太赫兹科学与电子信息学报

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4 + PVSOBM PG 5FSBIFSU[4DJFODF BOE & MFBUOSPOJD * 0(

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接触网断线落在碳纤维车体的过电压仿真分析

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(1. YD'L~Ç å fD'D'D²5Í) 5K|~\$ U••H L~Ç 266000Už2. Y)*a |.ý¬Kò~\$ 0X 5 m 5-@/¢ | U••>« V Ë 030032)

摘 要U•电气化铁路运行环境的复杂性使接触网存在断线的可能,断开的接触网导线落在动 车表面容易形成车体过电压。为了评估碳纤维动车车体由于导电性劣于传统铝合金车体而引起的 过电压危害,基于某公司设计的半碳纤维半铝合金司机室车体结构,建立了动车组浪涌过电压电 路模型。通过仿真求解接触网断线落在动车司机室车顶时司机室不同位置浪涌过电压的传输特性, 得到车体过电压最大幅值 L7在 μs内快速衰减,对车载电子设备造成安全隐患,并提出将 车载设备的接地线缆直接连接在车厢的接地碳刷附近,为司机室车体的过电压防护设计提供理论 依据。

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4JNVMBUJPO BOBMZTJT PG PWFS WPMUBHF PG CPEZ PG ESJWFS T DBC

96 :VUF•'&/(:VNJU9#+1"* (BLOD•B1"/('VRJB⊍Q(B10 8FORJOH

\$33\$ 2 J O H E B P U¥+ J G BB+ O2 H O\$H RE B P 4 I B O EUP \$D H J OŽB

5IF SE 3FTFBSDI *OTUJUVUF PG \$IJOB & MFDU+351BOZID/BO514DBOD#Y\$MBPEHEZ (SPVQ \$PSQP

"CTUBBBDNQMFYJUZ PG UIF SBJMXBZ PQFSBUJPO FOWJSPONFOU NB MJOBFOE UIF CSPLFO DPOUBDU XJSF GBMMJOH PO UIF TVSGBDF PG UIF PG UIF DB*CO OPFSEZFS UP FWBMVBUF UIF PWFS WPMUBHF EBNBHF PG \$BS \$'31 DBC CPEZ EVF UP JUT QPPSFS DPOEVDUJWJUZ UIBOUEDIBU PG U DJSDVJU NPEFM PG \$'31 USBJO CPEZ JT FTUBCMJTIFE CBTFE PO UIF EFTJEOF USBOTNJTTJPO DIBSBDUFSJTUJDT PG TVSHF PWFSWPMUBHF TPMWFE CZ T5JINFVNMBBYUJNPYON WPMUB7HEFOSEFBDUFFTOVBUFJUS &BJODJEJMTZ BJO QPUFOUJBM TBGFUZ IB[BSE GUPS]TPQ SOPPOBESTEFEFRUMBOUNEOFUHSPVOEJOH X FRVJQNFOU TIPVME CF DPOOFDUFE EJSFDUMZ &FJEOSI QISFPWISEPFVTOEBJO UIFPSFUJDBM CBTJT GPS UIF EFTJHO PG PWFSWPMUBHF QSPUFDUJPO .FZXFUSGESTPLFO DP;OUJBIDUT QVFJFOEPFWSFESJNOPMUBHF

ÙU•%líC Í *aÍ EF 0u@ê 3EL < 9 8/7 Ò+° (ß, •ù Ñ? 4}Ù3ë : V Ñ \ U•'; A *aI Đ 9 ý *K Ô ^ U•ÙC " VC K\$ U• Ñ? 4}E T Ç*a U• (3ë Ø ºlíC 3ëC 6 å U• ÔD'3ð3ûDó " Y Ñ \D'M¢ (7 P -- C U• TD' •="LŽ Ž <Dó*a · U• F %D'D©@ê 3+° μ " SEL <\$^ TK¼ Ϊ

f²@ð \ Ñ? 4} Ù 3ë9i T-ß 3Đ4 \$ f Đ D' M¢ "D' • Dó*a · % D' D© @ê 3+° μ " S U• X ³ ü[~] \$ ü & +° v-ß 3Đ4 vJ 4Fý \$ f Đ D' • f î5/ U•"wFû ¢ Ô (&-ß 3Đ 4 D' •+°Kg à î œ U• &/÷ ² \$ f Đ D' • Dó*a ·*aC M · U• EF Dó +,K 2 ¼ ² Ñ? 4} Ù 3ë9i T-ß 3Đ 4 \$ f Đ D' M¢ "D' • Dó*a ·+° LD¿ '¥ S U• f \$ f Đ D' •+°Dó*a ·K^ Đ @ê @ĺ ü Ç ²)2 @æ É š

1 动车组车体阻抗特性

A · ÔD' 2~7 #D' • f L4 J 4Fý | Å U• \$ f Đ (1 , 8 #)D' • f v-ß 3Đ4 vJ 4Fý | Å D' • «D©3ÿ ° *] Á â Ó Å D'M¢ 0 Å 3ð < f, V • U•E FØ 2 $\hat{u}7$ ®D' Î0u t f 4 VLŽU• \hat{u} LŽOu t f, V*aKg ,*a K ^5€U• ® * 1 I.f \$ f ĐD' • 2 f-ß 3Đ4 , J 4Fý PF 2 U• ¢ Y R_{efrp} , L_{efrp} % À-ß 3Đ4 F 2+° V = î œ U• R'_{efrp} , L'_{efrp} % À-ß 3Đ4 F 2+° 3á = î œ U• R_{AI} , L_{AI} =".f J 4FýF 2+° V = î œ U• R'_{AI} , L'_{AI} =".fJ 4FýF 2+° 3á = î œ 2~7 #D' Î f "D' J 4Fý | Å U• R_{hori} , L_{hori} % À V = î œ U• R_{vert} , L_{vert} % À 3á = î œ D'D' Á " F fJ 4Fý | Å U• R_{ioint} =".fD'K E Ñ "



% ° 2~7 D'+°J 4 FýD'• U• K1 ³(Z [6-7] - D'• V = *a Kg f 12.8 mΩU•*a K f 5.78 μHU•3á = *a Kg f 2.8 mΩU•*a K f 0.61 μH % ° 1 , 8 D'+° \$ f ĐD'• U•J 4 Fý -ß 3Đ4 | Å 0 Œ, v e š (•*a Kg@Í0à ~; $R = \rho l/S$ U• ¢ Y R f*a Kg U•ρ l S 2 W % À | Å+°*a Kg(³ J«Ò, V VLŽ/ U• \$ f ĐD'•J 4 Fý F 2 V = J«Ò f Ë '+°, v U• ¢ î œ 9 U• E @Ð f V = *a Kg f Ë '+°, v U• ϔ 6.4 mΩUž î5/ ϔ, (3ë*a K@Í0à ~; U•

$$L = \frac{\mu_0 l}{2\pi} \left(\ln \frac{2l}{r} - 0.75 \right) \tag{1}$$

; Y U•μ₀ f,K/¦-í ((³ Už/, r f | Å+°J« Ò, VLŽ v ° U•• (3ëJ« ÒE S ° VLŽ v ° " U•J« Ò/4U- fË '+°, v U•% œM¥ B ´; U• Dý h@Đ f*a KFû fË '+°, v U•š•ÔÙ\$fĐJ 4FýD'•F 2 V =*a K3Ò fË ' +°, v U•ϔ 2.89 μH 3á = îœ 9 ý*K B

-ß 3Đ4 Å*T | Å g>-1 *] • =4B 3ó / 4 <+°J& n å ; 2 W f [O]10 [0/90/09/00]s [0/90/45/-45/0]s +° 3.ù n 4 « ,*] Đ õ 4B 3ó /, Ñ 4 <+° n 4 « ¢ Y U•[O]10 f•, J& n>b Ò+° • =J& n n 4 « U•[0/90/09/00]s fW 2 .ù>b Ò+° • ĐJ& n n 4 « U•[0/90/45/-45/0]s f1 4.ù>b Ò+° π/4 J& n n 4 « U•58 Đ õ 4B 3ó n 4 «*] Đ õ 4B 3ó /, Ñ 4 < U• 9 "TJ& n>b Ò J& nM! »+°K MÄ ^[1-2] D' • ß 3Đ4 | Å FFó*T*] È 3å 4B 3ó /, Ñ 4 <+°-ß 3Đ4 n 4 «U• f\$ f 50 mm×50 mm×2 mm+° c " U•!ë • Đ å =E =xKg à "wA U• à \ È 3å 4B 3ó +°-ß 3Đ4 n 4 «!ë • Đ å =+°Kg à 2 /! D⁻ s , U•*aKg(³ S 3Ò f 450 $\Omega \cdot mm^2/m$ U•*a K 3Ò f 0.18 µH 582WJ +°*aKg(³ f 0.018 $\Omega \cdot mm^2/m$ U• J 4) 9 4 T-ß 3Đ4 | Å+°[°]T, Z U• >ò f ¢ 5€ U•*] °J +° (*a SE f°-ß 3Đ4 | Å U•I 9 4 | Å+°Kg à î œ *TJ 4}+°Kg à î œ + J 4}>ð h f 200, (û Ÿ å 8 \$0‡4} 6+° €, h œ, f 200)U• Æ Ò f 0.1 mmU•D' • J 4Fý | Å f·6€ 3ÿ ° U•9Å+Ú Æ Ò 3Ò f mm(6 7 2 n 0 3 mm) E5 Æ Ò 2 W f 0.2 mm , 6 mm ¢ f \$,\$ 8+°J 4} c ", J 4Fý c "E =xKg à "wA U• à \ J 4}*aKg 3Ò fJ 4Fý+° 300 9 U•*a K3Ò fJ 4Fý «+° 1.2 9 š • \ 0Ã-ß 3Đ4 UJ 4} UOD' •+°*aKg 3Ò fJ 4FýD' •+° 20 9 U•*a KfJ 4FýD' •+° 1/4 *] • à \ \$f ĐD' •J 4Fý F 2 V =*aKg 3Ò f 6.4 mΩU•*a K3Ò f 2.89 µHU•3á =*aKg 3Ò f 2.8 mΩU•*a K3Ò f 0.61 µHUžß 3Đ4 F 2 V =*aKg 3Ò f 1.92 ΩU•*a K3Ò f 3.47 µHU•3á =*aKg3Ò f840 mΩU•*a K3Ò f 0.73 µH

2 仿真模型构建

& ° ÔD'3ð g*aC 3ÿ ° U•3ÿ 4 ÊKqD' • | Å1§ · Ç*a3ëC Kg à D' \pm @ê 3 · #0u U• % ÔD'3ð3ÿ °E =x*a C î œ 0u t ÔD'3ðDó*a · M ·*] Ç*a2'4 , ÔD'3ð PF 23ð < Ç*a2'4 *]'_i A *a l N´3ë Ñ? 4} lÎ D" "m3ë3ð < '_i A *a l Ç*a*a · U_s f 27.5 kV 5/;}0¬ •J* · Ø ., Ñ Ç*a å ;+° •3ë*a!@ BlíC '_i A

4} U• & ^o Carson)2 @ $#^{71}$ U•0u t*aKg R_s *a K L_s % *a å C_s 2 W f 3.4 Ω 0.034 1 mH , 0.283 μF ÔD'3ð M · D'D© Ô C2'4 D'Î \tilde{N} 2'4 P * a42 * # f TENAX-Train-Plux U• * a ? \ g ÙC " wK 1 P ·*a42 P ·*a42J« Ò3Ò f 2 mU•P ·*a42J&@ê T3 \ 6 D'U• ¢ Y 3 D' _ 6 D'+°P ·*a42J« 20 mU•4 D' _ 5 D'+°P ·*a42J« 26 m • yJ« Ò*a42+°*aKg *aK *aå2 W f 0.2 mΩ/m 0.17 μH/m 0.32 μF/m 'jAg · "Fó*T XFRM-Linear 3ë S · " U• · ", M Ó*a K f 0.34 HU•, M Ó*a K f 62.09 HU• 95/;}P z · Ó4 3ð*a Kg "m " q >-1 "m M f E2 M f U•*]4 4D 1 $\emptyset - \cdot \emptyset \cdot 0 (17\hat{U})$'s (Insulated Gate Bipolar Transistor U•IGBT) ... -0130 4 58 < U• % °D' •Dó*a • Ó*K : j • ù U• •%AF2)*' 9@Í K1 ³(Z [6-7] - U•• VBKD©*a Ô fMÉ Æ Ë(³ 8 VBKD©*a f ü Ç*a6) U• g Ë(3 f 4 800 kWU•3û @Í0Ã ÃU• · "BKD©0u t*aKg R f f 600 kWU•û g ⋅"f 0.71 Ω A · ÔD'Fó*T ^5€*aKg "+° Ñ \ å ; U• Ñ *a Kg μ=ñ TD' Î+° • 7 å U•*aKg h f 50 mΩU•&b :*] Ñ *a42 2 WE Ñ TD' Á y :+ 2 VD = âD 0 U•0u t*aKg *a K 2 W f 2.4 mΩ 2.04 μH • B U• Ñ \-ß c 0+ *aKg3Ò f 5.03 m Ω š • $\tilde{A} \setminus \hat{O}D'3\delta D\delta^*a \cdot +, K M \cdot \mathbb{R}^*$ 2 I.f



* 2 ÔD'3ðDó*a ⋅ +,K M ⋅

;†3ë 2 4 F 2=".f Ñ? 4} T Ù%å 0 Ù, U•&b :9i T \$ f Ð (1 #D')D'M¢-ß3Đ4, Ó(D%å) M·Y+°A B C D E%å f*a·Îl´+°y4š U•2 W=".fD'ÁJ 4 Fý, Ó D'M¢J 4 Fý, Ó J 4 Fý ÿÿ-ß3Đ4 *xLŽ D'M¢-ß 3Đ4, Ó D'Á-ß3Đ4, Ó, :Dš Ñ \-ß c

3 仿真结果分析

Ñ? 4} (3ë Y Ñ \-ß 3Đ4 D'• : U•D'M¢-ß 3Đ4 , Ó*a y,ØK sP U•,P*a yDê \² 26 kV 9 8 y4š+°"-",Dó*a · BB·ë & X,7 U•T 60 μs ± EK=œ ûU• w : T;8/ ±" Ô D'ÁJ 4Fý, ÓDó*a · q h f 6 kVUž D'Á-ß 3Đ4 , ÓDó*a · q h f 23 kVUžJ 4Fý ÿ-ß 3Đ4 *xLŽ 0 U•Dó*a · , S q hDê \² 20 kV Ñ \-ß c 0Dó*a · q h! D⁻; U•f 34 V

Dó*a · T V = L ÙDó/7 Y U• úD'M¢-ß 3Đ4 , Ó \J 4Fý-ß 3Đ4 *xLŽ U•, S q h 7Ky ² 6 kVU• úJ 4Fý-ß 3Đ 4 *xLŽ \D'M¢J 4Fý , Ó U•, S q h 7Ky ² 8 kVU• \$ f ĐD'• "J« 26 mU•J 4FýF 2 ,-ß 3Đ4 F 2F) [13 mU• •Dó*a · T-ß 3Đ4 D'•="LŽ V = LD; Dó/7 Y U•*a · 7Ky q Ò f 461.5 V/mU•Dó*a · TJ 4FýD'•="LŽ V = LD; Dó/7 YU•*a · 7Ky q Ò f 615.4 V/m Dó*a · T3á = L ÙDó/7 Y U• ú-ß 3Đ4 , Ó+°D'M¢ \D' Á U•, S q h 7Ky ² 3 kVU• úJ 4Fý , Ó+°D'M¢ \D' Á U•, S q h 7Ky ² 6 kV ÔD'D' ÎP Ò3Ò f 4 mU• •Dó*a · T-ß 3Đ4 , Ó!ë 3á = L Ù U•, S*a · 7Ky q Ò f 750 V/mU• TJ 4Fý , Ó!ë3á = L Ù U•, S*a · 7Ky q Ò f 1.5 kV/m Dó*a ·!ë

•*a K ,*aKg+° ,, T U•Dó*a · ý*K [8• ¢ T 60 μs ± EK=œ û
3) \$ f ĐD' •Dó*a ·!ë3á = L Ù=œ û q Ò °V = L Ù U• TJ 4Fý="LŽ L Ù+°=œ û q Ò °-ß3Đ4 ="LŽ
4) D' •Dó*a · S ° 2 kVU• 9\$ BßD'D©*a |@ê 3 μ " \+° Ñ '3 ò U•:Dš Ñ \-ß c 0Dó*a ·, S h 5 34 VU•

1) -ß3Đ4 D' •+° (*a S g>- ÉB, B n+°J 4} U•J 4} T Ê f (*a S+° 8 "U• ‹6)B£ *a-í {:i+° ^*T 2) Ñ? 4} Ù3ë9i T \$ f ĐD' • F (7 D' •*a y,ØK sP U• , S*a ·Dê \ ² 26 kVU•*] ° Ñ? 4} % *a å D'

EFDó 2 ¼ , "wA -ß 3Đ4 | Å ,J 4}+°Kg à '¥ S U•Ô (&-ß 3Đ4 D' •+°Kg à îœ U• &/÷ ² \$ f ĐD' •Dó*a · *aC M · U•EFDó +,K 2 ¼ ² Ñ? 4} Ù 3ë9i T-ß 3Đ4 \$ f ĐD'M¢ "D' •Dó*a ·+° LD¿ '¥ S U• £ •3ÿ@æ ® 7U•

4 结论

*a ⋅ f 2 kVU•IA ⋅ ÔD'\$ fĐ ±*a |@ê 3 Ñ \%å E Ñ T Ñ \-ß c 0

lí 3 TB/T3021-2001 ′ líE• fD'D'D2*a |=ñ4š (Y0X12.2.6 •>ð Æ^[8]U•D'D©*a |@ê316) « +°, S"-",Dó

Fig.3 Over-voltage of broken contact line falling on the body of driver's cab * 3 \tilde{N} ? 4} Ù3ë9i T \$ f ĐD' ++°Dó*a ++,K" Ž

 $3\dot{a} = L\dot{U}=ce\hat{u}q\dot{O} \circ V = L\dot{U} U \cdot TJ 4F\dot{y}="LZL\dot{U}+\circ=ce\hat{u}q\dot{O} \circ - B3D4 ="LZ'$

^ fD'D©*a |@ê 3 µ " \+°E Ñ%å

参考文献:

- [] DH(·IÓ -ß3Đ4(*a94|Å+°-@/¢:À*T [+](ç)⁻IÎ 94|Å -*6% P30°/H(+VO3FTFBSDIBOE BQQMJDBUJPO PG DBSCPO GJCF\$, +]SFCCOFGP30°FDIDEGP05°ED/EEVDNUBWTEJDDFTN\$90 PPNTQIPTFJUF⁻ KITTO
- [] z FoJ7 -ß3Ð4 94 |ÅT7VUM² +°À*T [] Y)u' -* 8F(£60 2VBOCGQQMIJDBUJPO I DBSCPO GJCFS DPNQPTJŲFFT\$IUJ160 FDTFFT10QOBDVTUJD GELPNIET KITTO
- [] ...#(líC Ñ? 4}d>íÙ3ë ·qöM°K^Ö é ·@/¢ []+Y)@ê3/7 46/.JB3PFTFBSDI PO DPNN BDDJEFOUT BOE QSFWFOUJWF NFB[T+V\$\$FFJOPBG10/1381P0LLF6&OSHBU0/MFXFBS2E1690,JHP;04U6125 DU MJO 4#(-
- [] (·, líC Ñ? 4} d>í Ù3ë · q:M°K^0,*'Î/¢ [-] &0} ¬[,ý 8"/(1BO3FTFBSDIPODPNN BDDJEFOUT BOE QSFWFOUJWF TUS[B]+UF#NYZIMPEGJOOH-SF3LEFDODOSPBANJPMHXZBZ%FDWPFDNUFBODNUFFØJU EP\$J/,*46/+;,'
- [] 7ûL L;½ & ° 3ëLK4}4 + °PEKIÍC + ý"w2'4 [] VB—¥.ý':*a | →'Ñ 46 9 V F ;)"/(9JBPZ)WUOHTQFFE SBJMXBZ NPOJUPSJOH TZTUF[N] €BVEEDBPMO PXGJS5FFMS1BTIFFSTUF[O4 & MFDUSPOJD *OGPSNBUJPO 5FDEOPPIMPHZZ,:%"
- [] L9Dê ÔD'3ðsKy?D'•"--",Dó*a·2/-@/¢ [%]<F)>«fÐEFS')60%B4UVEZ PO TVSHF PWF EJTUSJCVUCJIPPEDZ PDGB107BFSE CZ QBOUPHSBQI[9%]BJ\$TTF**OH\$EBMCHEP**VEUSIPXOETQUO+HJBPPEGUB&O6H 6C EP\$5J,*\$%.%
- [] Kt,(PEKÔD'3ðsKy?®-Dó*a·Ž<f)2:½ bå"-@/¢ [%, <F)>«fÐEFS' \$)&/ 1B40UVEZ PO UIF PWFSWPMUBHF NFDIBOJTN BOE TVQQSFTTJOH NFUIPE JO UNFQNQFSBEPMAJFSTBTJOPG \$IFOH\$EEJVO4BPVUIXFTU +JBPUPOH 6OJWFSTJUZ
- [] Y))â3òBOÍ)2 "F D"E•ĐEFfD'D'D²*a |=ñ4š (# 5 [4] CØY)3ò&'t.j 4UBOEBSEJ[BUJPO "ENJOJTUSBUJPO P30BJUMIXEBZEFBPQEP400CTMB1BV19QIN\$FIQIOB WFIJD#M15T [4] #FJK4JU0BHOEBSET 1SFTT PG\$IJOB

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>@/¢ å = f*a!@2'4 Kò <@ê@ĺ *a-í¨å .emailU•	/¢ å = f 9 4 Å ¬ [*a-ík	<^Ь[.
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冯玉明(1987-)U•*cU•-• U•P 3Ó /7 4 U•g>@	/¢ å = f2'4 3Ó*a-í ¨ å ∶K^ Đ	
/¢ å = f*a-í¨å ,LŠ Ñ? Ç*a2'4 @ê@ĺ .		

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