs, many efforts have been continuously devoted to extracting more UV photons in the DUV

LED chips. For extracting those upward-traveling DUV photons, many strategies such as high-reflectivity metal contacts^[9, 10], meshed p-GaIn structure^[11, 12], and photonic crystal structure^[13] have been reported. Moreover, a variety of micro/nanostructures, including the nano-lens^[6, 14, 15], a patterned sapphire substrate^[16–19] and localized surface plasmons^[20], have been demonstrated for reducing the total internal reflection (TIR)^[21], which can help to extract the downward-traveling DUV photons in the DUV LEDs. Besides, the optimization of the angle^[22], the geometric shape^[23], and the reflector of the sidewall^[24, 25] have also been investigated to enhance the emission of the TM-polarized light arriving at the chip sidewalls.

Apart from these important investigations, the emerging DUV micro-LED (μ -LED) device architecture and the preliminary device characterizations show its potential to enhance the EQE^[26], which could be attributed to the reduction of the re-absorption of sideways-traveling photons as revealed by a recent cathodoluminescence study^[27]. However, it should be noted that each μ -LED inevitably possesses very low LOP due to the reduced emission area, which seriously hindered their further applications. Therefore, it is necessary to build interconnected DUV μ -LEDs to obtain large output power, called μ -LED arrays. Recently, Floyd *et al.* found that DUV μ -LED array structure can significantly reduce the thermal impedance of each μ -LED and thus enhance the sidewall out-radiation of the self-generated heat^[28]. However, so far, the underlying mechanism of performance enhancement for those μ -LED arrays is still lacking, and no systematic investigation, particularly from an optical perspective, on the light propagation within each μ -LED and its array has been carried out.

In this letter, we present a systematic study on the electrical and optical behavior of light-emitting arrays. We designed and fabricated two kinds of arrays. One array is composed of 10 × 10 μ -LEDs, with each device having 20 μm in diameter,

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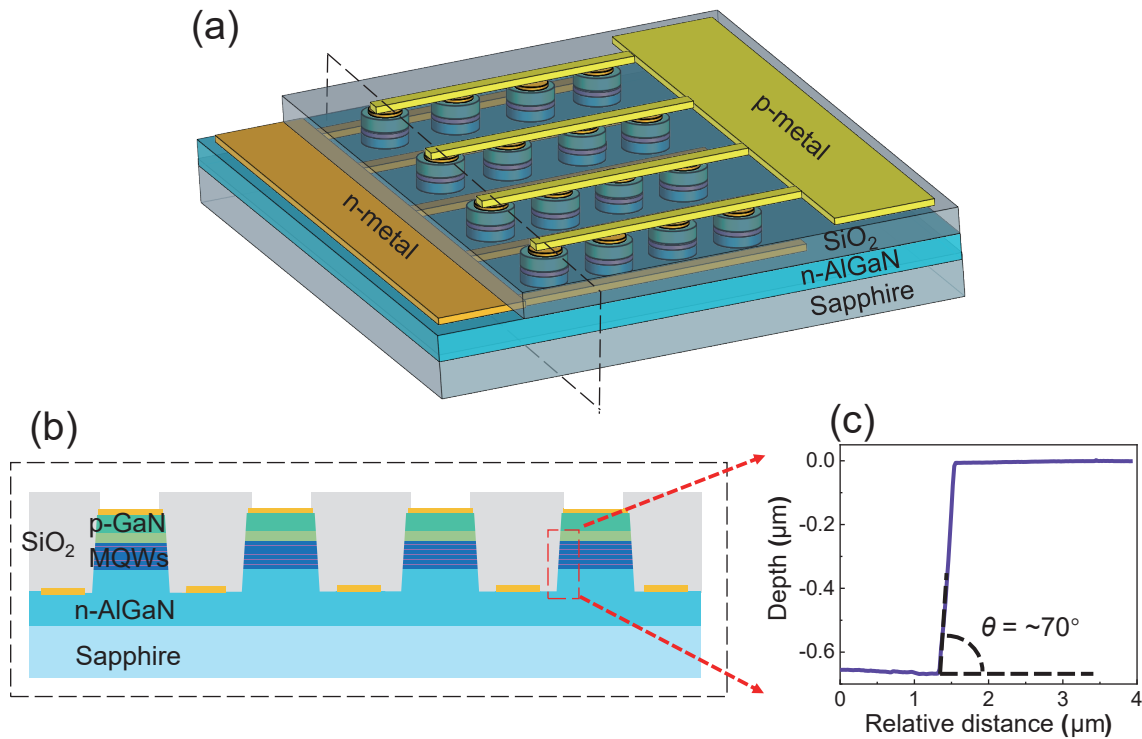


Fig. 1. (Color online) (a) Schematic of a fabricated DUV μ -LED array and (b) its cross-section of the DUV μ -LED array and (c) the profile of the sidewall and θ is the inclination angle of the sidewall.

named as μ -LED array ($20\ \mu\text{m}$) and another array is made of $4 \times 4\ \mu$ -LEDs with each device showing $50\ \mu\text{m}$ in diameter, named as μ -LED array ($50\ \mu\text{m}$). At the same time, we fabricated a regular conventional LED (C-LED) whose surface-emitting area is identical to those two types of arrays. During the device test, we found that the μ -LED array shows significantly boosted EQE, WPE, and LOP performance, owing to the enlarged LEE in each μ -LED with a smaller chip size. The numerical finite-difference time-domain (FDTD) calculations have been implemented to better understand the light propagation behavior within LED chips with different chip sizes and to reveal the underlying mechanism of the LEE enhancement in μ -LEDs.

2. Experiments

Similar to our previous report^[26], the epi-structure for our DUV LEDs consist of a $2\text{-}\mu\text{m}$ -thick AlN buffer layer on the *c*-plane sapphire substrate, a $2\text{-}\mu\text{m}$ -thick *n*-doped $\text{Al}_{0.6}\text{Ga}_{0.4}\text{N}$ layer, a $0.6\text{-}\mu\text{m}$ -thick *n*-doped $\text{Al}_{0.48}\text{Ga}_{0.52}\text{N}$ layer followed by five periods $\text{Al}_{0.45}\text{Ga}_{0.55}\text{N}/\text{Al}_{0.60}\text{Ga}_{0.40}\text{N}$ ($2.5\ \text{nm}/10\ \text{nm}$) MQWs, a 50-nm -thick *p*-doped $\text{Al}_{0.70}\text{Ga}_{0.30}\text{N}$ electron blocking layer, and a 350-nm -thick *p*-GaIn. The wafers were fabricated into the truncated cone-shaped active mesas using the inductively coupled plasma (ICP) etching equipment. The C-LED has an emission area of $200\ \mu\text{m}$ in diameter. The 4×4 and $10 \times 10\ \mu$ -LED arrays have chip size of $50\ \mu\text{m}$ in diameter and $20\ \mu\text{m}$ in diameter, respectively. We intended to keep the same total emission area for these three kinds of devices for performance comparison. Then, the metal stack of Ti/Al/Ni/Au ($20/80/40/100\ \text{nm}$) as *n*-electrode and the Ni/Au ($20/50\ \text{nm}$) as *p*-type contact was deposited by the electron beam evaporator. An 800-nm -thick SiO_2 film was deposited as an electrical insulation layer by using plasma-enhanced chemical vapor

deposition (PECVD). Next, the SiO_2 film on the *n*- and *p*-electrode was etched by the reactive ion etching (RIE) first and then by the buffer oxide etchant (BOE). Finally, the Ni/Al/Ni/Au ($20/500/100/120\ \text{nm}$) metal contacts were formed by the electron beam evaporator. The schematic of the μ -LED array and its cross-section epi-structure are shown in Figs. 1(a) and 1(b), respectively.

The inclination angle of the sidewalls is around 70° which is characterized by the atomic force microscopy (AFM), as shown in Fig. 1(c). The electroluminescence (EL) spectra, the light output power, and the far-field emission for all the fabricated devices were measured from the back of the sapphire (not the epi-side) at room temperature. The far-field emission distribution of the LEDs was recorded by measuring the radiant intensity in angular steps of 10° on a three-axes rotation stage using a power meter at a distance of $50\ \text{mm}$ from the LED chips.

3. Results and discussions

The current–voltage (*I*–*V*) curves for all the three investigated DUV LEDs are illustrated in Fig. 2(a). The forward voltages for the μ -LED array ($50\ \mu\text{m}$) and the μ -LED array ($20\ \mu\text{m}$) are slightly lower than that for the C-LED, as a result of the lower series resistance in the parallel device configuration and different *n*-contact areas. The inset of Fig. 2(a) shows the logarithmic plot of the forward *I*–*V* curves. The reverse bias leakage values were as low as $\sim 0.1\ \text{pA}$ at an applied voltage of $-4\ \text{V}$, showing the high quality of the as-grown epi-films and the low damage of the device during the dry-etching process. Notably, the μ -LED array has a minor increase of leakage current than that of the C-LED, which could be attributed to the sidewall defects that may act as the current leakage pathways^[29]. The EL spectra for the

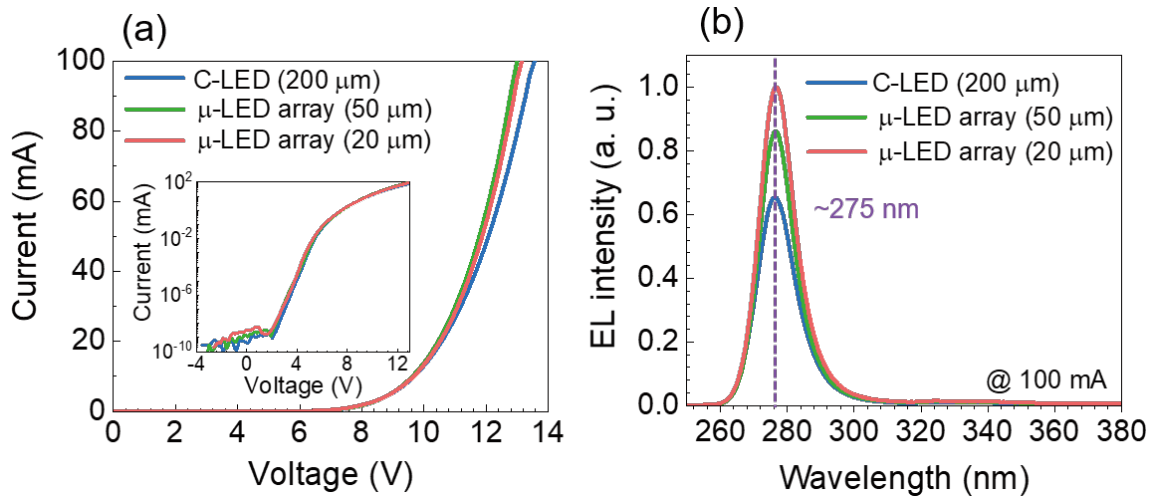


Fig. 2. (Color online) (a) The current–voltage (I – V) characteristic of the DUV LEDs. The inset shows the corresponding logarithmic plot. (b) The spectra of the DUV LEDs operating at the driving current of 100 mA.

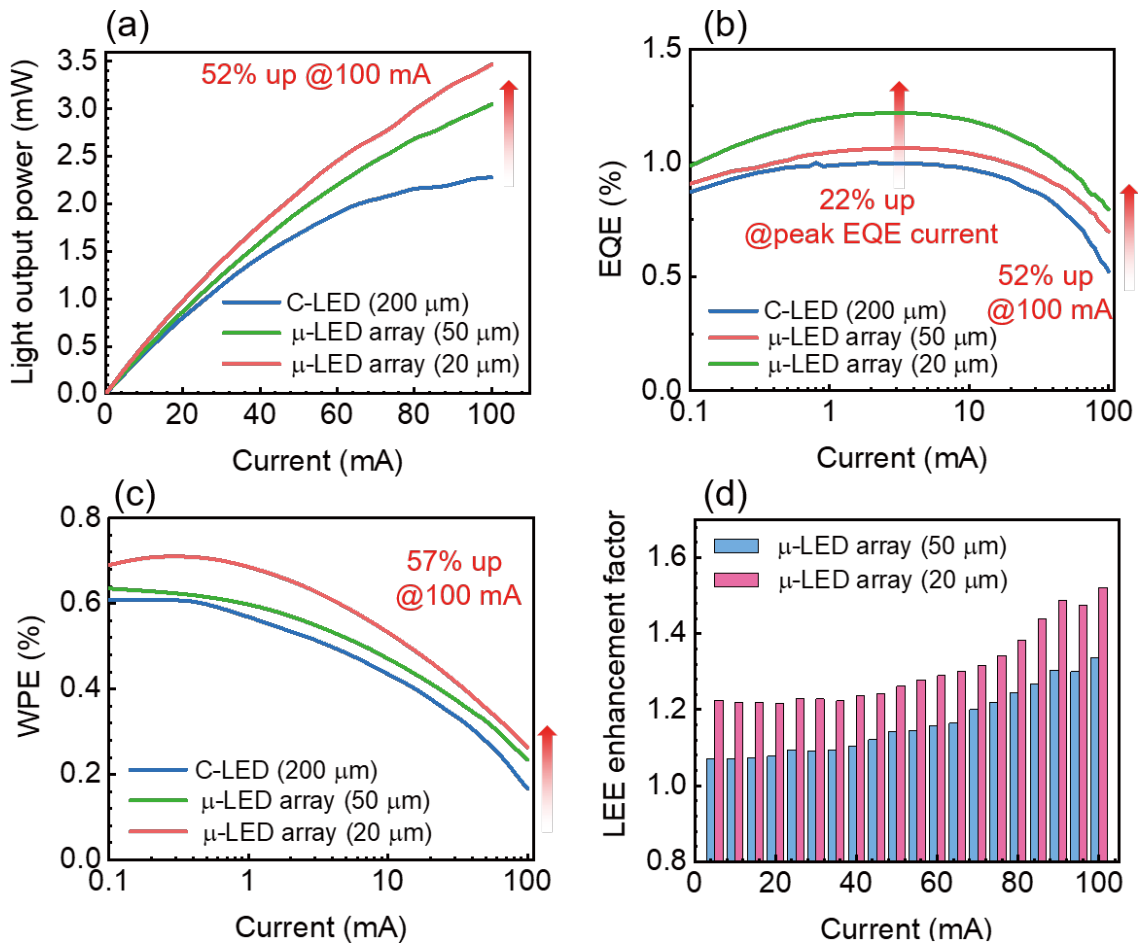


Fig. 3. (Color online) (a) The light output power (LOP), (b) the external quantum efficiency (EQE), (c) the wall-plug efficiency, and (d) the LEE enhancement factor of the DUV LEDs at different currents for the three investigated devices.

three devices at the injection current of 100 mA are shown in Fig. 2(b). The peak wavelength for all the devices is ~ 275 nm, indicating that the change of the cone mesa size does not affect the emission wavelength. The EL emission intensity for the array is higher than that of the C-LED, and the μ -LED with a smaller diameter shows a higher EL intensity, which provides an initial confirmation of the performance enhancement of the μ -LED array.

As shown in Fig. 3(a), the μ -LED array (50 μm) and the μ -LED array (20 μm) exhibit a higher LOP by 34% and 52% than that of the C-LED under the injected current level of 100 mA, respectively. Notably, the LOP of the device gradually increases with the increased injection current, but the LOP of C-LED reaches the maximum value at about 100 mA (the injected current density of 318 A/cm²) owing to the current injection saturation. Importantly, the μ -LED array can sustain a

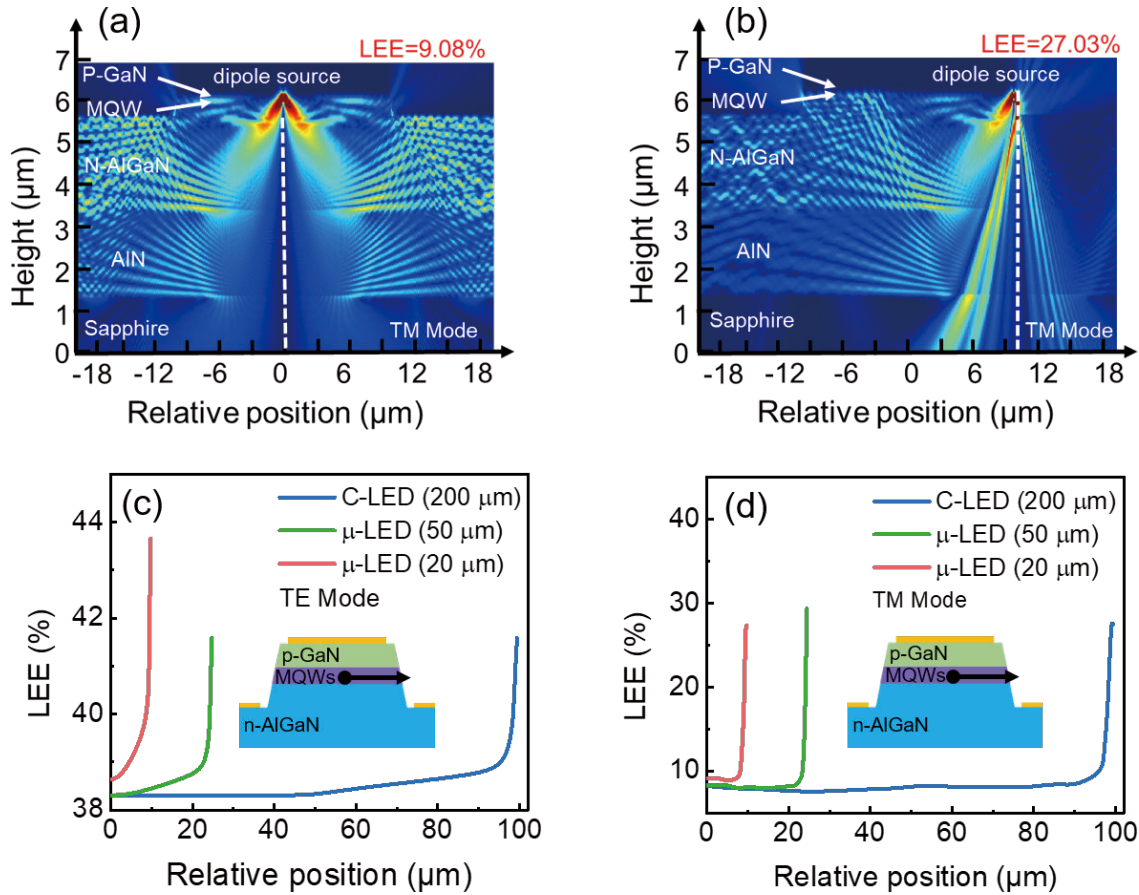


Fig. 4. (Color online) Electric field distributions for the light propagation paths of the TM-polarized light when the dipole source at (a) the center of the mesa and (b) the edge of the mesa. The LEEs for the (c) TE- and (d) TM-polarized light as a function of the position of the dipole source for the C-LED, μ -LED (50 μm), and μ -LED (20 μm), respectively. The insets of the (c) and (d) are the device schematic which indicates the position change of the dipole source.

much higher current injection. In the μ -LED array, since the μ -LEDs are interconnected in parallel, each μ -LED is only injected several milliamperes under the total injection current of 100 mA, which is far from the current saturation. Therefore, the enhanced LOP leads to a significant higher EQE by 34% for the μ -LED array (50 μm) and by 52% for the μ -LED array (20 μm) at 100 mA, as displayed in Fig. 3(b). The peak EQE is 7% and 22% higher in the μ -LED array (50 μm) and μ -LED array (20 μm), respectively, in comparison to that of the C-LED. We also quantify the EQE droop levels at the injection current of 100 mA (the droop is defined as from the highest to the lowest), which are 47.2%, 34.6%, and 34.1% for the C-LED, the μ -LED array (50 μm), and the μ -LED array (20 μm), respectively. Then, the WPE values of the LEDs can be calculated from LOP measurements by^[2],

$$\text{WPE} = \text{EQE} \cdot \text{CIE} = \text{LOP}/(IV) \quad (1)$$

From the calculation results shown in Fig. 3(c), the μ -LED array (50 μm) has higher WPE by 40%, and μ -LED array (20 μm) has higher WPE by 57% at 100 mA than that of the C-LED. This improvement is slightly larger than the EQE enhancement at 100 mA (34% for μ -LED array (50 μm) and 52% for μ -LED array (20 μm)), due to the possible higher current injection efficiency (CIE) in the μ -LED array configuration. Nevertheless, it can be explained that the enhancement of the WPE mainly lies in the effective improvement of EQE since all

three LEDs have the same internal quantum efficiency (IQE) as they are fabricated on the same wafer. Therefore, there are ample reasons to explain that the enhancement of the LOP, EQE, and WPE is mainly attributed to the improvement of LEE. Furthermore, Fig. 3(d) shows the LEE enhancement factor^[30] obtained by the ratio of EQE of the μ -LED array to C-LED. The LEEs of the μ -LED array (50 μm) and μ -LED array (20 μm) are approximately 1.3 times and 1.5 times higher in comparison with that of the C-LED, respectively. Moreover, the LEE enhancement factor of μ -LED array is greater at higher injected current levels. These results indicate that the μ -LED array can efficiently improve the LEE of the DUV LEDs.

To further reveal the underlying mechanism of the optical performance enhancement for the DUV μ -LED array, we further use FDTD simulation to analyze the LEEs for C-LED and the μ -LED arrays. In the simulation, a single dipole that served as the radiation source for the LED is located in the middle of the MQW layer^[31]. Moreover, the perfectly matched layers (PMLs) are set around the LED, which can completely absorb the light escape from the simulation region. A power monitor is placed at 500 nm away from the bottom of the AlN layer to collect the photons that escape from the DUV LED. It is worth noting that we only set a single dipole in the MQW layer as the radiation source. Considering the possible co-existence of TM- and TE-polarized light, both LEEs of the TM- and the TE-polarized light with different mesa sizes are cal-

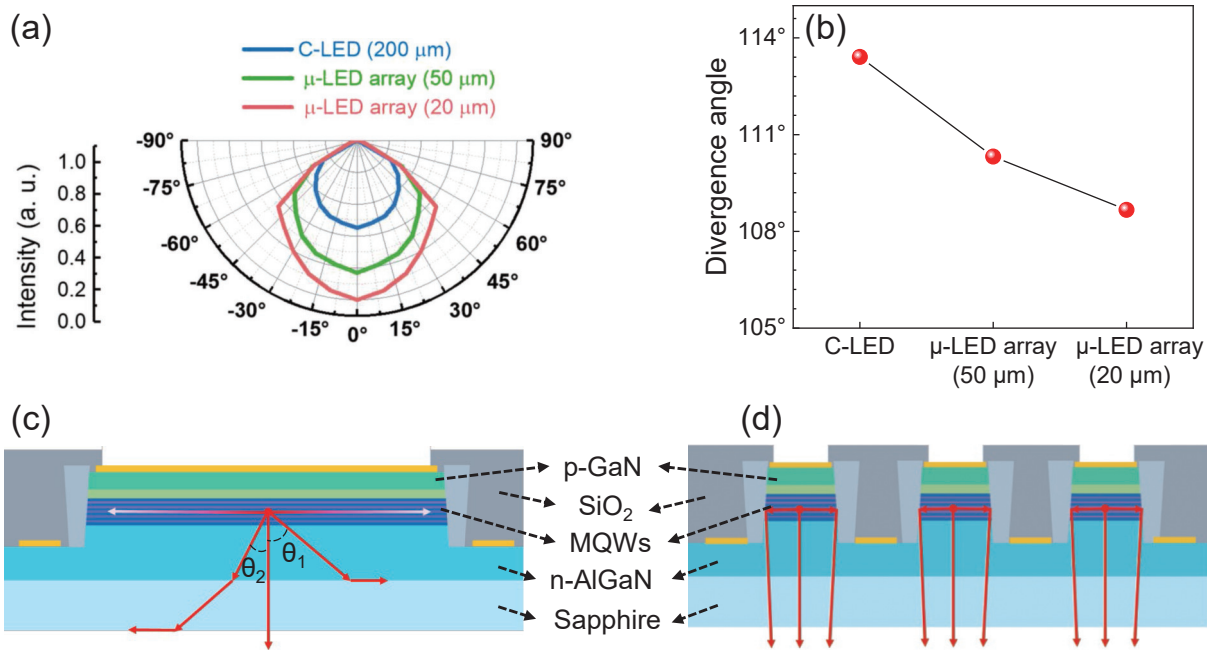


Fig. 5. (Color online) (a) Far-field patterns for the C-LED, the μ -LED array (50 μm), and the μ -LED array (20 μm) at 100 mA. (b) The divergence angle of the far-field patterns. The schematic illustrations of light propagation characteristics in (c) the C-LED and (d) the μ -LED array.

culated. We also performed the LEE calculation by changing the position of the dipole source within the device.

As an example, the electric field distributions for the DUV μ -LED (20 μm) are shown in Figs. 4(a) and 4(b). It can be observed that more DUV photons have been reflected on the sapphire side as the dipole source moves to the edge of the inclined sidewall. Furthermore, as shown in Figs. 4(c) and 4(d), it can be found that the LEEs of TM- and TE-polarized light increase as the dipole source moves to the mesa edge. Hence, we may conclude that the enhanced LEE of the μ -LED is mainly benefitting from an enlarged ration of the sidewall area to the emission area. The smaller the device is, the larger the ratio becomes, which promotes higher LEE eventually.

Additionally, we also recorded the far-field radiation pattern of the C-LED, the μ -LED array (50 μm), and the μ -LED array (20 μm) at the injection current of 100 mA, which are presented in Fig. 5(a). A significantly stronger extracted light intensity was observed for the array over the entire angular radiation range compared with that of the C-LED. The μ -LED array (20 μm) shows the highest light intensity. The spatial light intensities of all three samples reached to the maximum values at the emission angle of 0° when the devices were working at 100 mA. In Fig. 5(b), the divergence angle of the far-field patterns, extracted from Fig. 5(a), are 113.4°, 110.3°, and 108.7°, for the C-LED, the μ -LED array (50 μm), and the μ -LED array (20 μm), respectively. To better explain the phenomenon, schematic illustrations of light propagation characteristic in the C-LED and the μ -LED array are exhibited in Figs. 5(c) and 5(d). In the C-LED, the severe TIR would block the downward-traveling DUV photons inside the device; meanwhile, the lateral-traveling DUV photons would be re-absorbed with a travel distance of $\sim 15 \mu\text{m}$ ^[27]. In contrast, the μ -LED array not only can shorten the lateral propagation distance of photons, thus reducing the chance to be re-absorbed but also can increase the chance to be reflected downwards by the inclined sidewall. Therefore, the μ -LED array exhibits a

higher light intensity with a smaller divergence angle (light propagation is more forward directionality).

4. Conclusion

In summary, we have performed a systematic investigation on the electrical and optical performance of the DUV μ -LED array. Compared with the C-LED, the DUV μ -LED array (20 μm) shows a larger LOP by 52% at 100 mA with a higher peak EQE by 22% and a narrower divergence angle. Moreover, through the numerical analysis, it has been verified that the enlarged LEE for the μ -LED array is attributed to an enhanced light reflection at the sidewall along with the shortened lateral propagation distance of photons. Hence, the DUV μ -LED array with a smaller pixel size should exhibit better optical performance owing to the higher LEE. With an even smaller size (for example, 10 μm), a much higher LEE could be expected. Also, the light propagates with better directionality in the μ -LED array. These observations offer a comprehensive understanding of the optical behavior in the μ -LED array, which can help the community to build high-efficiency and high-power DUV LEDs for various applications.

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