

# PHOTONICS Research

## All dielectric metasurfaces for spin-dependent terahertz wavefront control

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Metasurfaces consisting of artificial subwavelength structure arrays have shown unprecedented ability to manipulate the phase, amplitude, and polarization of light. Separate and complete control over different spin states, namely the orthogonal circular polarizations, has proven more challenging as compared to the control over orthogonal linear polarizations. Here, we present and experimentally demonstrate several spin-dependent wavefront control metasurfaces in the terahertz regime using all-silicon dielectric structures. Such spin-dependent all-silicon metasurfaces are easy to fabricate and have potential applications in spin-involved ultracompact and miniaturized terahertz optical systems as well as terahertz communication systems.

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### 1. INTRODUCTION

The spin of a photon is the quantum mechanical counterpart of the polarization of light, and each photon of left-/right-handed circular polarized (LHCP/RHCP) light carries a spin angular momentum of  $\pm\hbar$ , where  $\hbar$  is the reduced Planck constant [1]. In addition to spin angular momentum (SAM), a photon of circular polarization can also have orbital angular momentum (OAM) which is dependent on the spatial degrees of freedom of light [2], including the intrinsic orbital angular momentum due to optical vortex within the beam and external orbital angular momentum due to the beam propagation in the transverse direction [3]. The spin-orbit interactions (SOIs) between these three types of angular momentums underpin a variety of interesting phenomena [4], including optical spin Hall effect [5–7], spin-directional coupling [8–12], and spin-dependent beam shaping [13–16], which have potential applications in quantum communication and spin-based optical elements. The underlying physical mechanism of SOI can be explained by the geometric Berry phase originating from the coupling between the SAM and the local coordinates of the media system

[17], that is, rotating the transverse  $x$ - $y$  coordinates of the inhomogeneous media induces opposite phase shifts for LHCP and RHCP incidences. Conventionally, SOIs have been studied in helical fibers [18], gratings [13], and anisotropic crystals [15]. These systems are either of low efficiency, application-limited, or bulky. Recently, metasurfaces comprising artificial subwavelength planar structures have presented unprecedented abilities to manipulate the polarization, amplitude, and phase of light [19], offering a competitive artificial platform for flexible and considerably enhanced SOI effects [4,20,21].

The building element of SOI metasurfaces is generally called a Pancharatnam–Berry optical element (PBOE) [13,22]. A perfect PBOE will completely flip the input circular polarization to its orthogonal state with an extra geometric phase shift that is double the element's orientation angle. Single layer plasmonic metasurfaces were first utilized to study SOI [16,23]. However, their power efficiency was low due to the compromise between anisotropy and transmittance [23]. To increase the SOI efficiency, multilayer plasmonic, coherently controlled, and dielectric metasurfaces have been adopted [22,24,25]. Specifically, dielectric metasurfaces consisting of high contrast dielectric

elements have recently attracted increasing research interest [26,27]. For such a dielectric element, the anisotropy is flexibly tailorable over a large range, and the material loss can be made negligible by properly selecting dielectric materials, endowing it with a significant advantage in the search for a perfect PBOE.

Besides the power efficiency, another challenge of SOI is that the inherent geometric phase shifts of a PBOE over different circularly polarized inputs are equal in magnitude with opposite signs [16]. Therefore, the achieved functionalities are limited only through the geometric phase. To make the imposed phase shifts for RHCP and LHCP inputs independent and thus the spin-control more flexible, further transport phases have been introduced by utilizing PBOEs of various geometries [28]. Through the combination of the transport phase and the geometric phase, independent and complete phase and wavefront control over orthogonal circular polarizations has been demonstrated. Such a method has greatly expanded the applications of PBOEs in polarization optics [29–31], including polarization detection [32], splitting [33], polarization contrast imaging [34], multiplexing, and encryption [35–37].

In this context, we present a design method of spin-dependent all-silicon dielectric metasurfaces by simultaneously involving the geometric phase and transport phase in the constituting PBOEs. The PBOEs are anisotropic rectangular posts distributed in a tetragonal lattice on silicon substrate. Two functional metasurface devices are designed and experimentally characterized in the terahertz regime, including a spin-selective Bessel/half-wave metasurface device and a spin-dependent Bessel/vortex beam generator. The Bessel/half-wave metasurface generates a cross-polarized Bessel beam under the LHCP incidence, whereas it only flips the polarization under the RHCP incidence. The Bessel/vortex beam generator produces Bessel and vortex beams separately under the LHCP and RHCP incidences. Such metasurface devices have the potential to help realize miniature THz systems, with key applications in spin switching, contrast imaging, coding, and encryption.

## 2. DESIGN STRATEGY

A perfect PBOE functions as a half-wave plate, i.e., there is a  $180^\circ$  phase difference between the phase shifts along the local fast and slow axes of the PBOE. The corresponding rotated transmission matrix in the Cartesian coordinate system can be expressed as [33]

$$\begin{aligned} \mathbf{T} &= \begin{bmatrix} t_{xx} & t_{xy} \\ t_{yx} & t_{yy} \end{bmatrix} = t_0 \mathbf{R}(-\alpha) \begin{bmatrix} 1 & 0 \\ 0 & -1 \end{bmatrix} \mathbf{R}(\alpha) \\ &= t_0 e^{i\varphi_f} \begin{bmatrix} \cos(2\alpha) & \sin(2\alpha) \\ \sin(2\alpha) & -\cos(2\alpha) \end{bmatrix}. \end{aligned} \quad (1)$$

Here, the former and latter subscripts of the transmission coefficient  $t_{ij}$  ( $i, j = x, y$ ) indicate the polarization directions of the output and input lights, respectively;  $t_0$  is the transmission amplitude along the two eigen axes, fast ( $f$ ) and slow ( $s$ );  $\varphi_f$  is the transport phase shift along the fast axis; and

$\mathbf{R}(\alpha) = \begin{bmatrix} \cos(\alpha) & \sin(\alpha) \\ -\sin(\alpha) & \cos(\alpha) \end{bmatrix}$  is the rotation matrix, in which  $\alpha$  denotes the rotation angle of the PBOE's local fast axis with

respect to the  $x$  coordinate. To directly study the spin-dependent response of the PBOE, it is required to further transfer the above matrix into the circular polarization base

$$\begin{aligned} \mathbf{T}_c &= \begin{bmatrix} t_{ll} & t_{lr} \\ t_{rl} & t_{rr} \end{bmatrix} = t_0 \begin{bmatrix} 0 & e^{i(\varphi_f - 2\alpha)} \\ e^{i(\varphi_f + 2\alpha)} & 0 \end{bmatrix} \\ &= t_0 \begin{bmatrix} 0 & e^{i\Phi_{lr}} \\ e^{i\Phi_{rl}} & 0 \end{bmatrix}, \end{aligned} \quad (2)$$

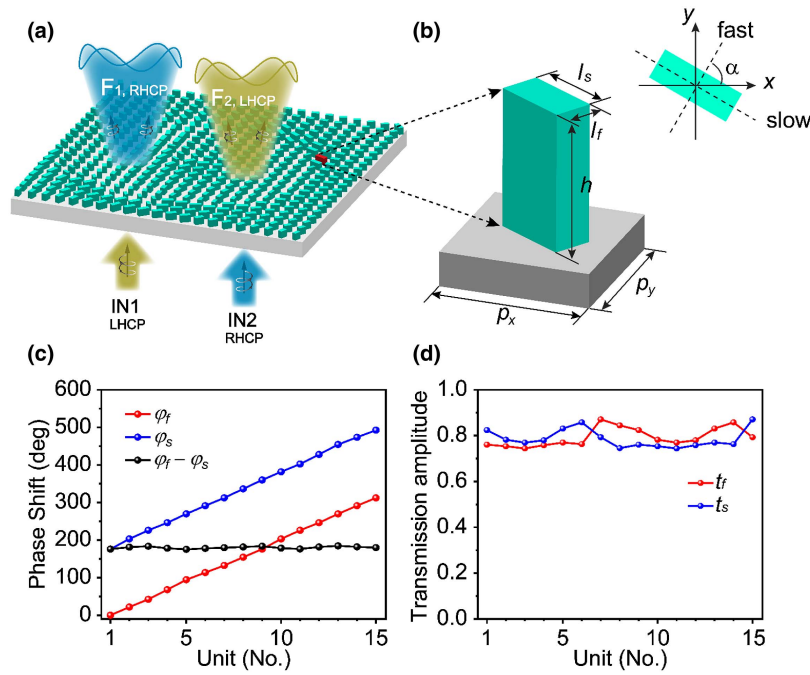
where the subscripts  $l$  and  $r$  indicate LHCP and RHCP, respectively. It is easily seen from Eq. (2) that, with a perfect PBOE, the LHCP light can be completely converted to RHCP light and vice versa. The overall phase shift  $\Phi_{lr}$  for the RHCP incidence equals  $\varphi_f - 2\alpha$ , and the overall phase shift  $\Phi_{rl}$  for the LHCP incidence equals  $\varphi_f + 2\alpha$ . In addition to the geometric phase terms  $2\alpha$  and  $-2\alpha$  determined by the rotation angle, the output phase shifts for the LHCP and RHCP incidences also contain the transport phase term  $\varphi_f$ , which is determined by the dimensions of the PBOE element. This provides an effective freedom in decoupling the overall output phases  $\Phi_{lr}$  and  $\Phi_{rl}$ . With the desired  $\Phi_{lr}$  and  $\Phi_{rl}$ , the corresponding required transport phase  $\varphi_f$  and rotation angle  $\alpha$  can be obtained as

$$\varphi_f = \frac{\Phi_{rl} + \Phi_{lr}}{2}, \quad (3a)$$

$$\alpha = \frac{\Phi_{rl} - \Phi_{lr}}{4}. \quad (3b)$$

Thus, by varying  $\varphi_f$  and  $\alpha$  of the PBOEs, complete and independent control over the orthogonal circular polarizations can be achieved. As  $\varphi_f$  is determined by the geometric parameters, PBOEs of different dimensions are needed to achieve independent phase patterns  $\Phi_{lr}$  and  $\Phi_{rl}$ . Therefore, two key criteria should be taken into consideration: (1) a  $180^\circ$  phase difference between the two local axes with equal transmission amplitudes for every single PBOE is required to ensure perfect cross polarization conversion, and (2) the relative transport phase shifts  $\varphi_f$  of the PBOEs need to enable the complete  $360^\circ$  phase coverage of  $\Phi_{lr}$  and  $\Phi_{rl}$ .

Based on our previous work [33,38], we employ high-resistivity silicon rectangular posts distributed in a periodic tetragonal lattice on the same silicon substrate to realize the above PBOEs. The schematic of a spin-dependent metasurface consisting of the above PBOEs is shown in Fig. 1(a). The metasurface flips the input spin state from LHCP/RHCP to RHCP/LHCP and imparts independent wavefront control functions  $F_1/F_2$  at the same time. Figure 1(b) shows the zoomed-in schematic of a single rotated PBOE marked by the red rectangular posts in Fig. 1(a). The periods are  $p_x = p_y = 150 \mu\text{m}$ . The inset of Fig. 1(b) shows the rotation operation of the PBOE in the  $x$ - $y$  polarization base. The rectangular posts are of constant height  $h = 200 \mu\text{m}$  but of varying  $l_f$  and  $l_s$  dimensions. Here, the center operating frequency is set to 1.0 THz. To achieve an  $n$ -level phase discretization with a phase increment of  $360^\circ/n$  for both  $\Phi_{lr}$  and  $\Phi_{rl}$ , the corresponding increment of  $\varphi_f$  can be calculated as  $180^\circ/n$  from Eq. (3a), and  $2n - 1$  PBOEs of various geometric parameters



**Fig. 1.** (a) Schematic of the spin-dependent metasurface, which consists of PBOEs and can generate two arbitrarily designable beam functions,  $F_1$  and  $F_2$ , under orthogonally circularly polarized incidences. (b) Schematic of a rotated constituent PBOE marked by the red rectangular post in (a). (c) and (d) The simulated transport phase shifts and the corresponding transmission amplitudes of all the 15 PBOEs.

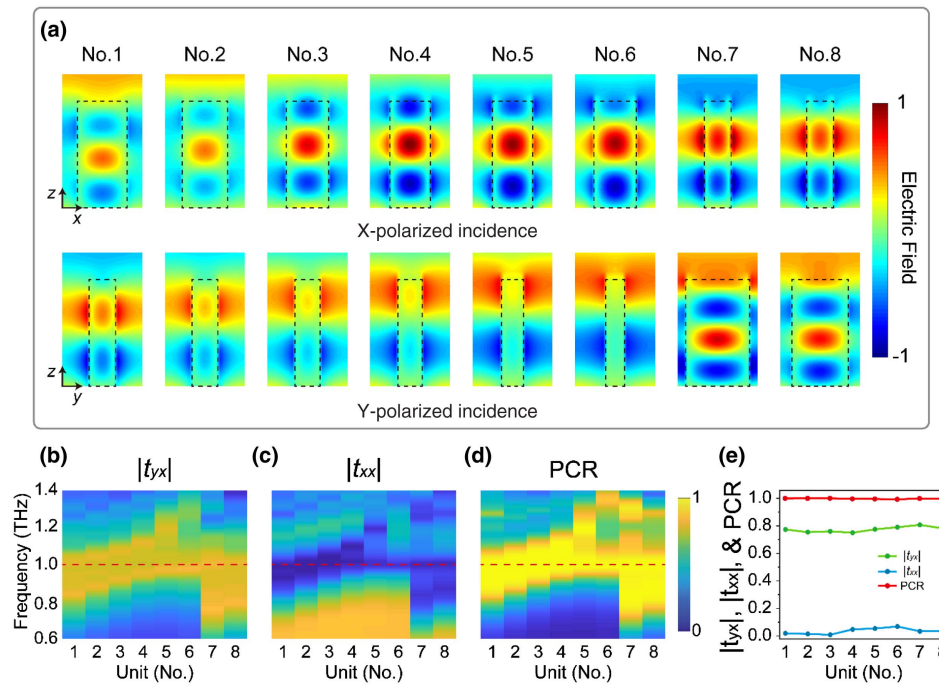
are required. Meanwhile, the localized orientation angles are integer multiples  $90^\circ/n$  and within an open interval  $(-90^\circ, 90^\circ)$ . Due to the structure symmetry of the post,  $\varphi_f$  and  $\varphi_s$  are symmetric in the local coordinate system about  $f = s$ . Therefore, the real quantity of the PBOEs can be simplified to  $n$ . The other  $n - 1$  PBOEs can be obtained by successively rotating the first  $n - 1$  fundamental PBOEs by  $90^\circ$ . With  $n = 8$  as an example, here, the geometric dimensions of the selected 15 PBOEs are given in Table 1, which contain 8 fundamental PBOEs (No. 1 to No. 8). Figure 1(c) illustrates the simulated transport phase shifts  $\varphi_f$  (the red dotted line) and  $\varphi_s$  (the blue dotted line) of all the selected PBOEs with  $\alpha = 0^\circ$ . The simulation details are shown in Appendix A. The black dotted line gives the corresponding phase deviations  $\varphi_f - \varphi_s$ . It can be seen that the phase deviations are all very close to  $180^\circ$ . Meanwhile, the corresponding transmission amplitudes are also calculated, as shown in Fig. 1(d), which all remain at a high level around 0.8, indicating a high working

efficiency. These amplitudes are obtained by taking the square root of the intensity transmittances of the terahertz waves from the silicon substrate across the posts to the air. These results imply that all the selected elements can serve as efficient PBOEs.

To further investigate the phase control and cross-polarization conversion performances of the 8 fundamental PBOEs, the electric field distributions at 1.0 THz are simulated, as shown in Fig. 2(a). It can be seen that the output phases of  $E_x$  and  $E_y$  are out of phase in each PBOE, and both of them gradually change by  $180^\circ$  from No. 1 to No. 8. As for the last 7 PBOEs (No. 9 to No. 15), the corresponding simulated electric field distributions under  $x$ - and  $y$ -polarized incidences are the same as those of the first 7 PBOEs under  $y$ - and  $x$ -polarized incidences. Figures 2(b) and 2(c) illustrate the simulated transmission amplitude spectra  $|t_{yx}|$  and  $|t_{xx}|$  of the 8 fundamental PBOEs, whereas Fig. 2(d) illustrates the corresponding polarization conversion rates (PCRs) calculated by

**Table 1. Geometrical Parameters and Relative  $\varphi_f$  of the Selected 15 PBOEs**

No.	$\varphi_f$ (deg)	$l_f$ ( $\mu\text{m}$ )	$l_s$ ( $\mu\text{m}$ )	No.	$\varphi_f$ (deg)	$l_f$ ( $\mu\text{m}$ )	$l_s$ ( $\mu\text{m}$ )
1	0	93.5	50	9	180	50	93.5
2	22.5	85.5	49	10	202.5	49	85.5
3	45	80	47.5	11	225	47.5	80
4	67.5	76	45.5	12	247.5	45.5	76
5	90	75.5	41.5	13	270	41.5	75.5
6	112.5	80	35.5	14	292.5	35.5	80
7	135	50	120	15	315	120	50
8	157.5	50	106				



**Fig. 2.** (a) Simulated electric field distributions of  $E_x$  (top row, in the  $x$ - $z$  cross section) and  $E_y$  (bottom row, in the  $y$ - $z$  cross section) at 1.0 THz of the 8 fundamental PBOEs under  $x$ - and  $y$ -polarized incidences, respectively. (b) and (c) Simulated transmission amplitude spectra  $|t_{yx}|$  and  $|t_{xx}|$  of the 8 fundamental PBOEs (No.1 to No.8) with  $\alpha = 45^\circ$  under the  $x$ -polarized incidence. (d) Calculated PCR of the 8 fundamental PBOEs. (e) Extracted  $|t_{yx}|$ ,  $|t_{xx}|$ , and PCR values at 1.0 THz.

$|t_{yx}|^2 / (|t_{yx}|^2 + |t_{xx}|^2)$ . It can be seen that the  $y$ -polarized (cross-polarized) transmissions are obviously larger than those of the  $x$ -polarized (co-polarized) transmissions at around 1.0 THz for all PBOEs, where the PCRs all nearly approach 1. To show the cross-polarization conversion performances more clearly, the corresponding  $|t_{yx}|$ ,  $|t_{xx}|$ , and PCR values at 1.0 THz marked by the dashed red lines are extracted in Fig. 2(e).

### 3. RESULTS AND DISCUSSION

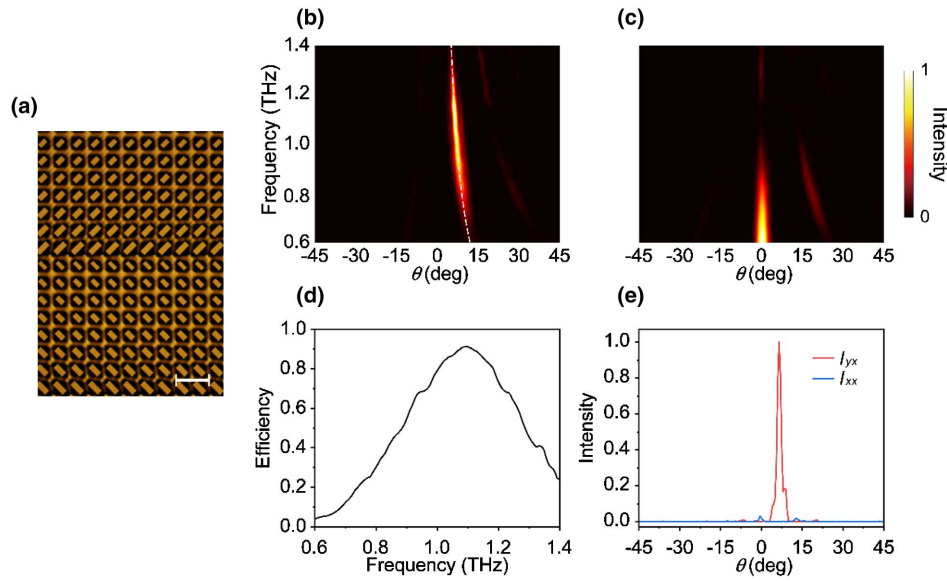
To experimentally verify that the selected PBOEs meet the two criteria, i.e., perfect cross-polarization conversion and complete phase coverage, a polarization conversion deflector (PCD) is first constructed by patterning the PBOEs into a linear phase distribution along the  $x$ -axis. To enable the complete phase coverage of  $360^\circ$  with a phase increment of  $22.5^\circ$ , the super unit cell comprises 16 PBOEs of which the corresponding phase shifts range from  $0^\circ$  to  $337.5^\circ$  in sequence. Therefore, the periods are  $D_x = 16p_x = 2.4$  mm along the  $x$ -direction and  $p_x = 0.15$  mm along the  $y$ -direction. The orientation angles of all the PBOEs are  $45^\circ$ . Deep reactive ion etching process is employed for the fabrication; see Appendix B. The total size of the fabricated PCD sample is  $9.6$  mm  $\times$   $9.6$  mm, which is the same for all devices in this work. Figure 3(a) shows the optical microscope image of the fractional PCD sample.

The PCD was then characterized using our customized all-fiber terahertz time-domain spectrometer (TDS) system [38]. For bandwidth characterization and simplicity, a linearly polarized input is used here. Figures 3(b) and 3(c) show the measured  $y$ - and  $x$ -polarized outputs under  $x$ -polarized input. It can

be seen that almost all the  $x$ -polarized input is converted to  $y$ -polarized light and deflected to the  $+1$ st diffraction order, which confirms both the ability to achieve a full phase coverage and the  $180^\circ$  phase difference between  $\varphi_f$  and  $\varphi_s$ . Notably, the PCD also supports broadband operation. To illustrate the bandwidth, the power efficiency as a function of frequencies is shown in Fig. 3(d). Here, the power efficiency is defined as the ratio of the output power at the desired polarization and diffraction order to the overall output power. Figure 3(d) highlights that the maximum power efficiency is about 91% and appears at 1.1 THz. The deviation of this operating frequency from the design is likely due to fabrication accuracy. Thus, we focus on the following device performance at 1.1 THz. Figure 3(e) shows the measured normalized intensity curves of the  $x$ - and  $y$ -polarized outputs at 1.1 THz. The measured deflection angle is  $\theta_d = 6.5^\circ$ , which coincides with the general Snell's law  $\theta_d = \arcsin(\lambda/D_x)$  [39].

From the measured results of the PCD, it can be concluded that the selected basic PBOEs can well satisfy our requirements in achieving efficient and independent control over the complete phases of the orthogonal circular polarizations at 1.1 THz. Following the above experimental confirmation, we further fabricate two functional devices.

One is a Bessel/half-wave metasurface, which serves as a Bessel generator under the LHCP incidence but as a half-wave plate under the RHCP incidence. To generate the Bessel beam under the LHCP incidence, a linear gradient of  $\Phi_{rl}$  along the polar coordinate is required, assembling the conventional axicon phase distribution. Therefore,  $\Phi_{rl} = 2\pi\rho \arcsin(\theta_B)/\lambda$  [40]. Here,  $\rho$  is the polar coordinate, and  $\theta_B$  indicates the

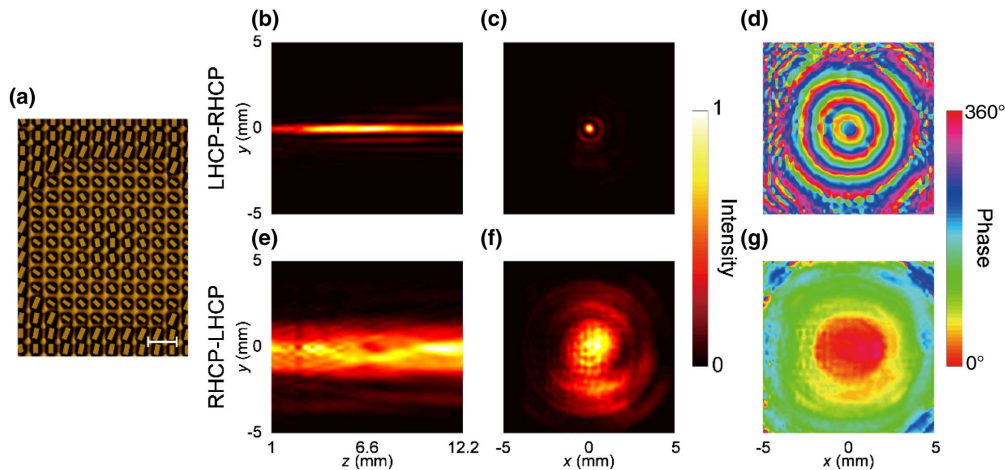


**Fig. 3.** (a) Microscopic image of the fabricated PCD. Scale bar: 300 μm. (b) and (c) The measured normalized intensity distributions as a function of the diffraction angle and the frequency of the  $y$ - and  $x$ -polarized outputs under  $x$ -polarized input, respectively. The white dashed line in (b) indicates the theoretical angles for the +1st diffraction order. (d) The power efficiency of the PCD. The maximum power efficiency appears at 1.1 THz. (e) The normalized intensity profiles of  $x$ - and  $y$ -polarized output at 1.1 THz.

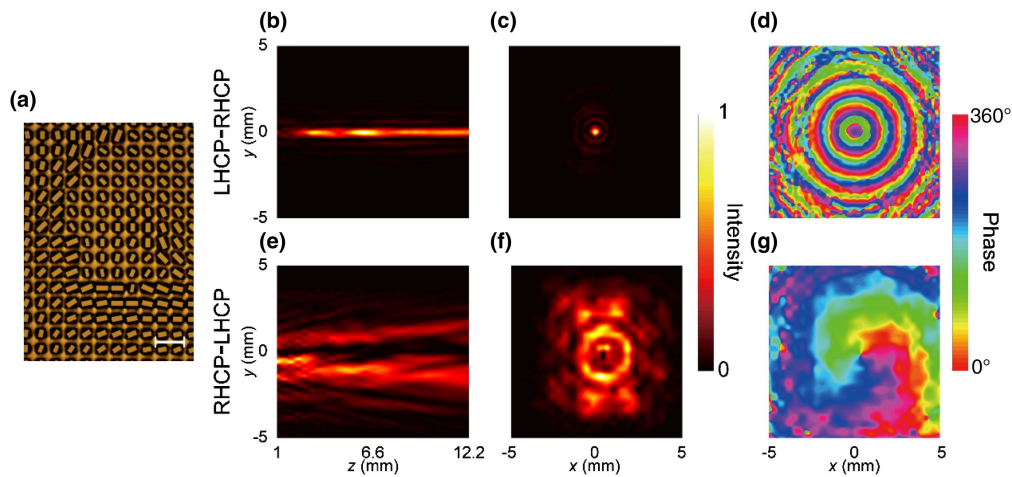
deflection angle of the output light with regards to the optical axis and is dependent on the radial span  $P$  of the  $360^\circ$  phase coverage along the polar direction by  $\theta_B = \arcsin(\lambda/P)$ .

Meanwhile, attributing to the inherent cross-polarization conversion function of the PBOE metasurface,  $\Phi_{lr}$  does not need any localized alteration but keeps a constant  $C$ . Then, the metasurface can be constructed with the selected PBOEs of the transport phase  $\varphi_f = \pi\rho \arcsin(\theta_B)/\lambda + C/2$  and the rotation angle  $\alpha = \pi\rho \arcsin(\theta_B)/(2\lambda) - C/4$ . Figure 4(a) shows the optical microscope image of the fabricated Bessel/half-wave metasurface for which  $P$  is set as 1.24 mm. The

metasurface was characterized by a fiber-based near-field scanning THz microscopy (FNSTM) [41]. Figure 4(b) illustrates the measured normalized RHCP intensity profile in the longitudinal plane  $x = 0$  under the LHCP incidence from the substrate side. It is clearly seen that there is a typical diffraction-free feature in a distance longer than  $30\lambda$  along the propagation direction. The transverse normalized intensity and phase profiles at 8 mm above the metasurface are also measured, as shown in Figs. 4(c) and 4(d). Both profiles show typical Bessel features: an intense central spot is surrounded by weak concentric rings due to the limited size of the metasurface, and an almost



**Fig. 4.** (a) Microscopic image of a fraction of the fabricated Bessel/half-wave metasurface. Scale bar: 300 μm. (b)–(d) The measured normalized RHCP intensity distributions at the longitudinal propagation plane at  $x = 0$  and the intensity and phase profiles at the transverse plane at  $z = 8$  mm under the LHCP incidence. (e)–(g) The corresponding measured LHCP distributions under the RHCP incidence. In the measurement, the longitudinal plane spans from  $-5$  to  $5$  mm along the  $y$ -direction and  $1$  to  $12.2$  mm along the  $z$ -direction, whereas the transverse plane spans from  $-5$  to  $5$  mm along both the  $x$ - and  $y$ -directions. The scanning steps are  $0.2$ ,  $0.2$ , and  $0.4$  mm along the  $x$ -,  $y$ -, and  $z$ -directions, respectively.



**Fig. 5.** (a) Microscopic image of a fraction of the fabricated Bessel/vortex metasurface. Scale bar: 300  $\mu\text{m}$ . (b)–(d) The measured normalized RHCP intensity distributions at the longitudinal propagation plane at  $x = 0$ , and the intensity and phase profiles at the transverse plane at  $z = 5$  mm under LHCP incidence. (e)–(g) The corresponding measured LHCP distributions under the RHCP incidence, in which the transverse plane is at  $z = 8$  mm.

linear phase gradient along the radial direction. Under the RHCP incidence, the measured longitudinal normalized LHCP intensity, and the transverse normalized intensity and phase profiles are shown in Figs. 4(e)–4(g). It can be observed that the beam keeps propagating as a Gaussian-type wave. Thus, under the RHCP incidence, the metasurface only performs the cross-polarization conversion function as a half-wave plate.

The second device is a Bessel/vortex metasurface, which is capable of producing Bessel and vortex beams separately by switching between the LHCP and RHCP incidences. The Bessel beam for the LHCP input is designed to the same specifications as the former device, while the first-order vortex beam for the RHCP input is designed with a topological charge  $+1$  by  $\Phi_{lr} = \theta$  [42], where  $\theta$  is the azimuthal angle. Using the same design principle, we can obtain the  $\varphi_f$  and  $\alpha$  required to be patterned on the metasurface. Figure 5(a) shows the optical microscope image of the fabricated sample. Under the LHCP incidence, the measured normalized RHCP longitudinal normalized intensity profile at  $x = 0$  is illustrated in Fig. 5(b). Figures 5(c) and 5(d) illustrate the transverse intensity and phase profiles at  $z = 5$  mm. Similar Bessel features are observed as those seen in Figs. 4(b), 4(c), and 4(d). Figure 5(e) illustrates the measured normalized LHCP longitudinal intensity profile at  $x = 0$ , and Figs. 5(f) and 5(g) illustrate the transverse intensity and phase profiles at  $z = 8$  mm, under the RHCP incidence. Two distinct divergent lobes can be seen from the longitudinal propagation plane, in which the intensity along their central line is almost 0. Meanwhile, the transverse intensity profile in Fig. 5(f) presents a doughnut spot, and the phase profile presents a helical phase of  $360^\circ$  encircling the phase singularity at the center. These features coincide with the  $+1$ st vortex beam as expected.

#### 4. CONCLUSION

Terahertz all-silicon dielectric metasurfaces for spin-dependent and complete wavefront control are realized using PBOEs

through introducing extra geometry inhomogeneity besides the rotation inhomogeneity. In this work, a simplified design strategy is utilized to facilitate the metasurface design attributing to the structure symmetry. Based on the simplified design, several exemplary metasurfaces are accomplished using the minimized fundamental constituting elements. One is used to confirm the performance of the selected PBOEs, while the other two metasurfaces demonstrate functional devices—a Bessel/half-wave metasurface and a Bessel/vortex metasurface. The measured results agree well with our design. Such dielectric metasurfaces are easy to fabricate, compatible with semiconductor integration, and have promising applications in ultra-compact and spin-involved optical terahertz imaging system and communication systems for polarization contrast imaging, coding, and encryption.

#### APPENDIX A: SIMULATION METHODS

To select the proper PBOEs, CST Microwave Studio is used to simulate the transmissions (including amplitude and shift) of the silicon posts, in which we set  $\alpha = 0^\circ$  and raster scan the lateral dimensions  $l_f$  and  $l_s$ . Periodic boundaries are applied along the  $x$ - and  $y$ -directions. Plane waves of  $x$  and  $y$  polarizations separately illuminate the structure layer from the substrate side. The corresponding outputs are detected using probes positioned at the far-field on the air side. After getting all the simulated transmissions, we selected the proper 15 PBOEs required for an 8-level phase control at 1.0 THz; see Table 1. The presented phase shifts in Fig. 1(c) are plotted by taking the  $\varphi_f$  of the first PBOE ( $l_f = 93.5 \mu\text{m}$ ,  $l_s = 50 \mu\text{m}$ ) as the reference, as it is the relative phase shifts that matter for the polarization and wavefront control. The electric field distributions in Fig. 2(a) are obtained by setting the field monitor at 1.0 THz in simulation.

#### APPENDIX B: SAMPLE FABRICATION

The silicon dielectric metasurfaces were fabricated using conventional photolithography and deep reactive ion etching

(DRIE) [43]. The silicon wafer used here is a  $\langle 100 \rangle$ -orientation, double-side-polished, high-resistivity (resistivity  $> 10000 \Omega \cdot \text{cm}$ ) 1-mm-thick wafer. First, the wafer was cleaned using a standard Radio Corporation of America (RCA) process. Next, a thin layer of photoresist (AZ460) was spun on the wafer at 3000 r/min for 40 s and baked at  $120^\circ\text{C}$  for 2 min. After that, conventional photolithography was performed to transfer the pattern from a predesigned quartz-chrome mask to the photoresist. Subsequently, the wafer was developed in a developer (400 K) for 18 s. After rinsing it in ultra-pure water for 20 min, the remained photoresist pattern was again baked at  $120^\circ\text{C}$  for 2 min. Then, the unprotected silicon parts were etched with a depth of  $200 \mu\text{m}$  using an inductive coupled plasma etcher (Sentech, ICP-RIE SI 500). Finally, the residual photoresist was chemically removed with an acetone and methyl alcohol solution.

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**Disclosures.** The authors declare no conflicts of interest.

**Data Availability.** Data underlying the results presented in this paper may be obtained from the authors upon reasonable request.

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