PHOTONICS Research

Continuous-wave operation of 405 nm distributed Bragg reflector laser diodes based on GaN using 10th-order surface gratings

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Single longitudinal mode continuous-wave operation of GaN-based distributed Bragg reflector (DBR) laser diodes with 10th-order surface gratings is demonstrated. The DBR consists of periodic V-shaped grooves on a 2 μ m wide ridge waveguide fabricated by using electron-beam lithography and plasma etching. The effect of different lengths of the DBR section and the gain section on the device performance has been studied. Periodic mode hops to the adjacent longitudinal Fabry–Perot resonator mode at shorter wavelength have been observed when increasing the operation current. Between the mode hops, single longitudinal mode emission at around 405 nm is achieved with a full width at half-maximum of 0.03 nm. A linear redshift of the emission wavelength with increasing temperature of 0.019 nm/K was derived. © 2022 Chinese Laser Press

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1. INTRODUCTION

Gallium nitride (GaN)-based laser diodes with narrowband emission in the blue-violet spectral region are interesting light sources for many applications such as atom spectroscopy, atomic clocks, medical diagnostics, and optical communication [1-5]. Compact single-mode laser diodes can be realized as distributed feedback (DFB) or distributed Bragg reflector (DBR) laser diodes. Comparing these two designs, the DBR laser has the advantages of (i) a reduced sensitivity against unwanted external feedback [6] and (ii) that lateral mode confinement and light amplification can be spatially separated from mode selection via grating dispersion. Moreover, the DBR concept allows lasers with relatively short resonator lengths to be realized despite large chip lengths. While the short resonator length leads to a low threshold current and a large differential efficiency, a large chip length simplifies laser fabrication in terms of cleaving laser facets and their dielectric coating [7,8]. Nevertheless, only few studies on GaNbased DBR laser diodes operating under pulsed condition have been published. DBR lasers with third-order surface gratings emitting at 401.3 nm have been reported [9]. The devices contained a 3 µm wide and 500 µm long ridge as gain section between 250 µm long grating sections, which were defined on the exposed cladding layer using holography. A threshold current density of 25 kA/cm² has been achieved with single peak emission and a linewidth of 0.04 nm. Dumitru et al. reported on DBR lasers emitting at 407.5 nm using a second-order surface grating defined by electron-beam lithography [10]. A threshold current density of 66 kA/cm² was achieved for a 2 μ m wide and 500 μ m long ridge as the gain section and 500 μ m long gratings at both ends of the ridge, which provided laser emission in the vertical direction. Single peak emission in the temperature range from 10°C to 70°C has been shown with a wavelength shift of 0.0119 nm/K. Xie *et al.* reported on DBR lasers with 3rd-, 13th-, and 19th-order surface gratings defined by electron beam lithography [11]. The devices contained 10 μ m wide and 800 μ m long ridges as the gain section and a 155 μ m long grating section with a 19th-order surface grating. It showed 500 mA of threshold current, 0.156 W/A of slope efficiency, and single peak emission with a linewidth of 0.45 nm at around 400 nm. We are not aware of any publication reporting on the continuous-wave (CW) operation of GaN-based DBR laser diodes.

Recently, we have successfully developed the technology for 10th-order V-shaped surface Bragg gratings on GaN, which can replace buried gratings that require a sophisticated two-step epitaxy [12–14]. The feasibility of these surface gratings has been qualified by successful demonstration of DFB laser diodes operating under CW condition [15]. In this paper, the CW operation of GaN-based DBR laser diodes using corresponding surface gratings is reported. The devices show single longitudinal mode emission with typical periodic mode hops and a temperature dependence of the emission wavelength similar to GaN-based DFB laser diodes.

2. SIMULATIONS

Detailed simulations of 10th-order surface gratings with varying residual layer thickness from the topmost quantum well and duty cycle of the grating have been presented in our previous work [12,13]. In this paper, the reflectivity and the loss of 10thorder V-shaped surface Bragg gratings in dependence of the length L_{DBR} of the DBR were calculated for different optical losses using the bidirectional mode expansion tool CAMFR [16]. The laser structure in this experiment comprised a 1 μ m thick Al_{0 12}Ga_{0 88}N:Si/GaN:Si superlattice with a period of 5 nm as lower cladding layer, a lower waveguide of 75 nm GaN:Si and 60 nm In_{0.01}Ga_{0.99}N:Si, a three-fold multiple quantum well with 3.5 nm thick In_{0.1}Ga_{0.9}N wells and 7 nm thick In_{0.01}Ga_{0.99}N:Si barriers, 60 nm In_{0.01}Ga_{0.99}N as the first upper waveguide layer, a 20 nm Al_{0.16}Ga_{0.84}N:Mg electron blocking layer, a 45 nm thick GaN:Mg second upper waveguide layer, a 520 nm thick Al_{0.12}Ga_{0.88}N:Mg/ GaN:Mg superlattice with a period of 5 nm as the upper cladding layer, and an 80 nm GaN:Mg cap layer [15]. The V-shaped grooves were assumed to have a slant angle of 20°, a residual layer thickness of 75 nm, a tip width of 10 nm, and a period of 802 nm. Moreover, the gratings are assumed to be infinitely extended into the lateral direction and covered by SiO₂. One should note here the differences between the simulated grating geometry and the real one described later. The real grating is 1.5 µm wide on a 2 µm wide ridge, i.e., it is not laterally infinitely extended. Nevertheless, the simulations should be suitable to predict reasonable lengths of the DBR section and expected trends for the experiment. As expected, Fig. 1(a) shows that with increasing grating length the peak in the reflectance spectrum becomes narrower but hardly changes its position. Figures 1(b)-1(d) show the maximum DBR reflectivity as well as loss and transmission at the corresponding wavelength as a function of L_{DBR} for varying modal absorption α , which was assumed to be the same for all layers.



Fig. 1. (a) Reflection spectrum for $\alpha = 30 \text{ cm}^{-1}$, (b) maximum reflectivity, (c) loss, and (d) transmission of 10th-order DBR sections with V-shaped grooves (assuming a laterally infinite grating) as a function of the length of the DBR section for different values of an additional modal absorption α .

The absorption accounts for free-carrier, defect, and interband absorption, the absolute magnitude of which is not precisely known. Thus, the computed loss results from the radiation loss inherent to higher-order Bragg gratings and the additional modal absorption, which further decreases the reflectivity. The large slant angle of the grooves (20°) already results in radiation losses of more than 40%, and the DBR reflectivity does not increase for L_{DBR} greater than 100 µm.

3. EXPERIMENTS

The group-III nitride laser heterostructure was grown on 2" GaN (0001) substrates using metalorganic vapor phase epitaxy. The p-type Mg-doped layers were activated by annealing the wafers in oxygen-containing ambient. Except for the surface gratings, i-line stepper lithography was used throughout the chip processing. A 2 μ m wide and (650 \pm 10) nm high ridge was fabricated along the whole 600 µm long chip using plasma etching. As shown in Fig. 2(a), the ridge consists of an unpumped DBR section and a pumped gain section. The ratio $L_{\rm DBR}/L_{\rm gain}$ of the corresponding lengths has been varied as follows: 50/550, 100/500, and 200/400 (length in µm). 1.5 µm wide Pd/Pt p-contact stripes were fabricated on the gain section only. Tenth-order surface gratings with 802 nm period were written on the DBR section of the ridge with 0.25 µm distance from its edges employing electron-beam lithography and plasma etching as shown in Fig. 2(b). The grooves have an



Fig. 2. (a) Schematic side view of a DBR laser diode consisting of a gain section and a DBR section; top-view scanning electron microscope images of (b) the DBR laser chip before the SiO_2 deposition and (c) the 10th-order surface gratings with V-shaped grooves.

opening width at the surface of (430 ± 10) nm, a depth of (650 ± 10) nm, a slant angle of 20°, and a tip width of ~ 10 nm [see Fig. 2(c)]. The DBR section was passivated using 300 nm thick SiO₂. The rest of the chip process followed standard procedures. The laser chips were provided with an antireflection coating ($R_{AR} < 0.2\%$) on the rear facet (DBR section) and a low-reflection coating ($R_{LR} = 25\%$) on the front facet (gain section). They were soldered p-side up on CuW submounts again soldered on Ni/Au-plated copper heat sinks, so called C-mounts. All measurements were performed under CW operation in normal laboratory atmosphere. The light output power and voltage versus current (L-I-V) characteristics of the laser diodes from the rear and front facets were measured, keeping the C-mount temperature at 20°C. High-resolution emission spectra at variable temperature and current were measured with an optical spectrum analyzer (Yokogawa AQ6373), providing a resolution limit of 0.02 nm.

4. RESULTS

Figure 3 shows the L-I-V characteristics of the DBR laser diodes of different L_{DBR} with the power measured from both facets. It should be mentioned that the lasers were not burned in before the measurement and, during the initial CW operation especially, the bias changes slightly. This explains the differences between the *I-V* curves in Figs. 3(a) and 3(b). Changes in optical power due to burn-in effects or degradation are small



Fig. 3. Optical power-current-voltage characteristics of DBR laser diodes with L_{DBR} of 50, 100, and 200 μ m for emission from (a) the front facet and (b) the rear facet.

compared to the differences between lasers with DBR gratings of different lengths discussed below. The threshold current of the DBR laser diodes does not significantly depend on L_{DBR} and is in the range (85 ± 15) mA. The average threshold current density (threshold current over ridge area) and the average slope efficiency of several nominally identical DBR laser diodes were determined to be (8.2 ± 1.0) kA/cm² and (0.26 ± 0.04) W/A, respectively, for $L_{\text{DBR}} = 50 \,\mu\text{m}$; (8.3 ± 0.8) kA/cm² and (0.33 ± 0.04) W/A, respectively, for $L_{\text{DBR}} = 100 \,\mu\text{m}$; and (10.0 ± 1.3) kA/cm² and (0.42 ± 0.07) W/A, respectively, for $L_{\text{DBR}} = 200 \,\mu\text{m}$. The increased average threshold current density with increasing L_{DBR} and hence decreasing $L_{\text{gain}} = L_{\text{chip}} - L_{\text{DBR}}$ could be attributed to enhanced mirror losses α_{m} , given by

$$\alpha_{\rm m} = \frac{1}{L_{\rm gain}} \ln \frac{1}{\sqrt{R_{\rm f} \cdot R_{\rm DBR}}}$$

Here, L_{chip} is the constant chip length, $R_f = R_{LR}$ is the reflectivity of the front facet, and R_{DBR} is the reflectivity of the DBR section. The observed laser output power jump at the threshold indicates the presence of a saturable absorber in the unpumped DBR section, which results in a hysteresis and bistable laser behavior. Based on simulations, a DBR section longer than 50 µm should provide a mode reflectivity larger than 0.28 (when the modal absorption is lower than 100 cm⁻¹), which is independent of the DBR section length. Therefore, increasing the DBR section length ($L_{\text{DBR}} > 50 \ \mu\text{m}$) would be equivalent to reducing the effective resonator length alone, and the slope efficiency at the front facet should increase. This fits the experimental data. However, the ratios of output powers from the rear facet and the front facet (P_r/P_f) measured at 30% above threshold of the DBR laser diodes with the L_{DBR} of 50, 100, and 200 µm were 1.23, 0.62, and 0.13, respectively. The continued decrease of P_r/P_f , even for large values of L_{DBR} , is unexpected. Furthermore, the DBR laser diode with L_{DBR} of 50 µm showed multi-peak emission (not shown here). This suggests that the 50 µm long DBR section does not operate as a wavelength-selective mirror as intended and that its reflectivity is lower than that of the front facet ($R_{LR} = 0.25$). Moreover, both the 100 µm long and 200 µm long DBR sections showed higher rear facet emission than expected by simulations. Similarly unexpected is the fact that the 100 µm long DBR section shows an around 5 times higher P_r/P_f than the 200 µm long DBR section. The differences between simulation and experiment could result from structural imperfections of the fabricated gratings, which are associated with optical losses, or from simplifications of the grating structure in simulations. In reality, the grating is not laterally infinitely extended but even somewhat narrower than the ridge. Therefore, the simulations probably overestimate the reflectivity of the grating and underestimate its losses.

DBR laser diodes with $L_{\text{DBR}} > 100 \,\mu\text{m}$ showed periodic steps of the output power, indicating mode hops known from other DBR lasers [17–20]. When the current is increased, the output power seems to level off first before finally a mode hop occurs as shown in Fig. 4(a). The effect can be attributed to a change of the difference in temperature and, therefore, in refractive index between the gain section and the DBR section



Fig. 4. (a) Output power-current characteristic and (b) 2D colormap of emission spectra at different currents of a DBR laser diode with L_{DBR} of 200 µm measured at the front facet. Inset: high-resolution emission spectra of the DBR laser diode at 105 mA.

when increasing the current. With increase of the current, the gain section heats up stronger than the DBR section, and the modal gain spectrum shifts to longer wavelengths while the reflectivity spectrum of the grating is rather fixed. Thus, the slope efficiency decreases when the lasing mode is increasingly shifted away from the maximum of the reflectivity spectrum of the DBR section until lasing hops to the adjacent shorter wavelength mode. This is confirmed by an overall redshift of the lasing wavelength with a wavelength tuning coefficient of 0.002 nm/mA, which is interrupted by steps [see Fig. 4(b)]. The step height of about 0.04 nm agrees with the expected spacing of adjacent longitudinal laser modes. In the current ranges between two mode hops, the laser operates in single longitudinal mode with a full width at half-maximum (FWHM) of the emissions peak of 0.03 nm and a side-mode suppression ratio (SMSR) of 40 dB [see the Fig. 4(b) inset].

Temperature-dependent measurements show that single longitudinal mode operation is maintained over a temperature range of 20°C to 40°C with a peak shift of 0.019 nm/K as shown in Fig. 5. This is comparable to the temperature sensitivity of GaN-based DFB laser diodes [12]. Since in this experiment the temperatures of the gain section and the DBR section were changed simultaneously, the previously mentioned mode hops did not occur, and the laser operated on the same longitudinal mode for the entire time.



Fig. 5. Temperature dependence of the peak emission wavelength of a DBR laser diode with L_{DBR} of 200 μ m operated at 100 mA.

5. SUMMARY

Single longitudinal mode CW operation of 405 nm DBR laser diodes has been demonstrated. Tenth-order surface Bragg gratings with V-shaped grooves were defined on 2 µm wide ridges with 0.25 µm distance from the edge of the ridge employing electron-beam lithography and plasma etching. With increasing length of the DBR section, the ratio of output power from the rear facet to that from the front facet reduced from 1.23 to 0.13. Thermal detuning of the gain section and the DBR section with increasing operation current resulted in periodic oscillations of the output power at the front facet due to mode hops. Between the mode hops, single-mode operation at around 405 nm with an FWHM of 0.03 nm (resolution limit of 0.02 nm) and an SMSR of 40 dB was obtained. Temperature-dependent measurements indicated single longitudinal mode operation between 20°C and 40°C and a linear redshift of the lasing wavelength of 0.019 nm/K. This is comparable to the temperature sensitivity of GaN-based DFB lasers.

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Data Availability. Data underlying the results presented in this paper are not publicly available at this time but may be obtained from the authors upon reasonable request.

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