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# Generation of super-resolved optical needle and multifocal array using graphene oxide metalenses

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Ultrathin flat metalenses have emerged as promising alternatives to conventional diffractive lenses, offering new possibilities for myriads of miniaturization and interfacial applications. Graphene-based materials can achieve both phase and amplitude modulations simultaneously at a single position due to the modification of the complex refractive index and thickness by laser conversion from graphene oxide into graphene like materials. In this work, we develop graphene oxide metalenses to precisely control phase and amplitude modulations and to achieve a holistic and systematic lens design based on a graphene-based material system. We experimentally validate our strategies via demonstrations of two graphene oxide metalenses: one with an ultra-long ( $\sim 16\lambda$ ) optical needle, and the other with axial multifocal spots, at the wavelength of 632.8 nm with a 200 nm thin film. Our proposed graphene oxide metalenses unfold unprecedented opportunities for accurately designing graphene-based ultrathin integratable devices for broad applications.

**Keywords:** femtosecond laser reduction; graphene oxide; metalens; multifocal spots; optical needle

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## Introduction

Ultrathin flat diffractive optical devices with sub-wavelength thickness, such as metalenses, have emerged as promising alternatives to conventional diffractive devices, which offer new opportunities for myriads of miniaturization and interfacial applications, such as visual reality/augmented reality helmet-mounted display systems, miniaturized cameras<sup>1,2</sup>, and other functional interfaces<sup>3-10</sup>. Conventional Fresnel Zone Plates focus light by diffracting from a binary mask that modulates the amplitude of the incident radiation<sup>11</sup>. Although the Fresnel Zone Plates achieve focusing effect with deep sub-

wavelength thickness with metal coatings, the diffraction efficiency is low due to the blockage of light. More importantly, the wavefront cannot be accurately controlled to achieve high focusing performance. On the other hand, a more advanced solution is represented by Fresnel lenses, which introduce a phase only modulation varying along the radial direction to focus light more efficiently, enabling the minimized absorption losses, and well controlled wavefront<sup>12</sup>. Furthermore, the aberration can be pre-compensated by carefully designing the phase modulation structure, leading to advantages of high numerical aperture (NA) and better focusing resolution for

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optical systems. To guarantee a smooth spherical phase profile for efficient light focusing, the thickness of Fresnel lens has to be at least equal to the effective wavelength  $\lambda_{\text{eff}} = \lambda/n$ , where  $n$  is the refractive index of the medium.

Nowadays, due to the increasing demands on integratable optical components, the thickness of flat lenses needs to be reduced significantly, which inevitably challenges the design and fabrication techniques. Therefore, it is desired to achieve ultrathin flat metalenses design, which modulates the phase and amplitude of the incident beam simultaneously for high focusing performance with subwavelength thickness. Although, focusing and holograms have been achieved using phase only modulation in previous works, considering practical applications and sampling theory, controlling both phase and amplitude of the electric field allows more flexibilities in the design, thus it is easier to achieve more accurate light intensity distributions for tighter focal spots and holograms of higher quality<sup>13,14</sup>. Thus, the simultaneous amplitude and phase modulations are also necessary for applications such as full-color holography as well as laser beam synthesis with the characteristic of high resolution, high precision and high signal-to-noise ratio<sup>3,15,16</sup>.

Alternatively, flat lenses can be designed based on nanostructure engineering such as plasmonic nanostructures<sup>4,6</sup> and metasurfaces<sup>1,3,15–18</sup>. Comparing with conventional diffractive lenses, metalenses have broad advantages, such as reduced thickness and customized tunability, which could be used in both polarization and dispersion engineering<sup>19–21</sup>. Those are structural building blocks engineered to have specific optical properties of resonance and scattering, thus providing phase or amplitude modulations as new types of optical materials. Usually, plasmonic nanostructures and metasurfaces need to be fabricated either by electron beam lithography (EBL) or focused ion beam (FIB) lithography, which are expensive and challenging for scalability and post-processing customization. Recent developments in multilayer cascaded optical elements<sup>18,22</sup> and coalescing two types of meta-atoms<sup>15,16</sup> offer new opportunities to simultaneously modulate the phase and amplitude of an incident beam. Although, plasmonic and metasurface structures have been exploited in previous publications<sup>23–25</sup>, simultaneous control over phase and amplitude at a single position still needs further investigation, especially in 2D material systems, such as graphene and its derivatives. In addition, the multilayer or the coalesce

structures either requires prohibitive precise alignment between different layers or suffers from limited conversion efficiency due to spatial multiplexing methods, which adds extra complexity to designs and fabrication. In a word, although substantial effort has been devoted<sup>17,18,26</sup>, an effective and convenient approach to simultaneously achieving phase and amplitude modulations for practical applications still remains a great challenge.

## Result and discussion

Recently, high index dielectric materials, like GaN, ZnO and TiO<sub>2</sub>, have been widely used in the field of metasurface and metalens, due to their sufficient wavefront modulation capability, small intrinsic loss in visible range and compatibility with Complementary Metal-Oxide-Semiconductor (CMOS) technology<sup>27–29</sup>. In comparison, graphene-based materials have the advantages of strong mechanical properties, extraordinary electric conductivity, and zero band gap, making it an outstanding candidate for metalens, which is low cost and can further reduce the lens thickness to 200 nm<sup>30,31</sup>. Taking advantage of the conversion of graphene oxide (GO) material to reduced graphene oxide (RGO), a graphene-like material, in a laser reduction process, can simultaneously modulate phase and amplitude of incident light at a single position with an area that is defined by the laser focal resolution<sup>31–35</sup>. This allows simpler device design and fabrication as well as further miniaturization of ultrathin photonics devices to be stable in aerospace, chemical, and biological harsh environments<sup>36</sup>. Here, we generalize the quantitative phase-amplitude dependency for GO/RGO material (defined as the graphene-based materials) system and apply it in designing GO metalenses. Based on our quantitative phase-amplitude dependency, the positions of the concentric rings and the corresponding reduction extent of GO are precisely designed, free from the previous empiricism-based recipe<sup>31</sup>. Thus, the amplitude and phase modulations can be accurately controlled, and elaborately designed focal fields could be achieved using our GO metalenses. We experimentally validate the GO metalenses via demonstrations of two unique GO metalenses: one for focusing a super-resolved ultra-long ( $\sim 16\lambda$ ) optical needle (Fig. 1(a)), and the other for focusing an array of 4 axial focal spots (Fig. 1(b)), at the wavelength of 632.8 nm with an only 200 nm thin GO film. These GO metalenses can be easily integrated with lab-on-a-chip devices, thus offer

broad application possibilities in fast fluorescence microscopy<sup>37</sup>, ultrahigh density magnetic storage<sup>34,38</sup>, optical interconnects and particle manipulation<sup>39,40</sup>, particularly, in bio-photonics chip system<sup>40</sup>.

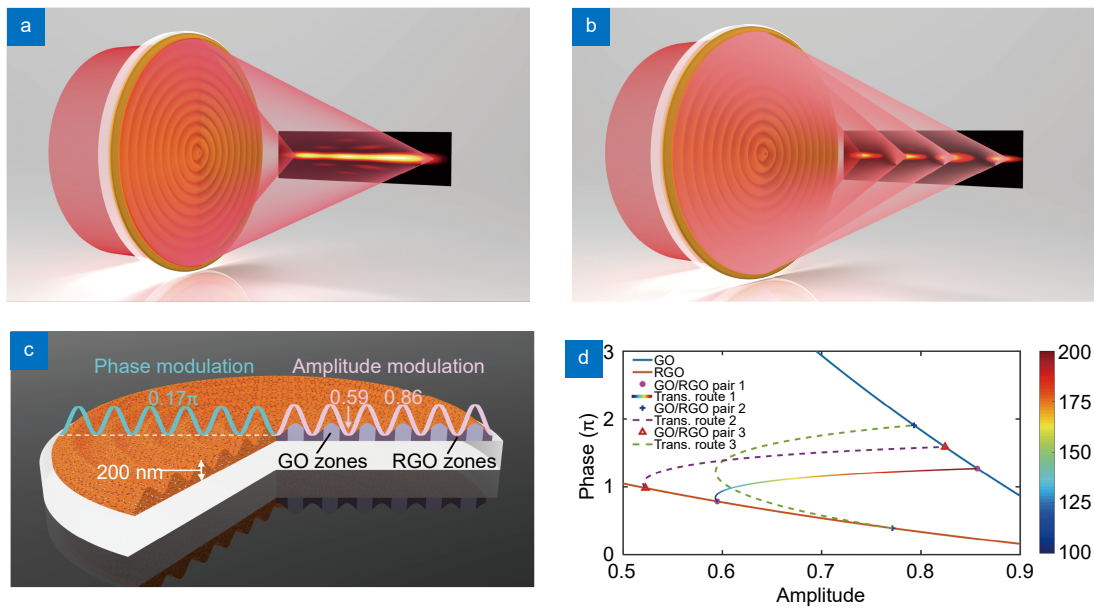
A planewave incidents on a glass substrate with a refractive index  $n_1$  and passes through the GO metalens with a thickness of  $t$  and a complex refractive index of  $\hat{n} = n + ik$ , and then it converges in the surrounding air medium ( $n_3 = 1$ ). The reflection coefficient for transverse-electric (s-polarized) light incident at an angle  $\theta_1$  is  $r_s = (r_{12} + r_{23}e^{2i\beta}) / (1 + r_{12}r_{23}e^{2i\beta})$ , where  $\beta = 2\pi / \lambda_0 n_2 t \cos(\theta_2)$  describes the phase factor.  $r_{mn} = (p_m - p_n) / (p_m + p_n)$ ,  $p_m = n_m \cos(\theta_m)$ , and  $\theta_m = \arcsin(\sin(\theta_1) / n_m)$ , which is the complex-valued form of the Snell's law<sup>41</sup>. For transverse-magnetic (p-polarized) light,  $p_m$  is replaced by  $q_m = \cos(\theta_m) / n_m$ . The total reflectivity is given by  $R_s = r_s^2$  and  $R_p = r_p^2$ . In the meantime, the absorption of the film can be calculated as  $A = \exp(-\alpha t)$ , where  $\alpha = 4\pi k / \lambda$  is the absorption coefficient. Therefore, the overall transmission of the film is given by  $T = 1 - A - R$ , which provides the amplitude modulation. The phase modulation is  $\phi = 2\pi n t / \lambda$ . The complex refractive index and the thickness should be functions of the spatial position vector  $\vec{r}$ , which can be expressed as  $\hat{n}(\vec{r}) = n(\vec{r}) + ik(\vec{r})$  and  $t(\vec{r})$  to design and fabricate functional flat diffractive photonic devices. Such a requirement can be met by the graphene-based material system. The laser reduction can trigger the insulator-semiconductor-semi-metal transition in GO material by effectively decreasing the bandgap with removing the oxygen-functional groups<sup>32</sup>. Upon laser reduction the real part ( $n$ ) (the refractive index) and the imaginary part ( $k$ ) (the extinction coefficient) increase, and the layer thickness of GO (8.1 Å) ( $1 \text{ Å} = 10^{-10} \text{ m}$ ) gradually decreases to that of graphene (3.4 Å) (See theoretical analysis in Supplementary information Section S1.2). In addition, the complex refractive index and the film thickness can be well controlled by laser power with detailed levels and high spatial resolution<sup>32</sup>. This property allows the design and fabrication of GO metalenses with high precisions in the amplitude and phase modulations and their spatial distributions.

The focusing schemes of the GO metalenses are shown in Figs. 1(a) and 1(b), in which a planewave incident light beam is focused by the GO metalenses into a super-resolved optical needle and an axial multifocal spot array, respectively. We choose these two cases because they re-

quire very accurate phase and amplitude modulations both in design and fabrication, in which the results are extremely sensitive to design/fabrication imperfections. Although the axicon for focusing an ultralong focal spot has been demonstrated by metalens before<sup>42</sup>, the linear phase modulation always causes either low focal resolution or relatively short nondiffracting distance. In addition, multifocal spots are conventionally achieved by phase plates or metasurfaces to modulate the incident beams at the back aperture of the objective lenses, where bulky high NA objective lenses are required<sup>43-48</sup>. In the meantime, the conditions for achieving multifocal arrays are even stricter, because it requires distinct constructive and destructive interference at the exact positions, otherwise, the focal spots connect with each other and cannot be well distinguished. Even though there are several demonstrations of multifocal arrays generation using metalenses<sup>29,49</sup>, the generation of multifocal arrays using a 2D material lens has not been reported.

The schematic demonstration of the GO metalenses is shown in Fig. 1(c), which is composed of concentric RGO rings and GO rings. The RGO rings are formed by direct femtosecond laser reduction on a uniform GO film, in which process the absorption and the refractive index increase while the thickness reduces<sup>31</sup>. In this way, the GO metalens achieves both phase and amplitude modulations simultaneously at the same position (Details of phase and amplitude modulation analysis can be seen in Methods and Supplementary Information Section S1.2). Due to near Gaussian shape intensity distribution of the fabrication laser beam, the resulted modulations show a Gaussian profile as demonstrated previously<sup>31</sup>. It has been found that the Gaussian profile is more advantageous in both focusing performance (resolutions) and diffraction efficiency<sup>31</sup> (See theoretical analysis in Supplementary information Section S1.2).

The phase-amplitude dependence is illustrated in Fig. 1(d). The blue line and brown line are the phase-amplitude relationships for the GO and RGO at the wavelength of 632.8 nm, respectively. Note that the maximum thickness change ( $\Delta t$ ) of the film depends on the initial thickness  $t$  of the GO film in the relationship of  $\max(\Delta t) = t/2$  due to the change of layer spacing of graphene-based materials as demonstrated before. In the meantime, the changes of maximum refractive index ( $\Delta n$ ) and extinction coefficient ( $\Delta k$ ) are independent on the film thickness and depend only on the material properties. However,  $\Delta k$  and  $\Delta t$  are all decided by the



**Fig. 1 | Schematic figures of GO metalens and its demonstrations.** (a) Optical demonstration for optical needle generated by GO metalens. (b) Optical demonstration for four axial focal spots generated by GO metalens. (c) Schematic figure of GO metalens on a glass substrate, the total thickness is 200 nm. When reduced by femtosecond laser in RGO area, the absorption and refractive index increase while the thickness is reduced to 100 nm. (d) Phase-amplitude relationship of GO/RGO pairs. Three GO/RGO pairs on blue and brown lines, whose thicknesses are 200 nm/100 nm, 300 nm/150 nm, and 250 nm/125 nm, are labelled with dot (●), cross (+), and triangle (Δ), respectively. The first and the second numbers indicate the thickness of the initial GO films (e.g. 200 nm) and the thickness (e.g. 100 nm) of RGO after laser reduction. The transitional routes between GO/RGO pairs are plotted. The GO/RGO pairs with dot marker and transitional route 1 with solid lines are utilized in this work. The colorbar relates to thickness of the RGO film, which is controlled by the laser reduction extent.

reduction extent, which is eventually controlled by the laser power. Thus,  $\Delta k$  and  $\Delta t$  are correlated. The strategy to find out the relationship between the  $\Delta n$ ,  $\Delta k$  and  $\Delta t$ , is by preparing the film with a certain thickness, then reducing it with different laser powers to obtain different reduction extents<sup>32</sup>. The resulted thicknesses are measured by an atomic force microscope (AFM) and the complex refractive indexes are measured by a spectroscopic ellipsometry<sup>32</sup>. Three GO/RGO pairs are shown on the blue and brown lines (Fig. 1(d)), whose thicknesses are 200 nm/100 nm, 300 nm/150 nm, and 250 nm/125 nm, and are labelled with dot (●), cross (+), and triangle (Δ), respectively. There is a generalized square root exponential relationship between the phase-amplitude modulations if the GO to RGO transition is continuous. The transitional routes for these GO/RGO pairs are illustrated by chromatic solid line, green dash line, and purple dash line, respectively. The color bar indicates the thickness of RGO for transitional route 1, which is controlled by the laser reduction extent. These routes describe phase-amplitude dependency, which can be expressed as (Supplementary information notes S1.1)

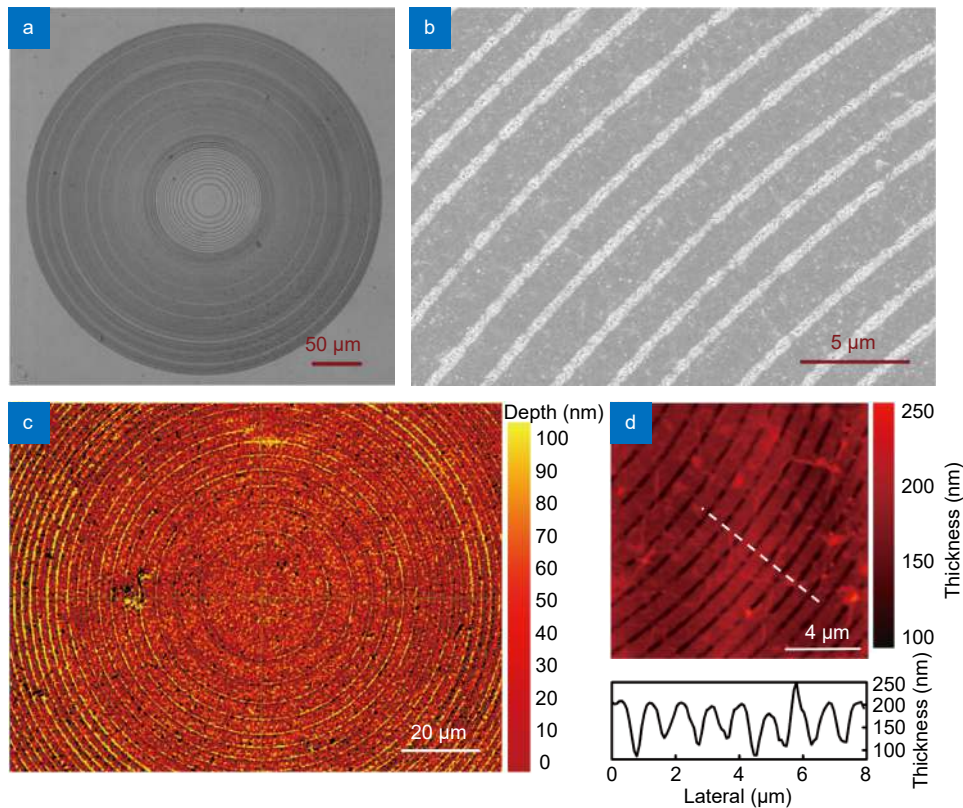
$$Amp^2 = \exp(C \cdot \phi), \quad (1)$$

where,  $\phi$  and  $Amp$  are the phase and amplitude of GO/RGO, respectively.  $C$  is the parametric equation of thickness  $t$ . The quantitative dependency is applied in designing GO metalenses, and the GO and RGO thicknesses are chosen as 200 nm and 100 nm, which is GO/RGO pair marked with dot (●). The transitional route is the chromatic solid line shown in Fig. 1(d) with a color bar indicating the thickness.

The position and the linewidth of each ring can be flexibly manipulated to optimize the light interference in the focal region of the incident beam. The linewidth of the rings is fixed at 400 nm, which is decided by the resolution of the laser fabrication system. Based on our quantitative phase-amplitude dependency, the optical needle lens and the multifocal lens are designed using an optimization process, in which the positions of the rings are input variables; the desired focal region optical field is the target function (see Methods).

The designed lenses (Supplementary information Table S2 and Table S3) are fabricated by reducing the GO film with direct laser writing (DLW), the optical setup of which is shown in Fig. S4. The optical image of the multifocal lens is shown in Fig. 2(a), which has a radius of around 180  $\mu\text{m}$  composing of 100 rings. By magnifying





**Fig. 2 | Characterization of GO metalens.** (a) Optical image of GO metalens taken by an optical microscope with an objective of  $\times 20$ ,  $NA=0.5$ , the scale bar is  $50\ \mu\text{m}$ . (b) The zoom-in image of the up-right corner taken by an SEM, in which the scale bar is  $5\ \mu\text{m}$ . (c) Large-scale surface morphology of GO metalens measured by a 3D optical profiler. The scale bar is  $20\ \mu\text{m}$ . (d) The zoom-in image of the lower-right corner taken by an AFM. The scale bar is  $4\ \mu\text{m}$ .

the structure with a scanning electron microscope (SEM) (Fig. 2(b)), the  $400\ \text{nm}$  linewidth by laser reduction is verified. In order to visualize the morphology of the lens, a three-dimensional (3D) optical profiler (Bruker ContourGT InMotion) (Fig. 2(c)) and an AFM (Fig. 2(d)) were used. The results indicate that the thickness is reduced, and the Gaussian like profiles resulting from the laser reduction can be clearly identified (indicated by the cross-sectional plot in Fig. 2(d)), which is similar to our design in Fig. S3(a). The maximum  $\Delta t$  defined as the difference between the top and bottom in the curve is  $100\ \text{nm}$ , which exactly meets our design condition. The maximum ring radius ( $a_{\text{max}}$ ) and focal lengths for both GO metalenses are  $\sim 175\ \mu\text{m}$  and  $210\ \mu\text{m}$ , respectively. The corresponding NA is  $\sin(\arctan(a_{\text{max}}/f))$ , which equals to  $0.64$  for both GO metalenses. Note that the NA demonstrated here is much higher than that in most references of the metasurface lenses<sup>10,22,50,51</sup>. Under this circumstance, we used the original Rayleigh-Sommerfeld theory without any approximation to calculate the focal intensity distribution<sup>52</sup>, because we have demonstrated that conventional theoretical framework based on the

Fresnel approximation can no longer give precise intensity distribution in the focal region of the metalenses<sup>52</sup>.

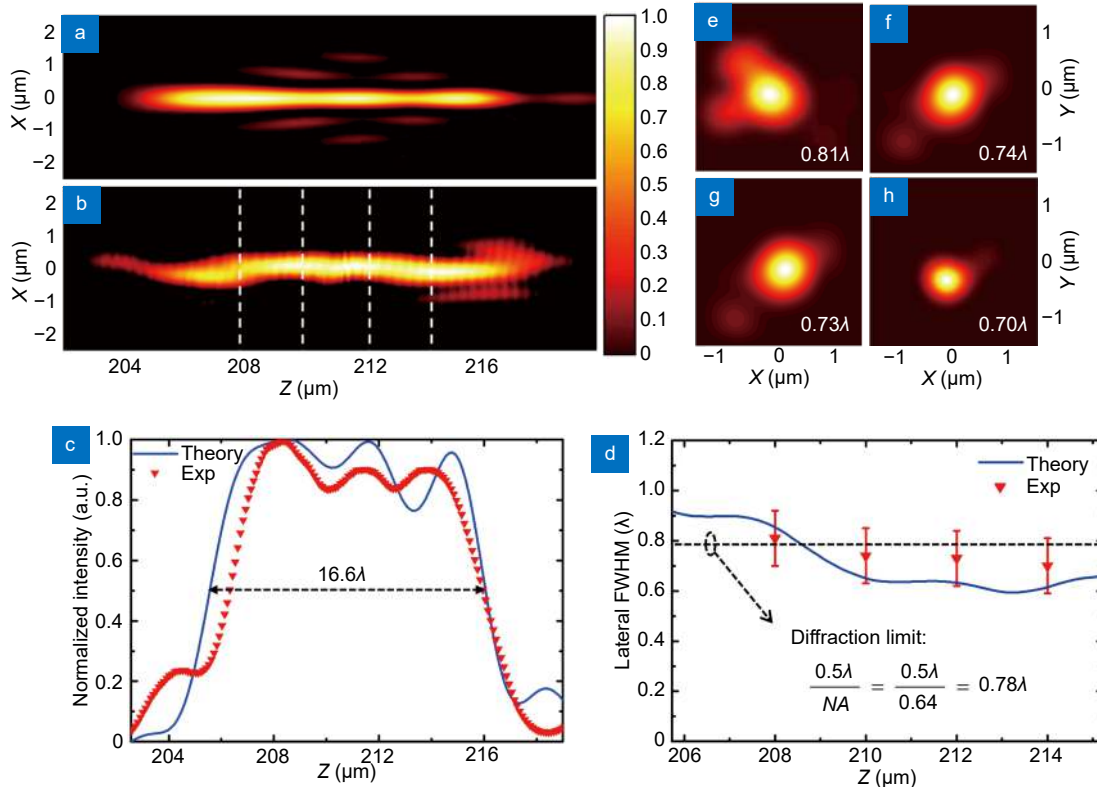
The focusing performance is characterized by a homemade imaging system (Fig. S5) consisting of a high NA objective ( $NA=0.8$ ,  $100\times$ ) mounted on a nanometric piezo stage and a tube lens ( $f = 200\ \text{mm}$ ). The intensity distribution in the focal region is captured by a high dynamic range (HDR) charge coupled device (CCD) camera. The lens is illuminated by the collimated planewave from a He-Ne laser at  $632.8\ \text{nm}$ .

The theoretical result of the optical needle in the  $x$ - $z$  plane is shown in Fig. 3(a), in which a needle with a sub-wavelength full width at half maximum (FWHM) along the lateral direction (Fig. 3(d)) covering the axial range of  $16.6\lambda$  ( $10.5\ \mu\text{m}$ ) in designed (Fig. 3(c)). The corresponding experimental intensity distributions in the  $x$ - $z$  plane and lateral FWHM are shown in Figs. 3(b) and 3(d), which fit well with the simulation results. In Fig. 3(c), both theoretical and experimental normalized intensity along the optical axis are depicted with little discrepancy. Furthermore, normalized intensities at corresponding positions shown in Figs. 3(b) (marked by the

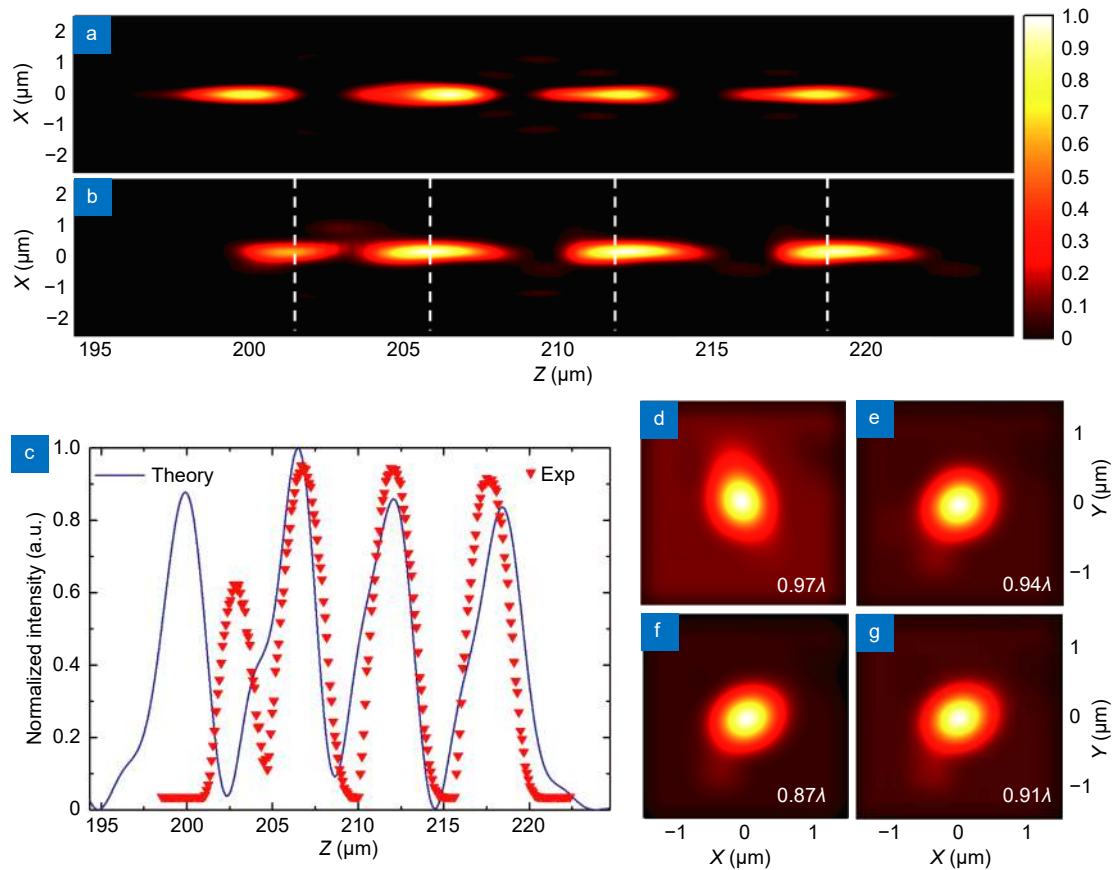
white dash lines) are demonstrated in Figs. 3(e)–3(h), and the lateral FWHMs at these positions are  $0.81\lambda$ ,  $0.74\lambda$ ,  $0.73\lambda$ ,  $0.70\lambda$ , respectively (Fig. 3(d)). The conventional diffraction-limited lateral resolution and axial resolution are  $0.5\lambda/NA = 0.78\lambda$  and  $2\lambda/NA^2 = 4.87\lambda$ , respectively. Therefore, the resolution of the optical needle is beyond the conventional diffraction-limited resolution, the super-resolved light needle is achieved by exploiting the concept of supercritical focusing condition<sup>53,54</sup>, which is defined between conventional diffraction limit and super oscillatory criterion ( $0.38\lambda/NA$ ). In our design method (detailed design process can be found in Methods and Supplementary information Section S1.2), by elongating the focal spot along the axis direction to form an optical needle, the lateral resolution beyond the diffraction limit can be achieved.

In addition, the theoretical and experimental results of the axial multifocal array in the  $x$ - $z$  plane with four nearly identical focal spots along the optical axis are shown in Figs. 4(a) and 4(b). The lateral and axial resolutions of each spot are  $\sim 0.7\lambda$  and  $\sim 4\lambda$ , respectively. The experimentally measured normalized intensity distribu-

tion along the  $z$ -direction is shown in Fig. 4(c), which agrees well with the theoretical result in the same plot. The Figs. 4(d)–4(g) show that the four focal spot distributions are smooth and nearly identical at the positions marked by dashed lines in Fig. 4(b), with lateral FWHMs of  $0.97\lambda$ ,  $0.94\lambda$ ,  $0.87\lambda$ ,  $0.91\lambda$ , respectively. It is worth mentioning that the well-separated focal spots with uniform intensity distributions can only be achieved by accurate phase and amplitude modulations, which can be attributed to the accurate control of the complex refractive index and the thickness with the laser reduction technique. Here, with quantitative phase-amplitude dependency guiding our design and laser fabrication, we demonstrate the generation of multifocal arrays with high qualities in the case of using GO metalenses. Although some discrepancy between simulation and experiments can be seen in Fig. 3 and Fig. 4 due to the surface roughness of the as-prepared GO films (the detailed analysis can be found in Supplementary information Section S1.3), the super-resolved optical needle and overall multiple foci distribution are still reasonably well matching the simulation to verify the accuracy of our amp-



**Fig. 3 | Focusing characterization of optical needle GO metalens.** (a), (b) Normalized intensity distributions in the  $x$ - $z$  plane from theoretical calculation and experiment, respectively. (c) Theoretical and experimental normalized intensity plots along optical axial in the focal region. (d) Theoretical lateral FWHM plot along  $z$ -direction near focal region and experimental FWHM points at the positions marked by the dash lines shown in (b) at  $208\ \mu\text{m}$ ,  $210\ \mu\text{m}$ ,  $212\ \mu\text{m}$ ,  $214\ \mu\text{m}$  respectively. (e)–(h) Normalized intensity distributions at corresponding positions shown in (d), the lateral FWHMs at these positions are  $0.81\ \lambda$ ,  $0.74\ \lambda$ ,  $0.73\ \lambda$ ,  $0.70\ \lambda$ .



**Fig. 4 | Focusing characterization of axial multifocal spots GO metalens.** (a), (b) Normalized intensity distributions in the  $x$ - $z$  plane from theoretical calculation and experiments, respectively. (c) Theoretical and experimental normalized intensity plots along the optical axial in the focal region. (d)–(g) Normalized intensity distributions at positions marked by the dashed lines shown in (b), the axial positions are  $202 \mu\text{m}$ ,  $206 \mu\text{m}$ ,  $212 \mu\text{m}$ ,  $218 \mu\text{m}$ . The lateral FWHMs at these positions are  $0.97 \lambda$ ,  $0.94 \lambda$ ,  $0.87 \lambda$ ,  $0.91 \lambda$ .

litude and phase dependency and the design of our GO metalenses.

It is noteworthy that the GO metalenses are thicker than the metasurface designs based on metal structure. However, as metals are general lossy materials in visible range, the efficiency of the metal based design is limited to around 1%<sup>42</sup>, which is relatively low. On the other hand, the recent development of dielectric metasurface can significantly improve the focusing efficiency, however, the thickness of the metasurface needs to be several hundred nanometers, which is typically near the effective wavelength  $\lambda_{\text{eff}}$  of the incident light. Compared with the dielectric metasurface, our 200 nm metalenses are thinner due to the achievement of subwavelength thickness by applying both phase and amplitude modulations. In our GO metalenses, the effective wavelength of the 632.8 nm laser in the GO material is 351.6 nm. In addition, overall focusing efficiency is defined as the ratio of total power in a circular aperture with the size three times of the FWHM of the focal spot to the total power of the transmitted light through the lens<sup>55</sup>, which is

around 10%. Considering the amplitude modulation giving a transmission around 70%, the focusable energy compared with the energy immediately after amplitude and phase modulations is around 15%. The loss is mainly due to the zero-order transmission and the -1 order diffraction, which do not contribute to the focus. The efficiency can be further improved by introducing different modulation levels into the design that minimize the zero and -1 orders, which is feasible by controlling the laser power. As demonstrated in our previous work, up to 8 modulation levels can be obtained in the GO/RGO system<sup>32,35</sup>.

In our previous work we have proved that by using the simultaneous phase and amplitude modulations provided by photo-reduction of GO materials<sup>56</sup>, it is possible to focus optical energy with subwavelength resolution<sup>31</sup>. In this work, we further build the relationship between the amplitude and phase modulations to design the GO metalens to show advanced functionalities, such as an optical needle, and a multifocal array, which are quite challenging for any metalenses. Since the analytical

design method used in our previous work cannot be applied to generate advanced focal field distributions, we further developed an optimization method, which is able to provide sophisticated control to achieve the required lens designs. Compared with phase or amplitude modulation only metasurfaces, the simultaneous phase and amplitude modulations of the GO/RGO material system provide further flexibility to the design method. The successful demonstrations of the optical needle and the multifocal array not only prove the effectiveness of the design method, but also confirm the accurate phase and amplitude controls can be achieved in experiments. Therefore, combining the design method and experimental fabrication technique, it is possible to further demonstrate GO metalenses with different functionalities, thus broad applications.

### Conclusion

In conclusion, based on the unique optical properties of graphene-based materials (GO and RGO) under laser illumination, including the complex refractive index and the thickness change, we build up the quantitative phase-amplitude dependency, which provides a well-guided design process for photonic devices based on graphene-based materials with simultaneous amplitude and phase modulations at a single position. By understanding the phase-amplitude dependency, we are able to design photonic devices with a high accuracy. To validate the accuracy of our GO metalens design strategy, we experimentally demonstrated GO metalenses, which generate an ultra-long (~16λ) super-resolved optical needle and an axial multifocal array (4 focal spots) as examples. Although we have demonstrated only two designs in the study, the phase-amplitude dependency can be further applied to design other photonic devices such as optical chain, optical cage, optical bubble and optical tweezers for the applications in optical trapping, optical manipulating, optical delivering and optical staking<sup>47,57-59</sup>.

Due to the flexibility and mechanical robustness of graphene-based materials as well as the simple, low-cost, and scalable fabrication of GO metalenses, these ultrathin flat optical components enable great potential in applications and possess commercial value in integrated optical device<sup>33,60</sup>. Compared with the conventional nanofabrication techniques such as EBL and FIB, which are required for the fabrication of metasurfaces, the DLW technique is able to in-situ fabricate lens in a single step. The attributes of large-scale, long working distance, high lateral resolution and desired longitudinal morphology constitute a milestone that optical manipulation, port-

able microscope, parallel optical processing and high-density optical data storage can be realized in an integrated setup without the requirement of bulky optical elements<sup>43-46,48,61</sup>.

### Methods

#### Preparation of GO film

The ~200 nm homogeneous GO film was prepared using the vacuum filtration method with high quality GO solution synthesized by the modified Hummer's method<sup>62</sup>, and then was transferred onto a cover glass.

#### Lens design and optimization

The designs of the optical needle lens and the multifocal lens are based on the powerful interior-point optimization algorithm<sup>63</sup>. The target functions for optical needle and multifocal lenses are given by Eq. (1) and Eq. (2), respectively.

$$I_{\text{needle}}(z) = \begin{cases} 1, & 205.73 \mu\text{m} \leq z \leq 215.22 \mu\text{m} \quad (325\lambda \leq z \leq 340\lambda) \\ 0, & \text{otherwise} \end{cases}, \quad (2)$$

where,  $I_{\text{needle}}(z)$  is a rectangle function along the Z axis defined from 189.90 μm (300λ) to 227.88 μm (360λ).

$$I_{\text{multifoci}}(z) = \sum_{i=1}^4 1 - \left| \frac{1}{t_0} (z - z_i) \right|. \quad (3)$$

The target function of multifoci is a summation of triangular function along the Z axis defined from 189.90 μm (300λ) to 227.88 μm (360λ).  $t_0$  equals to 5λ, which also defines the FWHM of multifoci.  $z_i$  are peak positions, which are 315λ, 325λ, 335λ, and 345λ, respectively. The optimum designs have minimal variances between the actual field distributions and the merit functions. The electrical fields diffracted by the circularly symmetric lens illuminated by the planewave can be described by Rayleigh-Sommerfeld diffraction theory<sup>64</sup>. The electrical field at position ( $r=0, z=f$ ) is given by<sup>65</sup>:

$$\begin{aligned} E(r=0, z=f) &= \int_0^{a_{\text{max}}} E_0(r_1, z=0) r \frac{\exp(ik\sqrt{z^2+r_1^2})}{z^2+r_1^2} \\ &\times \left( ik - \frac{1}{\sqrt{z^2+r_1^2}} \right) dr_1, \\ E_0(r_1, z=0) &= \begin{cases} A_{\text{GO}} \exp(i\varphi_{\text{GO}}), & \text{without laser reduction} \\ A_{\text{T}} \exp(i\varphi_{\text{T}}), & \text{with laser reduction} \end{cases}, \\ I &= \text{abs}(E)^2, \end{aligned} \quad (4)$$



where,  $a_{\max}$  is the radius of the largest ring,  $k$  is the wavenumber.  $A_{\text{GO}}$  and  $\varphi_{\text{GO}}$  are the amplitude and phase modulations for GO in our design, respectively. Meanwhile,  $A_{\text{T}}$  and  $\varphi_{\text{T}}$  are the amplitude and phase modulations of RGO zones, which obey our GO phase-amplitude dependency (chromatic transitional route 1 in Fig. 1(b)). The intensity at the focal point is the square of the absolute value of the electric field.

The constrains of the optimization are shown in Eq. (5):

$$\begin{cases} a_{m+1} - a_m > l \\ a_1 > d \\ NA \geq NA_{\min} \end{cases}, \quad (5)$$

where,  $a_m$  are the ring positions for RGO.  $l$  denotes the minimum distance between the adjacent two rings, which is 1.0  $\mu\text{m}$ .  $d$  is the minimum radius requirement for the first ring, which is set to be 0.8  $\mu\text{m}$ .  $NA_{\min}$  is the minimum NA requirement in the optimization, which is set to be 0.6 for both multifocal lens and optical needle lens. For the sake of experimental fabrication accuracy, the width of all rings is set to be 400 nm. Moreover, the maximum phase modulation caused by the RGO and GO film is calculated to be  $-0.1700\pi$ ; the minimal transmittance of rings is set to be 0.3539; the working wavelength of the metalenses is 632.8 nm.

### Femtosecond laser fabrication

With a commercial laser 3D nanoprinting setup (Special Edition, Innofocus Nanoprint<sup>3D</sup>) (Fig. S4), the laser reduction process was performed on our as-prepared GO film according to the radii in supplementary information Tables 1 and 2. The femtosecond laser beam (100 fs pulse, 100 kHz, 800 nm) with a fabrication speed at 30  $\mu\text{m}/\text{s}$  was calibrated at 12  $\mu\text{W}$  for reducing the GO film, which is mounted on a 3D nanometric piezo stage (Physik Instrumente). A high NA oil objective ( $NA=1.4$ ,  $100\times$ ) is used in fabrication. The lateral resolution of laser fabrication on GO thin film is determined by the size of femtosecond laser focal spot and the laser interaction threshold with the GO material. The FWHM of the laser focal spot is determined by  $\lambda/2NA$ , where  $\lambda$  is the wavelength of the writing laser and  $NA$  is the numerical aperture of the writing objective lens. In our case, laser wavelength is 800 nm,  $NA$  is 1.4. Thus, the laser resolution is around 300 nm. In the direct laser fabrication of GO lenses, the linewidth is approximately 400 nm, due to the selection of laser power and the laser interaction threshold with the GO material.

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## Author contributions

B. H. Jia, H. Lin and C. W. Qiu conceived the idea and developed the strategy of the project. C. L. Hao and C. W. Qiu, developed the optimization algorithm, and designed the lens parameters. H. T. Wang conducted the GO film preparing, GO lens fabrication, GO lens characterization and focused light fields measurements. B. H. Jia, H. Lin and H. T. Wang contributed to data analysis. H. T. Wang and C. L. Hao drafted the manuscript. All authors discussed and commented on the manuscript.

## Competing interests

The authors declare no competing financial interests.

## Supplementary information

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