

Low-cost photoacoustic imaging systems based on laser diode and light-emitting diode excitation

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Photoacoustic imaging, an emerging biomedical imaging modality, holds great promise for preclinical and clinical researches. It combines the high optical contrast and high ultrasound resolution by converting laser excitation into ultrasonic emission. In order to generate photoacoustic signal efficiently, bulky Q-switched solid-state laser systems are most commonly used as excitation sources and hence limit its commercialization. As an alternative, the miniaturized semiconductor laser system has the advantages of being inexpensive, compact, and robust, which makes a significant effect on production-forming design. It is also desirable to obtain a wavelength in a wide range from visible to near-infrared spectrum for multispectral applications. Focussing on practical aspect, this paper reviews the state-of-the-art developments of low-cost photoacoustic system with laser diode and light-emitting diode excitation source and highlights a few representative installations in the past decade.

Keywords: Photoacoustic imaging; photoacoustic tomography; photoacoustic microscopy; laser diode; light-emitting diode.

1. Introduction

In 1880, Alexander Graham Bell¹ discovered and put forward the photoacoustic effect in solids for the first time. Due to converting absorbed optical energy into a temperature rise, a corresponding pressure change will generate an acoustic signal that can be detected by the ultrasonic receiver, then a highresolution image of optical absorption differences can be reconstructed to reveal the internal structure and function; this is the so-called photoacoustic imaging (PAI).^{2–5} In general, PAI has three major types: photoacoustic tomography or photoacoustic computed tomography (PAT/PACT), photoacoustic microscopy (PAM), and photoacoustic endoscopy (PAE).^{6–19} In PAT, an expanded pulsed laser beam illuminates the imaging area homogeneously.^{20–28} The laser-induced photoacoustic signal can be acquired using either singleelement scanning or multi-element array detection, which determines the imaging speed and image quality with various time-reversal reconstruction algorithms.

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Unlike PAT, PAM can be divided into acoustic-resolution PAM (AR-PAM) and optical-resolution PAM (OR-PAM), depending on whether the acoustic focus or optical focus is more tightly focussed.^{29–35} The spatial resolution and sensitivity of the imaging systems depend on the laser excitation and acoustic detection configurations. Like PAM, PAE is emerging as a novel technology for imaging internal organs with longer depth.^{36–41} The small photoacoustic endoscopic probe usually includes the function units of laser delivery, acoustic sensing, and mechanical scanning, which could be positioned close enough to the area of interest. Presently, the relatively slow imaging speed is limited by the mechanical rotational scanning for a crosssectional B-scan image.

Normally, the laser pulse duration is needed to be less than both the thermal and stress confinement times, such as nanosecond and femtosecond laser. For decades, PAI has developed a great extent as the development of the laser technology and optimization of the system structure.^{42–63} The PAI systems choose Q-switched Nd:YAG or OPO nanosecond lasers as excitation sources, which are usually expensive and bulky to be used as a handy tool for clinical applications.⁶⁴ As PAI is ceaselessly advancing in the wake of laser technologies, an alternative is to use the rising semiconductor lasers such as laser diodes and light-emitting diodes (LEDs). They have the competitive advantages of being inexpensive, compact, and robust. Furthermore, they commonly have high repetition rate and wide spectrum range for the real-time multispectral applications.⁶⁵ Currently, pulsed laser diodes are commercially available with a hundreds-watt-level power output at near-infrared (NIR) wavelengths, and continuous-wave (CW) LEDs can cover the full visible (VIS) spectrum.^{66–77} They could play a broad role in superficial vascular PAI, especially where the laser energy requirements are relatively modest. Although the relatively weak power represents a main disadvantage for efficient photoacoustic effect, there is still substantial scope to mitigate this for deeper imaging depth by time and frequency methods. In particular, the further promotion of PAE technology will make tremendous impact on the deeper imaging of internal organs. In this review, we focus on the current status and recent progress in PAI systems with the laser diode and LED excitations and highlight studies performed in the past decade.

2. Laser Diode-Based PAT (LD-PAT)

2.1. Pulsed LD-PAT

Ten years ago, a circular scanning-based LD-PAT system was developed, as shown in Fig. 1(a).^{78,79} It contained four 905 nm pulsed laser diodes, which can achieve 175 W peak output power, 0.1% duty cycle, and a pulse duration of 500 ns. Each of outputs was coupled to a fiber to irradiate the sample which has the same absorption coefficient with blood. The laser diodes with a pulse duration of 500 ns were used to excite the photoacoustic signals. A 3.5 MHz focussed transducer revolves around the sample to capture the signals with 100 steps by a stepper motor. The magnification of the amplifier is $40 \,\mathrm{dB}$ and the received signal was averaged 5000 times. Figure 1(b) shows the reconstructed image after deconvolving the photoacoustic data with the temporal shape of the pulse duration. The pulsed LD-PAT system achieved a two-dimensional image, which was demonstrated the potential to be used for short-range imaging applications such as visualizing



Fig. 1. (a) Cylindrical scanning LD-PAT system and (b) image obtained with a pulse duration of 500 ns (images adapted from Refs. 78, 79).



Fig. 2. In vivo imaging of rat brain in lateral plane at different scanning speeds: (a) 30 s, (b) 10 s, and (c) 3 s, superior sagittal sinus (SS); transverse sinus (TS) (images adapted from Ref. 80).

superficial vascular anatomy. It is considered that the work represents the first attempt in developing a new generation of compact and low-cost excitation system that provides an alternative to solidstate lasers. Before the two mentioned, Kolkman *et al.*⁵⁹ have shown an *in vivo* image by coupling the light of the pulsed lasers into a glass fiber. It took initial steps toward LD-based PAI, although the group did not show the configuration of system.

Another similar instrument of pulsed LD-PAT was applied to biomedical imaging in vivo. In this system, an 803 nm laser diode with pulse energy of 1.3 mJ and 7 kHz repetition rate was used as the excitation source.⁸⁰ Mice at 6 weeks have been selected for *in vivo* experiment, and the images of the rat brain were reconstructed by receiving photoacoustic signals in 30, 10, and 3 s periodic time. The resolution of the pulsed LD-PAT system is up to $380 \,\mu\mathrm{m}$ with a 2.25 MHz transducer. Figure 2 shows the relationship between the signal-to-noise ratios (SNRs) and scan time. The images of sagittal sinus and transverse sinuses are fairly distinct, and the SNR is low at high-speed imaging because of the low energy pulses. The pulsed LD-PAT system demonstrated that the pulsed laser diode could provide highspeed in vivo imaging for preclinical applications.

2.2. CW LD-PAT

A 784 nm intensity-modulated CW laser diode was used for PAT, as shown in Fig. 3(a).⁴³ The laser diode was modulated at 2.45 MHz with an output power of 120 mW and was coupled to a scanning head by an optical fiber. A 2.45 MHz bowl-shaped transducer was used to receive the photoacoustic signals. The reconstructed image of rabbit blood vessel was shown in Fig. 3(b). The photoacoustic signals have an SNR of 43 dB, and the system achieved an axial resolution of 0.45 mm and a lateral resolution of 1 mm. The CW LD-PAT system can provide the characteristic information of vasculature \sim 3 mm deep, but the single-frequency CW measurement misses the time domain information about the flight time of photoacoustic signal.

2.3. Dual-modality photoacoustic/ ultrasound system

Figures 4(a) and 4(b) show a clinical imaging system that was composed of ultrasound and PAI modality.⁸¹ A handheld probe is embedded with 805 nm laser diode arrays, which operated on a pulse energy of $0.56 \,\mathrm{mJ}$, repetition frequency of



Fig. 3. (a) Schematic of the CW LD-PAT system and (b) amplitude image of a rabbit ear vasculature (images adapted from Ref. 43).





Fig. 4. (a) Schematic of the handheld probe. US, ultrasound array transducer; P, deflecting prism; DOE, diffractive optical elements; DS, diode stack; MCL, micro-cylindrical lenses; CR, aluminum cooling rim. (b) External shape of the handheld probe, (c) photoacoustic/ultrasound image of a human proximal interphalangeal joint, and (d) ultrasound image of a human proximal interphalangeal joint (images adapted from Ref. 81).

10 kHz, and pulse duration of 130 ns. In addition, the probe combined the reflection mode photoacoustic and the single direction scan. A 7.5 MHz ultrasound array was employed with an acoustic lens to focus in the elevation plane at distance about 20 mm. Figures 4(c) and 4(d) show the ultrasound and photoacoustic images of the human proximal interphalangeal joint, showing a detailed absorption distribution alongside the anatomical structure. The pulsed LD-PAT system achieved an axial resolution of 0.28 mm, lateral resolution about 0.5 mm, and penetration depth up to 15 mm. It can obtain 10 images per second under the maximum imaging speed and each image was averaged 20 frames, which can provide a portable real-time dual-modality imaging for clinical applications. Recently, van den Berg et al.⁸² took further efforts toward commercial probes for preclinical detection of liver fibrosis. Both devices are combined in dual modality PA/US imaging, which enables robust noninvasive identification of the liver during experiments and accurate region-of-interest selection.

Laser Diode-Based PAM (LD-PAM) *Pulsed NIR LD-PAM*

A 905 nm pulsed laser diode operating on the OR-PAM model is shown in Fig. 5(a).^{83,84} The laser diode has 140 W peak power and pulse energy of $4.9 \,\mu$ J. The optical lens group with a numerical aperture of 0.62 has a focus length of 15 cm. The excitation source was composed of optical lenses and the laser diode, as shown in Fig. 5(b). A 4.53 MHz transducer was used to capture the photoacoustic signals by averaging 128 times. A dead ant with a length of $\sim 3.5 \,\mathrm{mm}$ and diameter of 0.7 mm was selected as the sample. Figures 5(c) and 5(d) show the two-dimensional reconstructed images which displayed characteristics of spatial shape and size. The pulsed NIR LD-PAM system demonstrated that the pulsed NIR laser diode can be employed for biological tissue imaging and may represent a potential development direction for superficial biomedical applications.

Another similar NIR LD-PAM system was used to image *ex vivo* mouse ear.⁸⁵ In this system, a pulsed



Fig. 5. (a) and (b) Photograph of pulsed NIR LD-PAM system and its laser diode excitation and (c) and (d) photoacoustic images of the ant along the depth and horizontal directions (images adapted from Refs. 83, 84).

laser diode with a wavelength of 905 nm and 130 W peak power was used as excitation source. The pulse repetition rate is 1 kHz and the pulse width is 124 ns. Figure 6(a) shows the photoacoustic image of the mouse ear, which contains major blood vessels and network pattern. The photoacoustic signal was performed 128 averaging with a 3.5 MHz transducer. In addition, a 905 nm 650 W pulsed laser diode was exploited for another set of experiment.⁸⁶ The reconstructed image of *ex vivo* porcine ovary was shown in Fig. 6(b). The imaging depth and SNR are

 $\sim 1 \text{ mm}$ and 25 dB, respectively. It proved the potential of pulsed NIR LD-PAM system for revealing the characterization of biological tissue and the diagnosis of the tissue cancer.

3.2. Pulsed VIS LD-PAM

A 300 mW VIS laser diode was exploited to the LD-PAM system, as shown in Figs. 7(a)-7(c).⁸⁷ The laser diode has a wavelength of 405 nm and a pulsed energy of 52 nJ. The pulse duration of the laser



Fig. 6. (a) and (b) Photoacoustic images of mouse ear and porcine ovary (images adapted from Refs. 85, 86).



Fig. 7. (a) and (b) Photographs of the compact laser diode and assembled excitation source, (c) schematic of the pulsed VIS LD-PAM system, (d) cross-sectional image of the carbon fibers, and (e) *ex vivo* image of mouse subcutaneous microvasculature (images adapted from Ref. 87).

diode is 174 ns and the pulse repetition rate can reach 1 kHz. A 3.6 MHz transducer was used to obtain the surfaces flaws of carbon fibers in Fig. 7(d), which was acquired by scanning along the z-axis with a 5 μ m step. The SNR of the photoacoustic image can achieve 22 dB without signal averaging and the lateral resolution reach up to 0.95 μ m. An image of a mouse back ex vivo is shown in Fig. 7(e), which was performed 512 averaging. Without contrast agent, the detailed features of the blood vessels were seen clearly. The pulsed VIS LD-PAM system was verified as a reliable mode for label-free imaging in superficial tissue.

A 405 nm Blu-ray DVD pickup head was integrated into an OR-PAM system. 68 The pickup head

can generate a tunable pulse duration ranging from 10 to 30 ns and a pulsed repetition rate of >30 kHz. A 50 MHz transducer was employed to acquire the photoacoustic signals. Figures 8(a)–8(c) show the reconstructed images of an unstained human blood smear, the zoom-in of the dashed region, and the maximum amplitude projection, respectively. Under a 1500-time signal averaging, the characteristics of red blood cells were visible clearly with a lateral resolution of 1 μ m, which has a great advantage in subsurface skin chromophores. Overall, the results verified the practicability of the pulsed VIS LD-PAM for label-free imaging in both small animal studies and blood examinations.



(a)



Fig. 8. (a) Three-dimensional photoacoustic image of an unstained human blood smear, (b) zoom-in of the dashed box in (a), and (c) maximum amplitude projection of the unstained human blood smear (images adapted from Ref. 68).

3.3. CW LD-PAM

A $405 \,\mathrm{nm}$ CW laser diode was utilized to photoacoustic and fluorescence microscopy.⁸⁸ The laser diode was modulated at 6 MHz and another $532 \,\mathrm{nm}$ CW laser diode was used as offset radiation. The schematic of the CW LD-PAM system is shown in Fig. 9(a). The dielectric mirror M2 separates luminescence from the excitation light, and the red reflector



Fig. 9. (a) Simplified schematics of the CW LD-PAM setup, (b) photoacoustic image of red blood cells, (c) photoacoustic image on microspheres, (d) fluorescence image of (c), and (e) overlay of (c) and (d) (images adapted from Ref. 88).



Fig. 9. (Continued)

M3 directs part of the light on a CCD camera which is exploited to get an overview image of the specimen. A needle hydrophone was employed to obtain the photoacoustic signals, and the luminescence light is led to an avalanche photodiode, respectively. The reconstructed image of erythrocytes was shown in Fig. 9(b), and the size of the image was $100 \times 100 \,\mu\text{m}$ with a step size of $1\,\mu\text{m}$. Figures 9(c) and 9(d) show the photoacoustic image and fluorescence image of fluorescent microspheres on a cover slip, and Fig. 9(e) was based on previous two images overlay. The signal intensity was strengthened after taking part in the 532 nm CW laser diode. Nevertheless, the photobleaching, optical absorption saturation, and temperature-dependent luminescence quantum yields of chromophores could result in a reduction in the corresponding signals.

4. LED-Based PAI (LED-PAI)

High-power LED as another potential alternative attributing to its low cost, miniature size, easy to integrate, besides, the efficient electronic driving and cooling system, and wide optical spectrum range from ultraviolet to NIR are peculiar strengths of LED. About a year ago, a high-power LED with a wavelength of 623 nm was employed in a LED-PAI system, as shown in Fig. 10(a).⁸⁹ The LED with 0.01% duty cycle can provide a pulse duration of 200 ns, repetition rate of 500 Hz, and pulse energy of $9\,\mu$ J. The sample was made up of three 1.4 mmdiameter tubes and rotatable driven by a stepper motor. A 3.5 MHz transducer was located on the opposite of the LED to capture the photoacoustic signal by averaging 5000 times. Figure 10(b) shows the reconstructed image of the tubes whose nominal values were within 0.1 mm of their nominal values. The penetration depth and image contrast ratio can reach up to $1.5 \,\mathrm{cm}$ and 11.5, respectively. The experimental results show that high-power LED could potentially be exploited in conjunction with NIR laser diode to obtain a wide range of biologically relevant wavelengths region for PAI.

In recent years, Hansen⁹⁰ took initial steps toward LED-PAI. Although the series of studies have proved the feasibility of using high-power LED as



Fig. 10. (a) Schematic of pulsed LED-PAI system and (b) reconstructed photoacoustic image (images adapted from Ref. 89).



Fig. 11. (a) Schematic of pulsed LED-PAI system, (b) maximum amplitude projection image, and (c) photoacoustic images of the mouse ear the horizontal and depth directions (images adapted from Ref. 91).

an excitation source for PAI, they did not demonstrate the feasibility of *in vivo* tissue imaging with LED, and the low SNR of photoacoustic signals caused by the low light intensity reduced the possibility of *in vivo* imaging. Furthermore, real-time imaging capability of their system was limited by the LED's low repetition rate and the large averaging time. Recently, in vivo tissue imaging has been proved for the first time by LED-PAI.⁹¹ In this study, a super-fast switching high-current LED driving circuit with a rise-time of 2.2 ns and a falltime of 3.5 ns operated at 200 ns pulses, a repetition rate of 40 kHz and provided 1.2 W output power at 405 nm. The LED-PAI system is schematically shown in Fig. 11(a). Two aspheric lenses were used to focus the LED beams into zone, which was around 1 mm^2 . The SNR can be up to 14 dB when the photoacoustic signal was averaged 4000 times at a point in the vasculature of the mouse ear.

Figure 11(b) shows the maximum amplitude projection image and the cross-sectional image corresponding to the dotted line shown in Fig. 11(c). The *in vivo* images indicated the potential for portable biomedical imaging applications, and the handheld PAI devices would be possible with further exhibited by achieving a higher pulsed light energy LED array.

5. Discussions

Laser diode relative to Q-switch Nd:YAG is simple, compact, inexpensive, and highly power efficient, and the output peak power of a single element laser diode can be only up to several hundred watts. Composing a single element diode array, focussing the light, coding light excitation, or stacking diode bars is possible to image biological tissue with appropriate SNR and spatial resolution. For real-time imaging applications, it is quite easy for laser diode to operate at a high repetition frequency. Nevertheless, laser diode still has a number of drawbacks. First, most high-power laser diodes are not miniature enough to be packaged into an endoscope except when using a coupling fiber. Secondly, portable devices which are equipped with high-power laser diode are still deficient in the driving and cooling systems. Thirdly, commercially available high-power laser diodes which does not contain visible wavelength limit their applications in multispectroscopic or VIS PAI. In addition, focal spot is the crux of the emphasis in stacked laser diodes, and it will be the biggest hurdle of fiber coupling of light.

On the other hand, the limited availability of VIS laser diode is the advantage of LEDs. In the range of VIS wavelengths, the biology tissue which contains chromophores, like vasculum, will benefit from excitation source of LEDs. High-power LEDs are securable as another attractive alternative owing to relatively efficient electronic driving and cooling system and wide optical spectrum range from ultraviolet rays to NIR relative to laser diodes. However, the desired illumination of LED was usually an irregular shape with a large viewing angle, making it difficult to realize beam shaping. Furthermore, the application of optical fiber coupler in the LED-PAI system would be inefficient for portable devices. Additionally, nearly all LEDs were in wide spectrum, which limits the usability of LEDs in quantitative analysis, such as blood glucose detection.

In this review, we discussed the state of the art of PAI systems with the miniaturized laser diode and LED excitations, which has shown progress in many aspects: from preclinical to clinical, from bench to bedside, and from expensive to low cost. Generally, they still need to develop in image quality, penetration depth, and imaging speed. From the portability and reliability point of view, the practical and affordable PAI technology will profit from the replacement of bulky solid-state lasers by tiny semiconductor lasers.

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