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Humidity sensing properties of spray deposited Fe doped ${\rm TiO}_2$ thin film

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Abstract: In the present work, ferrite (Fe) doped TiO₂ thin films with different volume percentage (vol%) were synthesized using a spray pyrolysis technique. The effect of Fe doping on structural properties such as crystallite size, texture coefficient, microstrain, dislocation densities etc. were evaluated from the X ray diffratometry (XRD) data. XRD data revealed a polycrystalline anatase TiO₂ phase for sample synthesized up to 2 vol% and mixed anatase and rutile crystalline phase for sample synthesized at 4 vol% Fe doped TiO₂. The crystalline size was observed to decrease with increase in Fe dopant vol% and also other structural parameters changes with Fe dopant percentage. In the present work, electrical resistance was observed to decrease with a rise in Fe dopant vol% and temperature of the sample. Thermal properties like temperature coefficient of resistance and activation energy also showed strong correlation with Fe dopant vol%. Humidity sensing properties of the synthesized sample altered with a change in Fe dopant vol%. In the present paper, maximum sensitivity of about 88.7% for the sample synthesized with 2 vol% Fe doped TiO₂ and also the lowest response and recovery time of about 52 and 3 s were reported for the sample.

Key words: Fe doped TiO₂; thin films; spray pyrolysis; humidity sensing

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1. Introduction

Titanium dioxide (TiO₂) is a versatile semiconducting metal oxide, which is extensively studied in nanoparticles and thin film form and found applications in various fields of science and technology. The notable properties of TiO₂ include high dielectric constant^[1], high refractive index and wide band gap^[2] etc. TiO₂ films have been effectively used in the preparation of solar cell^[3] and sensors for environmental pollutant gas detection^[4, 5], purification of environmental pollutants^[6] etc. with transition metal atom or their oxides as dopants into TiO₂, which can tune its properties^[7, 8].

Along with the interesting properties, ease of synthesis – including various physical and chemical methods – is also one of the significant factors responsible for the extensive studies on TiO_2 material. The chemical methods require less instrumentation and are commonly employed to synthesize the pure, metal and their oxide-doped TiO_2 thin films. Various chemical methods were employed for the synthesis of pristine and doped TiO_2 thin films out of these; spray pyrolysis is one of the simplified and economic techniques for the thin film deposition over a larger surface area. The metal oxide thin films were successfully deposited onto the substrate for using a modified spray pyrolysis technique, because of its versatile features like easy handling, multi-composite film deposition, and economic route. In the spray technique, films

Correspondence to: D L Gapale, gapaledeepak@gmail.com Received 13 MARCH 2021; Revised 18 JULY 2021. ©2021 Chinese Institute of Electronics were deposited by forming fine droplets of precursor solution and then driving them towards the hot substrate. The quality of film is governed by the air to precursor solution ratio, substrate temperature and the distance between spray nebulizer and substrate etc. The details about the spray system were well discussed in previous reports^[9, 10].

Transient metal ions or their oxides are commonly used dopants into TiO₂. The transient metal ions can significantly change crystalline structure, size and shape of the nanomaterial, surface morphology, optical band gap, surface to volume ratio etc. In literature, various reports show that properties like enhanced charge carrier separation^[11], reduction in band gap^[12–14], change in surface oxygen vacancies^[12], structural (anatase to rutile phase transition)^[15] due to metal dopants. Dopants like Mn, Fe and Ni^[14] have shown mixed phases in the compound whereas the transient metal dopants like Cu, Cd, V, Cr, Zn, Co, etc. were observed to stimulate the phase transformation from the anatase to rutile phase^[16].

Ferrous (Fe) can be a good dopant to tailor the properties of TiO₂ as the ionic radius of Fe³⁺ (0.64 Å) is very close to that of Ti⁴⁺ (0.68 Å), which makes the doping easy. Further, the doping of the ferrous (band gap is 2.4 eV) introduces an intermediate band gap state which then reduces the optical band gap of the TiO₂ films^[16].

The structural properties of host material like crystallite size, crystal structure dislocation as well as microstrain found to be altered by varying Fe dopant concentration. Fe dopant can also change electronic structure and enhance the photocatalytic activity as well as sensing properties of the parent titanium dioxide^[17].

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The design and development of the humidity sensor is one of the recent areas of research due to their wide range of applications in industrial processing, semiconductor and automobile industries, environment monitoring and control etc.^[18]. Over the past decade, the focus has been given on building sophisticated humidity sensors which work on wide range of relative humidity and temperature.

The TiO₂-based humidity sensor is a resistance-based semiconductor-type humidity sensor. In literature, various reports are available on pristine, doped and composite TiO₂ materials. Jyothilal *et al.* reported high sensitivity for TiO₂ nano-array synthesized using an electron beam-assisted physical evaporation technique with very low response and recovery time^[19]. Li *et al.* reported high sensitivity and low response time (24 s) for mesoporous Co-doped TiO₂ material^[20]. Zhang *et al.*^[21] reported high sensitivity with less response time (3.1 s) and large recovery time (76 s) for wet chemical synthesized TiO₂/SrTiO₃ composite material.

With this context, the present paper discusses the effect of Fe dopant concentration on structural, morphological and electrical properties and their correlation with humidity sensing performance.

2. Experimental

Fe-doped TiO₂ film samples were successfully deposited on glass substrates with various Fe dopant vol% by a spray pyrolysis technique. Analytical grade titanium tri-chloride (TiCl₃; Sigma Aldrich) and ferrous chloride tetra-hydrate (FeCl₂.4H₂O; Sigma Aldrich) were used as precursors. The concentration of both the precursor solutions was adjusted to 0.1 M to control the atomic weight percentage of the species (Ti and Fe). The two precursor solutions were mixed vigorously using a magnetic stirrer at room temperature with different vol% to maintain the fixed atomic weight percentage. Other spray parameters such as deposition temperature (350 °C), distance between spray gun to substrate (30 cm), solution flow rate (1 ml per minute), carrier air flow rate (7.5 lpm) etc. were kept constant during the deposition. After the deposition, samples were annealing at a temperature of 500 °C for 2 h in an air atmosphere.

The structural properties of the prepared films were studied by X ray diffractometry (XRD) using a BRUKER D8 AD-VANCE diffractometer. The microstructural properties were studied using scanning electron microscopy (SEM) with a JEOL-540LV microscope. The electrical and humidity sensing characterization was done by an in-situ set up designed for resistance measurement. To study humidity sensing properties, film resistances were measured as a function of change in relative humidity. A humidity meter (MEXTECH, model no. M288CTHW) was used to record relative change in humidity.

3. Results and discussion

3.1. XRD analysis

Fig. 1 presents XRD patterns for the pure and Fe³⁺ doped TiO₂ samples with different Fe dopant 1 vol%; annealed at a temperature of 500 °C. XRD pattern of pristine TiO₂ shows peaks corresponding to crystalline planes (101), (004), (200), (105), (211), (204) and (116), of anatase TiO₂ tetragonal phase. From Fig. 1. it is observed that the intensity of the diffraction peaks decreases with Fe³⁺ dopant 1 vol%. Also, the increase



Fig. 1. XRD patterns for pristine and Fe-doped TiO_2 thin films annealed at 500 °C (# rutile).

in peak broadening indicates the reduction in crystallite size with augmented Fe³⁺ doping. The deposited samples showed a polycrystalline nature with the anatase TiO₂ crystalline phase for pristine, 1 vol% and 2 vol% Fe³⁺ doped TiO₂ samples while the 4 vol% doping sample shows mixed anatase and rutile phase. No other impurity phases observed into the crystalline material, which confirmed that Fe³⁺ ions are successfully amalgamated into the TiO₂ lattice structure without the formation of iron oxide on the TiO₂ surface^[22]. This is because Fe³⁺ ion has an ionic radius (0.64 Å) comparable to Ti⁴⁺ (0.68 Å) and can also form octahedral coordination similar to Ti^{4+[23, 24]}.

The measured parameters like texture coefficient, microstrain, dislocation densities and specific surface area have been added in Table 1. Structural parameters such as texture coefficient, crystallite size, microstrain, specific surface area and dislocation density were calculated using appropriate formulae as discussed in an earlier report^[25].

The texture coefficient, micro strain, dislocation densities and specific surface area are respectively given by

Texture coefficient:

$$T_{\rm c}(hkl) = \frac{\frac{I(hkl)}{I_0(hkl)}}{\frac{1}{N} \frac{\sum I(hkl)}{I_0(hkl)}},$$
(1)

....

where $T_c(hkl)$ is the texture coefficient of the (hkl) plane, l(hkl) is the measured intensity from the (hkl) plane, $l_0(hkl)$ is the JCP-DS standard intensity of the (hkl) plane, and N is the number of diffraction peaks.

Microstrain:

$$\varepsilon = \frac{\Delta d}{d_0} = \frac{d - d_0}{d_0},\tag{2}$$

where d_0 is the interplanar distance of bulk material (TiO₂

Sample	Fe (vol%)	Crystallite size (nm)	Interplaner distance (Å)	Crystal phase	Texture coefficient	Microstain (10 ⁻³)	Dislocation (10 ¹⁴ cm ⁻²)	Specific surface area (m ² /g)
Pristine	-	31.21260	3.513233	A	1.5622	1.764	10.2646	49.416
1 vol% Fe:TiO ₂	1	28.25648	3.514076	А	1.4996	1.87	12.5246	54.586
2 vol% Fe:TiO ₂	2	25.07873	3.511046	А	1.0788	1.90	15.8997	61.502
4 vol% Fe:TiO ₂	4	24.69604	3.510535	A - 90.77 % R - 9.23 %	0.4755	2.48	16.3963	62.456

Table 1. Structural properties of pristine and Fe-doped TiO₂ thin films.



Fig. 2. SEM image for (a) pristine TiO₂, (b) 1 vol% Fe:TiO₂, (c) 2 vol% Fe:TiO₂ and (d) 4 vol% Fe:TiO₂ samples.

 d_0 = 3.520 Å), *d* is the experimentally predicted interplanar distance.

Dislocation density:

$$\delta = \frac{n}{D^2},\tag{3}$$

where *n* is a proportionality factor, for minimum dislocation density n = 1 and *D* is the crystallite size.

Specific surface area

$$5_{\mathsf{A}} = \frac{6 \times 10^3}{D\rho},\tag{4}$$

where S_A is the specific surface area, D is the crystallite size (spherical shaped), and ρ is the density of TiO₂ (anatase phase 3.890 g/cm³).

Properties of the thin film materials are strongly affected by a preferred crystallographic orientation or texture. The properties like crystal structure, crystal morphology and intensity of the diffraction peak can be ascribed to the presence of texture into film materials, thus it is essential to evaluate quantitative effect of the texture on the properties of material to optimize its applications. The value of the texture coefficient was calculated for the predominant crystalline plane, (101). Texture coefficient value that differs from unity indicates preferential orientation and if it is greater than unity, it indicates preferentially grown facets. Texture coefficient for pure TiO₂ sample is greater than that for Fe-doped TiO₂ as presented in Table 1. Reduction in preferential orientation was observed with an increase in Fe³⁺ dopant vol%. The fall in the texture coefficient (T_c) for the (101) plane indicates a reduction in the crystalline quality^[26]. The average crystallite sizes were calculated from the Scherrer's equation and the observed values of the crystallite size for pure and Fe-doped TiO₂ are tabulated in Table 1. The additional peak at $2q = 36.11^{\circ}$ corresponding to the crystalline plane (101) of rutile TiO₂ tetragonal phase was observed for 4 vol % Fe-doped TiO₂. The weight percentage of the anatase phase was observed to decrease 4 vol% Fe-doped TiO₂, which can be ascribed to non-considerable changes in crystallite size and dislocation densities of a film. Thus, average crystallite size for the Fe³⁺ doped TiO₂ thin films was observed to decrease with Fe³⁺ dopant concentrations and the fall in crystallite size is due to the Fe³⁺ ions, which can alter surface charge of TiO₂ material^[27].

Microstrain in the pristine and Fe³⁺ doped TiO₂ samples was calculated and was observed to increase with an increase in Fe³⁺ dopant vol%. Similarly, dislocation density and specific surface area of pristine and Fe³⁺ doped TiO₂ films were found to increase with increase in the amount of Fe³⁺, which indicates an increase in crystal lattice defects^[28]. The increase in microstrain can sizably reduce the crystallite size and enhance surface area of the films. The increase in specific surface area can then improve the surface activity of the Fe-doped TiO₂ thin film^[29, 30]. Improvement in surface activity of synthesis materials can affect the photocatalytic as well as sensing properties of the material.

3.2. Microstructural analysis

The SEM micrographs of the spray-synthesized pristine and Fe-doped TiO_2 samples are presented in Fig. 2, which show the samples exhibit interconnected webs like morphology and the particles are attached to the interconnected



Fig. 3. EDX spectrum of (a) pristine TiO₂, (b) 1 vol% Fe:TiO₂, (c) 2 vol% Fe:TiO₂ and (d) 4 vol% Fe:TiO₂ samples.

_		-	-		
	Sample	Fe (vol%)	Oxygen (at%)	Titanium (at%)	Fe (at%)
	Pristine	-	81.08	18.92	_
	1 vol%	1	84.61	14.23	1.16
	Fe:TiO ₂				
	2 vol%	2	86.14	12.29	1.57
	Fe:TiO ₂				

11.12

1.80

87.28

Table 2. EDX spectrum for pristine and Fe-doped TiO₂ thin films.

webs. Patil et al.[31] have reported similar web-like morphology for pristine TiO₂ films synthesized by the spray pyrolysis method. It is observed that the average web diameter changes with Fe dopant vol%. In the case of 1 vol% to 4 vol% Fe-doped samples, the agglomerated particles were observed to break into a flower-like structure, which enhances the surface area of these samples. The increase in surface area can improve the surface activity of the materials. With a further increase in Fe dopant vol%, some large-sized micro cracks were observed on the surface of synthesized film, as presented in Figs. 2(c) and 2(d). These cracks also enhance the surface area but their size is also important as it affects the sensing performance of the material. Micro pores were also found to be present on the surface of the film samples and their average size was observed to change with Fe³⁺ content. Micro pores are highlighted by using a red arrow while the micro cracks on the samples are highlighted using a yellow arrow. Pores whose surface end open or closed have their own significance for the sensing and photocatalytic applications. Surfaces with an open end have an advantage due to the enhancement in surface area and can improve the sensing performance^[32].

3.3. Elemental analysis

4 vol%

Fe:TiO

The elemental analysis for pristine and Fe^{3+} doped TiO_2 thin films was carried out using energy dispersive spectroscopy (EDX) method. The EDX spectra for pure and Fe^{3+} doped TiO_2 thin films with various Fe^{3+} concentrations are presented in Figs. 3(a)–3(d) and Table 2. These spectra show the peaks of Ti (energy ~ 4.5 keV), O (energy ~ 0.525 keV), Fe (energy ~ 6.398 keV) and Si (energy ~ 1.739 keV) without any other impurities. This confirms that the synthesized samples consist of Ti, Fe, and O elements present in Fe³⁺ doped TiO₂ thin films. The peak that corresponds to the Si element present in the EDX spectrum is due to the use of silica substrate for the thin film deposition.

3.4. Electrical properties

The electrical resistance of pristine and Fe doped TiO₂ films were found to decrease with increase in Fe³⁺ vol%. The resistance of 4 vol% Fe doped TiO₂ sample is more than that of the other samples due to the presence of micro crack on the sample and breakdown of agglomerated particles, which leads to the increase in its resistance. With the increase in temperature, the electric resistance of the samples increases initially (up to 120 °C) and then decreases with a further increase in temperature. Such an increase in resistance at a lower temperature range indicates the humid condition in the atmosphere. With an increase in temperature at a lower range, moisture absorbed by the samples decrease and the resistance of the film samples increases. This shows that the synthesized material has good humidity sensing properties. With a further increase in temperature, resistance of the film samples decrease. The exponential decrease in the resistance indicates semiconducting nature of the samples. It is reported in the literature when, for Fe-doped TiO₂ samples, there is a transition of n-type to p-type electrical conductivity. Also, at elevated temperatures, pristine TiO₂ exhibits ntype conductivity but the iron-doped TiO₂ materials present p-type electrical conductivity^[33]. Therefore, the majority charge carriers are electrons for pristine TiO₂ at higher temperature whereas they are holes for Fe-doped TiO₂. It is reported in the literature that for Fe-doped TiO₂ samples, Fe atoms replace Ti atoms in the oxide lattice and Fe atoms with acceptor impurities due to iron doping creates oxygen vacancies in the samples, such as oxygen vacancies and titanium interstitials serve as aggregation sites that result in increased p-type



Fig. 4. (Color online) Variation of resistance with temperature for (a) pristine TiO_2 , (b) 1 vol% Fe:TiO_2, (c) 2 vol% Fe:TiO_2 and (d) 4 vol% Fe:TiO_2 samples.



Fig. 5. (Color online) Variation of $log(R_a)$ with temperature to calculated TCR for (a) pristine TiO₂, (b) 1 vol% Fe:TiO₂, (c) 2 vol% Fe:TiO₂ and (d) 4 vol% Fe:TiO₂ samples.

conductivity. Here, with the increase in temperature, charge carriers get released within the material, which decrease the resistance of the materials. The temperature-dependent electrical resistance or resistivity can be considered in terms of temperature coefficient of resistance (TCR) and activation energy (E_a) . The Fe-doped TiO₂ materials are semiconducting materials with a negative temperature coefficient of resistance (NTC), which can be used as temperature sensors. The resistance (R_a) vs temperature (7) plot represents calibration curves for pristine and Fe-doped TiO₂ thermal sensor as shown in Fig. 4. TCR for the synthesized samples were calculated from the plot of $log(R_a)$ vs temperature (7) curve^[5] as shown in Fig. 5, the slope of the curve represents the value of TCR. These plots infer that TCR for the Fe-doped TiO₂ films are greater than that for the pristine TiO₂ samples. The TCR for Fe³⁺ doped sample was observed to increase from -0.0014 to -0.00034 $^{\circ}C^{-1}$ with Fe³⁺ dopant vol% as shown in Table 3.

Activation energy for the synthesized samples was calculated using Arrhenius plots of the synthesized samples as shown in Fig. 6. At lower temperatures, Mott variable range hopping (VRH) mechanism is observed in semiconducting nano-materials while at a higher temperature the Arrhenius mechanism dominates. Calculated activation energy was observed to increase from 0.3395 to 0.5201 eV for the heating cycle with increase in Fe^{3+} dopant vol% as tabulated in Table 3. The increase in activation energy at a higher temperature can be explained on the basis of activation of the working level due to iron doping into TiO_2 . During the cooling cycle, activation energy was observed to be higher than that during the heating cycle. The increase in activation energy during the cooling cycle is attributed to irreversible oxidation processes. With the increase in Fe concentration, the oxidation vacancies increases in the sample. Now, during the heating cycle the entropy of the sample increases with temperature. While during the cooling cycle, the entropy decreases with temperature; in this case the reactant species (may be from atmosphere) join with the sample surface to form over transection states along the interaction, such as transection states of the reactants leads to an increase in activation energy.

3.5. Humidity sensing properties

Humidity sensing performance of the Fe^{3+} doped TiO_2 samples synthesized at different Fe dopant concentrations were studied by measuring the change in resistance with corresponding change in relative humidity to determine sensitivity and as a function of time for a fixed humid condition; to determine response and recovery time of the sensor material. The resistance of Fe³⁺ doped TiO₂ samples was observed to decrease with the change in percentage of the relative humidity as presented in Fig. 7 and shows a nonlinear trend. A higher rate of change of sample resistance with a change in percentage of relative humidity was high at lower humidity and was low at higher relative humidity. Thus, the variation of resistance with a percentage of relative humidity is exponential in nature. Such an exponential nature of resistance with relative humidity may be due to the formation of the chemisorbed and physisorbed layers on the surface of the film samples in humid conditions. The concentration of surface charge carriers is an important factor that can affect the amount of absorbed water vapour on the surface of the samples^[34, 35] and can be tuned by varying concentration of dopants in the pristine TiO₂. The conduction mechanism in chemisorbed and first physisorbed layer can be ascribed to the tunnelling of electrons, while the conduction at the second physiosorbed layer is protonic conduction or the Grotthuss conduction mechanism^[36]. The second physiosorbed layer is always in equilibrium with the atmospheric humidity.

Sensitivity of a sensor can be defined as the ratio of difference in the resistance between dry and humid conditions to the resistance at dry conditions^[37]. Sensitivity of the sensor is expressed in terms of the percentage of sensitivity. For the samples under investigation, change in sensitivity with the corresponding change in percentage of relative humidity is shown in Fig. 8. Sensitivity of pristine and Fe-doped TiO₂ thin films increases rapidly at lower relative humidity which then saturates above 90% relative humidity. The saturation of sensitivity at higher relative humidity confirms the formation of a second physiosorbed layer, which indicates that the conduction process is due to photon transport between water molecules.

Reproducibility of sensor performance was studied by repeating the measurements at different periods of time and the results are presented in Fig. 9, which shows that the sensitivity of the sensor decreases as the time goes on.

Hysteresis is defined as the lag of the resistance/sensitiv-

Table 3. Electrical resistance, TCR and activation energy for pristine and Fe-doped TiO₂ thin films.

Sampla	Fe (vol%)	Room temp. resistance (M Ω)	TCR (°C ⁻¹)		Activation energy (eV)	
Sample			Heating	Cooling	Heating	Cooling
Pristine	_	382.4800	-0.00140	-0.007393	0.3395	0.3537
1 vol% Fe:TiO ₂	1	384.7108	-0.00124	-0.005736	0.4499	0.4673
2 vol% Fe:TiO ₂	2	258.5140	-0.00081	-0.001172	0.4947	0.5137
4 vol% Fe:TiO ₂	4	212.2913	-0.00034	-0.000738	0.5201	0.5348



Fig. 6. (Color online) Variation of $log(R_a)$ with 1000/T to calculate activation energy for (a) pristine TiO₂, (b) 1 vol% Fe:TiO₂, (c) 2 vol% Fe:TiO₂ and (d) 4 vol% Fe:TiO₂ samples.



Fig. 7. (Color online) Variation of resistance with percentage of relative humidity for (a) pristine TiO_2 , (b) 1 vol% Fe:TiO_2, (c) 2 vol% Fe:TiO_2 and (d) 4 vol% Fe:TiO_2 samples.



Fig. 8. (Color online) Variation of sensitivity with percentage of relative humidity for (a) pristine TiO_2 , (b) 1 vol% Fe:TiO_2, (c) 2 vol% Fe:TiO_2 and (d) 4 vol% Fe:TiO_2 samples.



Fig. 9. (Color online) Variation of sensitivity with percentage of relative humidity for different time interval for 2 vol% Fe :TiO₂ sample.

ity during the dehumidification process or it is the difference between resistance/sensitivity with respect to the humidification and dehumidification process. A sensor must have low hysteresis loss, which is correlated to the stability and reliability of the sensor material.

Hysteresis loss can be expressed in terms of percentage of hysteresis which can be calculated using the relation^[38]

% of hysteresis =
$$\left[\frac{R_{\text{dehumid}} - R_{\text{humid}}}{R_{\text{max}} - R_{\text{min}}}\right] \times 100\%$$
, (5)

where $R_{dehumid}$ is resistance at mean value of percent relative humidity (PRH) of the sample during dehumidification, $R_{dehumid}$ is resistance at mean value of PRH of the sample during humidification, R_{max} is the resistance at maximum PRH and R_{min} is the resistance at minimum PRH.

In the present study, it was observed that the percentage of hysteresis loss for the pristine sample is less, as compared to Fe doped samples; also it was found that the hysteresis loss increases with Fe doping as shown in Fig. 10. However, as the loss for all the samples is below 5%, which is too low as presented in Table 4, it suggests high stability and reliability of the synthesized samples as the humidity sensor which was confirmed by repeating the observations as well as by taking observations within a prescribed period of time.

The response time of a sensor is the time required to achieve 90% of the total resistance change for humidification/adsorption process while the recovery time is time required to achieve 90% of the total resistance change for the dehumidification/desorption process. Fig. 11 shows variations of change in resistance with corresponding change in time which presents response and recovery time for the pure and Fe-doped TiO₂ samples. The response time was found to change with a change in Fe dopant level. The minimum response time of 52 s was obtained for the 2 vol% of Fe-doped

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Fig. 10. (Color online) Hysteresis loops for for (a) pristine TiO₂, (b) 1 vol% Fe:TiO₂, (c) 2 vol% Fe:TiO₂ and (d) 4 vol% Fe:TiO₂ samples.

Table 4. Sensitivity, response, recovery time and % of hysteresis loss for pristine and Fe-doped TiO_2 thin films.

Sample	Fe (vol%)	Sensitivity	Response time (s)	Recovery time (s)	% of hysteresis loss
Pristine	-	83.72	77.5	3	1.19
1 vol%	1	86.71	62.5	3	3.11
Fe:TiO ₂					
2 vol%	2	88.68	52	3	3.66
Fe:TiO ₂					
4 vol%	4	80.47	82.5	4	5.34
Fe:TiO ₂					



Fig. 11. (Color online) Variation of resistance with time to calculate response and recovery time for pristine TiO_2 , 1 vol% Fe: TiO_2 , 2 vol% Fe: TiO_2 and 4 vol% Fe: TiO_2 samples.

 TiO_2 sample and with a further increase in Fe doping, the response time was found to increase. The recovery time observed for all the samples were very small; around 3 s as shown in Table 4.

The morphology of the sensing material plays an important role, which is ascribed to the amount of water vapour adsorbed and desorbed on its surface. The presence of the pore and its distribution over the surface of the sample considerably affects the sensitivity of the sample. During humidification, water vapours on the surface of the sensing sample shows a strong correlation with the pore size and its distribution. The open or closed pore surface has its own contribution in humidity sensitivity. Open pores have the advantage of capillary conduction mechanism, which can enhance sensitivity of the material^[39]. Closed pores reduce the surface area which then reduces adsorption of water vapours and reducea the sensitivity of the sensing sample. The formation of chemisorbed and physisorbed layers can also get affected by pore size and their distribution on the surface of the sensing samples^[40, 41].

Thus, getting optimum size micro-pores is a notable success for better humidity sensing performance^[42]. At room temperature, the humidity sensing mechanism is of an ionic type^[43]. The presence of pores and their distribution can enhance surface area of sensing material. In the present study, it was observed that sensitivity of the Fe-doped TiO₂ samples increases with the increase in the Fe dopant level, which can be ascribed to the increase in charge carriers due to doping and presence of micro pores and micro cracks. The presence of micro pores and micro cracks significantly influences the

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sensing properties. Micro pores and micro cracks have the advantage of a capillary conduction mechanism, which can enhance sensitivity of the material due to the adoption of humid air (water molecules) on the inner surface of the micro pores and micro cracks to formed chemisorbed and the first physiosorbed layer of water molecules. The sensitivity of the 2 vol% Fe-doped TiO₂ sample is high due to electron-tunnelling between donor water site and surface charge carriers, which was observed in the chemisorption layer of water molecules. The highest sensitivity of 89.06% was recorded for the 2 vol% Fe-doped TiO₂ sample. Further, the increase in Fe dopants to 4 vol%, could elevate the charge concentration as well as surface acceptor sites, facilitating the enhancement in sensitivity, but as can be seen from the morphology micrographs, at this dopant concentration (4 vol%), the dense film shows some cracks which can be held responsible to a reduction in sensitivity of the sample. The formation of the second physical adsorbed layer inside the large-sized micro cracks and breakdown agglomerated particles influences the protonic conduction in the 4 vol% Fe-doped TiO₂ sample, which reduces its sensitivity^[35, 25].

Chemisorption is an adsorption due to the chemical reaction between the surface species and the adsorbates, while the physisorption adsorption is due to van der Waals forces between chemisorbed layer and the adsorbates. The chemisorbed water molecules exerted an electrostatic field, which not only attracted water molecules but also reduced the strength of oxygen to hydrogen bonds of the physiosorbed water molecules. The electric potential present in chemisorbed water molecule is a source of resistance change, depending upon chemisorbed water molecules and its reaction with surface site adsorption altering the resistance of the samples. The chemical reactions in chemisorbed and physiosorbed water molecules are as follows:

$$\begin{split} H_2 O &+ O^- + 2 M^+ \rightarrow 2 \left(M^+ - O H^- \right) + e^- \\ & (\text{chemisorbed layer}) \,, \\ M^+ + H_2 O &\rightarrow M - O H \ + H^+ \left(\text{physisorbed layer} \right) \,, \end{split}$$

where M is Ti or Fe atoms species.

The sensitivity of the sensing material strongly depends on its surface charge species and the silica substrate does not affect the performance. The very large potential difference between adsorbed water molecules charges present inside the sample material and the substrate inhibits any conduction between them. Si is on the interface between the glass substrate and the samples; therefore, it could not influence the sensitivity of the samples. The elemental analysis of the sample showed the existence of Si from the glass substrate and not from the samples; therefore, the bare substrate does not exhibit any humidity sensing properties.

The complete results of the humidity sensitivity and response time of the sample varies with the Fe vol% were presented in Fig. 12. Which clearly indicates that the optimized Fe dopant vol% for better humidity sensing performance is 2 vol%.

With the increase in the amount of Fe, the structural parameters such as micro-stress, dislocation densities, specific surface area get advanced, which can be used to tailor the sensitivity accordingly.



Fig. 12. (Color online) Variation sensitivity and response time with different Fe vol% for Fe doped TiO₂ thin films.

4. Conclusions

Pristine and Fe-doped TiO₂ thin films were successfully synthesized by a spray pyrolysis technique on a glass substrate with Fe dopant vol%. The effects of the Fe dopant vol% on structural, electrical and humidity sensing properties of TiO₂ were successfully studied using appropriate methods. The structural properties like crystallite size, texture coefficient, micro-strain, dislocation density and specific surface area were estimated from XRD data. The XRD study shows that the crystallite size decreases with an increase in Fe doping percentage. The XRD profile also shows a small shift and reduction in the intensity of the characteristic (101) plane with doping. The mixed anatase and rutile crystalline TiO₂ phase were observed for the sample synthesized at 4 vol% Fe, while the other samples synthesized up 2 vol% showed a polycrystalline anatase tetragonal phase. The electrical resistance was observed to decline with a rise in dopant percentage. The temperature coefficient of resistance (TCR) and activation energy were also found to increase with the increase in Fe dopant percentage. Humidity sensing properties of the samples were also affected by the Fe dopant percentage and it was found that the sensitivity increases with Fe dopant vol% and was found to be maximum at 2 vol% doping of Fe. The minimum response time was observed to be 52 s for sample synthesized with 2 vol% of Fe.

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