PHOTONICS Research

Free-space realization of tunable pin-like optical vortex beams

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Received 27 January 2021; revised 18 March 2021; accepted 19 March 2021; posted 19 March 2021 (Doc. ID 420872); published 11 June 2021

We demonstrate, both analytically and experimentally, free-space pin-like optical vortex beams (POVBs). Such angular-momentum-carrying beams feature tunable peak intensity and undergo robust antidiffracting propagation, realized by judiciously modulating both the amplitude and the phase profile of a standard laser beam. Specifically, they are generated by superimposing a radially symmetric power-law phase on a helical phase structure, which allows the inclusion of an orbital angular momentum term to the POVBs. During propagation in free space, these POVBs initially exhibit autofocusing dynamics, and subsequently their amplitude patterns morph into a high-order Bessel-like profile characterized by a hollow core and an annular main lobe with a constant or tunable width during propagation. In contrast with numerous previous endeavors on Bessel beams, our work represents the first demonstration of long-distance free-space generation of optical vortex "pins" with their peak intensity evolution controlled by the impressed amplitude structure. Both the Poynting vectors and the optical radiation forces associated with these beams are also numerically analyzed, revealing novel properties that may be useful for a wide range of applications. © 2021 Chinese Laser Press

https://doi.org/10.1364/PRJ.420872

1. INTRODUCTION

During the last decades, there has been an increasing interest in the study of structured light and associated optical beam shaping techniques [1,2]. Prior to this enthusiasm, optical vortex beams constituting the fundamental element of singular optics [3–5] have already attracted a great deal of attention due to the peculiar characteristics associated with their phase singularity, topological charge, and hollow intensity distribution [6-12]. Their ability to carry orbital angular momentum (OAM), transferrable to an illuminated object, along with a number of related properties has further paved the way toward novel opportunities for scientific research and advanced applications [7]. These include, for example, optical tweezers and spanners [8,9] and high-order quantum entanglement [10,11]. The hollow-core intensity shape allows to circumvent the particles being susceptible to elevated absorptive heating, due to the high-intensity peak located at the center of the fundamental Gaussian beam typically emitted by a standard laser. All these applications require a comprehensive understanding of the In this regard, a larger variety of optical vortex structures have been reported in the literature [6,7]; some classical examples are optical Laguerre-Gaussian [13-15], high-order Bessel [16,17], helical Ince-Gaussian [18,19], and vector vortex [20,21] beams. Among them, high-order Bessel beams offer significant advantages with respect to other hollow beams because of their nondiffracting properties, which make them ideal for long-distance particle and atom transport [22]. It has also been shown that it is possible to generate high-order Bessel-like beams with the radius of the hollow core and maximum intensity fully controllable as a function of the propagation distance [23]. In general, diffraction is an undesired effect of light that causes beam expansion and peak intensity deterioration. A great amount of research efforts have been devoted in recent years to finding optical beams that are capable to counteract diffraction in different long-distance frameworks [24-27]. Although nondiffracting beams can be achieved via nonlinear effects forming spatial solitons [28-30] or via localized modes in

intensity distribution and OAM flux within optical vortices.

photonic structures [31], the requirement of nonlinear media and/or complex structure design could hamper the applicability of such beams. In free space, the first introduction of optical Bessel beams [32,33] has stimulated the generation of a variety of light beams with propagation-invariant properties such as Mathieu [34,35] and Bessel-like [23,36–38] beams.

Since Airy wave packet was introduced to optics [2,39,40], the nondiffracting properties of the light have also been extended beyond a straight-line propagation into curved paths, where various families of self-accelerating beams that are mostly based on an Airy-like profile have been proposed and demonstrated [41,42]. Of particular interest is the class of so-called "abruptly autofocusing beams," especially for potential uses in material ablation and medical surgery, driven by the fact that such radially symmetric self-accelerating beams can exhibit a low-intensity propagation combined with a controllable abrupt autofocusing right before a target [43-47]. Further research advances have also shown the possibility for the propagation of autofocusing vortex beams carrying OAM [48]. Due to their intrinsic characteristics, all these optical beams present significant diffraction and hence a rapid decrease in their peak intensities during subsequent propagation after the focal point. Applications exploiting the inherent properties of nondiffractive beams can benefit in many areas, including biomedical imaging, filamentation, particle manipulation, and free-space optical communications [2,49-55]. Ideally, every nondiffractive beam carries infinite power, thanks to which it can counteract diffraction indefinitely. Such a "perfect generation" with a stable amplitude profile over any propagation distance would require the illumination of an infinite transforming element with an ideal plane wave. Nevertheless, due to physical limitations present in all experimental settings, real beams must be truncated by an aperture and, as a consequence, diffraction takes place, resulting in antidiffracting beams with propagation distances extending from only a few centimeters to meters. (Note that the term "antidiffracting beam" is now widely used to refer to an arbitrary structured light that is capable of counteracting diffraction for a certain range of distances, although it is not "diffraction-free" in a strict sense. Such a mixed use of terms can be confusing because antidiffracting could be associated with a special propagation regime [56] such as freescale dynamics achieved in a particular type of nonlinear media [57-59].)

Recently, a new class of antidiffracting light waves, named "optical pin beams" (OPBs), has been demonstrated, showing a robust propagation through atmosphere turbulence over distances of kilometers when compared to a standard Gaussian beam [27]. Further research advances have also generalized the class of OPBs and demonstrated their robustness and intensity stability even in a strong scattering medium [60], with a better performance when compared with other nondiffracting beams such as abruptly autofocusing [43,45,46] and Bessel-type [32] beams.

In this paper, we report the first experimental demonstration of long-distance generation of pin-like optical vortex beams (POVBs) in free space, representing a topological extension of the previously introduced OPBs [27,60]. We analyze the existence of such POVBs. Compared to previous works based on fundamental Bessel configurations, the POVBs exhibit an initial autofocusing stage followed by an amplitude reshaping into a high-order Bessel-like beam, however, the hollow-core radius and the annular main-lobe width vary with the propagation distance. Interestingly, the peak intensity evolution can be easily controlled by imposing a properly designed amplitude modulation. POVBs are investigated not only from the viewpoint of their propagation properties, where several examples are numerically and experimentally illustrated, but also from their energy characteristics through calculating the associated Poynting vectors and optical forces.

2. THEORY

The analysis starts by introducing the vector potential of an arbitrary optical beam, $\vec{U}(r,\theta,z,t) = \psi(r,\theta,z) \exp(ikz - \omega t)\hat{x}$, assuming linear polarization along the *x* axis directed by the unity vector \hat{x} . Under a slowly varying envelope approximation, the linear wave equation describing the beam propagation dynamics can be expressed in cylindrical coordinates as

$$i\frac{\partial\psi}{\partial z} + \frac{1}{2k}\left(\frac{\partial^2\psi}{\partial r^2} + \frac{1}{r}\frac{\partial\psi}{\partial r} + \frac{1}{r^2}\frac{\partial^2\psi}{\partial\theta^2}\right) = 0.$$
 (1)

In Eq. (1), $\psi(r, \theta, z)$ denotes the electric field envelope, where r and θ represent the radial and azimuthal coordinates, and z is the longitudinal distance. In addition, $k = 2\pi/\lambda$ is the wavenumber of the optical wave, λ is the wavelength, ω is the angular frequency, and t is the time. The integral representation of Eq. (1) is given by the Fresnel integral

$$\psi(r,\theta,z) = -\frac{ik}{2\pi z} \int_0^r \int_0^{2\pi} A(\rho) \exp[i\phi(\rho,\varphi)] e^{ik\frac{\rho^2 + \rho^2 - 2\rho r\cos(\varphi-\theta)}{2z}} \rho d\rho d\varphi,$$
(2)

where $A(\rho)$ and $\phi(\rho, \varphi) = -kC_{\rho}(\rho/w_{\rho})^{\gamma} - l\varphi$ are the amplitude and the phase of the optical wave on the input plane, with ρ and φ indicating the radial and azimuthal coordinates at the onset of propagation, C_{ρ} is an arbitrary scaling parameter for the phase, γ the power exponent of phase modulation, l the topological charge, and w_{ρ} the phase normalization factor. To find an asymptotic solution to Eq. (2), we apply the stationary phase method by carrying out a procedure similar to the one in Ref. [60]. The beam envelope near the symmetry axis can be well approximated by the following expression:

$$\psi(r,z) = i^{-|l|} \sqrt{\frac{2\pi k}{2-\gamma}} A[\rho(z)] J_l \left[kr(C\gamma z^{\gamma-1})^{\frac{1}{2-\gamma}} \right] (C\gamma z^{\frac{\gamma}{2}})^{\frac{1}{2-\gamma}}$$
$$\times \exp\left\{ i \left[\frac{kr^2}{2z} + (C^2 \gamma^2 z^{\gamma})^{\frac{1}{2-\gamma}} \frac{k}{2} \left(1 - \frac{2}{\gamma} \right) - \frac{\pi}{4} (1+2|l|) - l\theta \right] \right\},$$
(3)

where J_l is the *l*th-order Bessel function, and $\rho(z) = (C\gamma z)^{1/(2-\gamma)}$, with *C* equal to $C_{\rho}/w_{\rho}^{\gamma}$. The overall propagation range depends on the maximum radius ρ_m at the onset distance through the relation $z_m = \rho_m^{2-\gamma}/(C\gamma)$. In this work, we limit the value of γ in the interval between 0 and 2. Additionally, Eq. (3) shows that the peak intensity evolution of a POVB can be controlled by properly engineering the initial amplitude structure $A[\rho(z)]$.

3. EXPERIMENTAL DEMONSTRATION

We have experimentally observed the POVBs described theoretically in the previous section. In our experimental setup, as illustrated in Fig. 1(a), a phase-only spatial light modulator (SLM), i.e., a liquid crystal device (Holoeye PLUTO-VIS-016, 8-bit gray phase levels, 1920×1080 pixels, $8 \,\mu\text{m} \times 8 \,\mu\text{m}$ pixel area) is employed to modulate the phase of a CW solidstate green laser (MGL-F-532 at $\lambda = 532$ nm, waist = 2 mm). Before impinging on the surface of the SLM, the Gaussian-like profile of the laser is expanded by a microscope system (40×, NA = 0.65, and f = 300 mm) to illuminate the active area of the device. According to Eq. (2), the generation of a POVB requires simultaneous reshaping of both the amplitude and phase profiles of an initial beam in real space. Since our SLM device does not provide the functionality of direct amplitude modulation, we employ an indirect technique as developed by Davis and his collaborators [61], which consists of encoding both the amplitude and phase information of a target beam onto a phase-only filter and then performing

the generation in the Fourier domain. To this purpose, a spherical lens (f = 300 mm) is used to compute the Fourier transform of the light reflected by the SLM, and an opaque mask of radius 0.5 mm is also placed at the Fourier plane to block the zeroth-order diffraction. Increasing the diffraction efficiency of the light to the first diffraction order is important for getting better results. To achieve higher diffraction efficiency, the spectral amplitude encoded into the phase-only mask of the SLM is not the one obtained by directly applying the formula of the encoding process, but it is created by means of a homemade lookup table compensating for eventual amplitude distortions. For detection, a costumed imaging system composed of a spherical lens (f = 100 mm) and a CCD camera (Coherent LaserCam-HR II, 12-bit dynamic range, 1280×1024 pixels, 4.6 μ m × 4.6 μ m pixel area) is used to record the transverse intensity distributions of POVBs. Furthermore, to retrieve the corresponding longitudinal intensity evolutions, the imaging system is also mounted on a

manual translation stage that allows for recording the beam



Fig. 1. Experimental observations of POVBs in free space for different values of the phase modulation exponent γ . (a) Schematic of the experimental setup used for the generation and detection of the POVBs. Path 1 highlights the beamline used for the generation, while path 2 the beamline used for carrying out the interferograms. (b1)–(d1) Normalized side-view of the beams in the *y*-*z* plane for (b1) $\gamma = 0.5$, (c1) $\gamma = 1$, and (d1) $\gamma = 1.5$. (b2)–(d2) Intensity distributions and (b3)–(d3) interferograms recorded at the distance z = 250 mm, marked by dashed white lines in (b1)–(d1). l = -2 is the topological charge. L, lens; M, mirror; BE, beam expander; BS, beam splitter; IS, imaging system; TS, translation stage; SLM, spatial light modulator.

profiles at selected distances with 1 mm resolution over long propagation (50 cm) in free space. We point out that such POVBs can in principle propagate to much longer distances whenever they are not limited by the size of both SLM and lab space [27].

Figures 1(b1)–1(d3) present experimental results associated with three different cases of POVBs, where the power-law phase exponent coefficient γ takes the values 0.5, 1, and 1.5. Without loss of generality, the topological charge l is chosen to be –2 for all the cases under consideration. The scaling parameter C_{ρ} related to the three values of γ is, respectively, 5.96, 3.77, and 3.12 µm, while w_{ρ} is 1 mm. The choice of C_{ρ} is not arbitrary, rather these coefficients are purposely calculated to obtain beam peak intensities appearing to a comparable propagation distance. The initial amplitude modulation is appropriately designed to generate POVBs exhibiting a lowvarying peak intensity over a long range of distances. In this case, a quasi-constant peak intensity evolution can be achieved using the formula

$$A(\rho) = A_{\text{POVB}}(\rho)i^{|l|}\rho^{-\gamma/2}\sqrt{\frac{2-\gamma}{2\pi\gamma kC}},$$
(4)

with $A_{\rm POVB}(\rho)$ being a constant coefficient related to the average beam power. The initial Gaussian beam is significantly expanded (radius = 8 mm) to meet the theoretical plane wave approximation of the initial condition. However, in case the influence of the Gaussian beam truncation cannot be neglected, it can also be embedded in the amplitude modulation for improving the maximum propagation range. Looking at the longitudinal intensity evolution in Figs. 1(b1)-1(d1), the POVBs undergo an initial autofocusing dynamic, reaching the highest peak intensity at a distance of about z = 200 mm and then exhibiting a dramatic reshaping of the intensity pattern into a high-order Bessel-like beam. A better visualization is provided in Figs. 1(b2)-1(d2), where the corresponding transverse intensity distributions recorded by the CCD camera at the distance z = 250 mm are presented. For $\gamma = 0.5$, both the hollow-core radius and the annular main-lobe width of the Bessel-like beam increase during propagation. In contrast, an opposite propagation dynamic occurs as γ takes a value larger than 1.0, for instance, 1.5 as used in Fig. 1. Indeed, no appreciable variation of the beam size is observed for a unitary value γ after the focal distance. Additionally, the beam intensity evolutions after the focal distance are examined. Since the initial amplitude is appropriately modulated to maintain a quasi-constant peak intensity during evolution, we observe a high intensity after 500 mm long propagation in free space for all these three cases. For comparison, we also performed a series of measurements of the POVBs without including any initial amplitude. Under such conditions, the beam intensities reach a maximum at a certain distance and decay significantly afterward, with undetectable light intensity at z = 500 mm, indicating the essential role played by the amplitude modulation. Finally, interferograms are recorded to examine the topological charge carried by the POVBs [see Figs. 1(b3)-1(d3)]. For each case, the interference fringes display a fork structure stemming from the phase singularity, indicating a topological charge l of -2. These results clearly demonstrate the robustness of the OAM carried by the vortex pin beams.

4. NUMERICAL SIMULATIONS

The above experimental observations can be corroborated with numerical simulations. To this purpose, Fig. 2 presents numerical results for the three cases corresponding to the measurements illustrated in Fig. 1. In particular, computations are carried out by solving Eq. (1) via the split-step Fourier transform method. All values of the parameters used in simulations are consistent with physical dimensions in our experimental setting. For the sake of completeness, we also list the other parameters used in our simulations: $\rho_0 = 0.5$ mm, $\lambda = 532 \text{ nm}, A_{\text{POVB}}(\rho) = 3.23$. The initial condition is constituted by a phase- and amplitude-modulated Gaussian beam, whose intensity value is zero inside a circle of radius ρ_0 . This assumption is motivated by the fact that the amplitude is diverging at the axis origin. As shown in Figs. 2(a1)-2(c1), the POVBs are observed to initially experience autofocusing dynamic at the earlier stage of their propagation followed by a subsequent reshaping into a high-order Bessel-like beam profile. Furthermore, normalized transverse intensity distributions retrieved at the distance z = 250 mm highlight the Bessel-like shape expected for the POVBs after the focal distance [Figs. 2(a2)–2(c2)]. For different values of the γ coefficient, the beam main lobes behave differently during propagation, hence exhibiting a propagation dependence. This behavior is also expected from the analytical solution in Eq. (3). Indeed, if R_{l0} is the full width at half-maximum (FWHM) of the *l*th-order Bessel function in Eq. (2), the radius of a POVB is given by

$$R(z) = \frac{R_{l0}}{2k(C\gamma z^{\gamma-1})^{\frac{1}{2-\gamma}}},$$
(5)

which depends in general on the propagation distance z except for the case $\gamma = 1$. R(z) increases (or decreases) as γ acquires a value smaller (or larger) than 1. Nevertheless, despite the progressive "expansion" or "shrinking" of the POVBs, their peak intensity remains almost constant over a long distance due to the initial amplitude modulation. Indeed, the peak intensity shows only slight oscillations around a constant value, with the oscillation frequency being increased for higher values of γ [see solid white lines in Figs. 2(a1)–2(c1)]. It is worth pointing out again that the amplitude modulation plays a primary role in the propagation dynamics of these vortex beams. Should only the phase modulation be applied to the initial Gaussian beam, the peak intensity of the POVB would have reached a maximum at a certain distance and then rapidly decaved to zero, similarly to the OPBs in Ref. [27]. The topological charge carried by the POVBs can be envisaged from their phase structures as shown in Figs. 2(a3)-2(c3). Wrapped phase patterns extracted at z = 250 mm from the numerical simulations show a clockwise spiral shape whose number of cycles is larger for low values of γ , and more importantly, they reveal a topological charge l = -2. Besides, in order to prove the validity of the analytical approximation on modeling the linear dynamics of POVBs, we also compare numerical results with analytical predictions from Eq. (3). Plots in Figs. 2(a4)-2(c4)show the overlapped output intensity profiles after 500 mm long propagation in free space for all the three cases of POVBs. The analytical curves match very well the numerical



Fig. 2. Numerical simulation of POVBs for different values of the parameter γ , with topological charge l = -2 and initial amplitudes predesigned to achieve a low-varying peak intensity over a long range of distances. (a1)–(c1) Normalized longitudinal intensity distributions in the *y*-*z* plane for (a1) $\gamma = 0.5$, (b1) 1, and (c1) 1.5; solid white lines in each panel plot the peak intensity evolutions. Corresponding (a2)–(c2) transverse intensity distributions and (a3)–(c3) wrapped phase patterns extracted at a distance z = 250 mm, marked by dashed white lines in (a1)–(c3). (a4)–(c4) Comparison between numerical (blue dashed lines) intensity profiles in (a1)–(c1) and analytical (red solid lines) prediction from Eq. (3), performed at the output after 500 mm long propagation.

simulations, especially in proximity of the main-lobe ring. The agreement further improves for even longer distances, thus quantitatively confirming the reshaping of the amplitudeand phase-modulated Gaussian beam at the onset into a high-order Bessel-like shape in the far field. These numerical and analytical results agree well with those from the experiments presented in Fig. 1.

5. CONTROL OF THE PEAK INTENSITY EVOLUTION

So far, the discussion has been only restricted to the PVOBs that display a constant or low-varying peak intensity evolution during subsequent propagation after initial autofocusing. Now we explore the tunability of the peak intensity over a long range of distances by properly engineering the initial amplitude modulation $A(\rho)$. Three typical examples are illustrated in Figs. 3(a1)-3(c1), where the peak intensities follow a hyperbolic secant, a flat-top, and a sinusoidal curve (as outlined by the white solid lines in Fig. 3). For these three cases, the POVBs are generated with the same power-law phase exponent coefficient $\gamma = 1.5$ but under different amplitude modulation $A(\rho)$ can be estimated by determining the function $A_{POVB}(\rho)$ to be inserted in Eq. (4) as

$$A_{\rm POVB}(\rho) = 3.23 \sqrt{I[\rho^{2-\gamma}/(C\gamma)]/I_0},$$
 (6)

where I(z) is the analytical peak intensity curve as a function of z. The exact profiles of $A_{POVB}(\rho)$ for all specific cases of POVBs analyzed in this paper are listed in Table 1. Furthermore, we perform a series of experiments to demonstrate POVBs featuring such predesigned peak intensity evolutions. Experimental results are presented in Figs. 3(a2)-3(c2), showing a clear modulation of the maximum intensity value along the propagation direction. The measured intensity variations show an evolution trend similar to the predicted curves.

6. POYNTING VECTORS AND OPTICAL FORCES

As seen above, the POVBs can be designed to exhibit tunable features, with either a constant or a pin-like vortex core as well as a controllable peak intensity evolution, in addition to preserved OAM during propagation. Besides the propagation properties, for both fundamental understanding and applications, it is also useful to investigate the energy-linked features associated with this class of optical beams. In this section, two key quantities related to the electromagnetic energy carried by POVBs are numerically explored: the Poynting vectors and the optical forces.

A. Poynting Vectors of POVBs

The Poynting vector represents the energy flux of the radiation field per unit area and is defined as $\vec{S} = \mu_0^{-1} \vec{E} \times \vec{B}$, with $\vec{B} = \nabla \times \vec{U}$ and $\vec{E} = ic^2 \omega^{-1} \nabla \times \vec{B}$ denoting, respectively, the



Fig. 3. Numerical (left) and experimental (right) results of POVBs in free space with $\gamma = 1.5$, topological charge l = -2, and different initial amplitudes designed to achieve a desired peak intensity evolution. Left-column panels illustrate the normalized longitudinal intensity distributions of POVBs whose peak intensity along the propagation direction follows (a1) a hyperbolic secant, (b1) a flat-top, and (c1) a sinusoidal curve as marked by a solid white line in each panel. Right-column panels show the corresponding experimental results. To provide a better comparison, experimental peak intensity evolutions (yellow dots) extracted from measurements at each distance *z* are overlapped to the corresponding curves from predictions (solid white lines).

Table 1. Analytical Peak Intensity of the POVBs in Fig. 3 as a Function of z

POVBs	Analytical Peak Intensity versus z
Steady state	$I(z) = I_0$ with $I_0 = 2.467 \text{ W/m}^2$
Hyperbolic secant	$I(z) = I_0 \operatorname{sech}(22z - 6.49)$
Flat-top	$I(z) = I_0 \exp[-(7.106z - 2.096)^4]$
Sinusoidal	$I(z) = I_0 \{1 - 0.5[\sin(6\pi z - 1.649)]^2\}$

magnetic and electric field, while μ_0 is the vacuum magnetic permeability, *c* the speed of light, and ∇ the nabla operator. For harmonic electromagnetic fields, the measured beam intensity directly relies on the time-averaged value of the Poynting vector over the wave cycle $T = 2\pi/\omega$. By applying the Lorentz gauge condition and the paraxial approximation, the average power flow can be expressed as [62,63]

$$\langle \vec{S} \rangle = \frac{1}{2\mu_0} (\vec{E} \times \vec{B}^* + \vec{E}^* \times \vec{B})$$

= $\frac{\omega}{2\mu_0} [i(\psi \nabla_\perp \psi^* - \psi^* \nabla_\perp \psi) + 2k|\psi|^2 \hat{z}],$ (7)

where the symbol (*) denotes the complex conjugate, $\nabla_{\perp} = \partial/\partial x\hat{x} + \partial/\partial y\hat{y}$ is the transverse nabla operator, and \hat{x}, \hat{y} , and \hat{z} are the unit vectors. In Eq. (7), the first term on the right side refers to the transverse component of the Poynting vector in the *x*-*y* plane, whereas the second term describes the energy flux flowing along the propagation direction *z*, revealing a direct proportionality with the beam intensity.

Numerically calculated Poynting vectors of the POVBs from Eq. (7) are illustrated in Figs. 4(a1)-4(a5) and 4(b1)-4(b5) at selected distances for two different values of γ . In particular, blue arrows displaying the transverse components of the Poynting vectors are superimposed to the corresponding

intensity distributions shown in the background. At the first stage, the energy flux radially flows from the beam sub-lobes toward the center [see Figs. 4(a1) and 4(b1)], leading to the focused vortex structure of the beam. After that, the energy flux mainly localizes and circulates around the high-intensity main lobe for subsequent long-distance propagation. Since for $\gamma = 1.5$ both the hollow-core radius and the main-lobe width of the POVB decrease during propagation, the transverse energy flux around the main lobe becomes gradually more localized [Figs. 4(b1)–4(b5)]. In contrast, the power flux remains invariant for $\gamma = 1$ as shown in Figs. 4(a1)–4(a5).

B. Optical Forces of POVBs

Optical forces originate from the transfer of linear or angular momentum from an optical beam to an illuminated object, essential for optical trapping and manipulation. As an illustrative example, we study here the optical forces exerted by a linearly polarized POVB on a spherical dielectric nanoparticle, suspended in a medium with a dielectric constant ε_m and featuring a radius *a* as well as a dielectric constant ε_p . If the particle size is sufficiently smaller than the light wavelength, the nanoparticle behaves like an electric dipole in accordance with Rayleigh scattering [64]. A simple description can be established by modeling the radiation pressure forces acting on an electromagnetic dipole, known as the Rayleigh regime, which consists of two components: the scattering and the gradient forces. The former is associated with the linear momentum changes through [64]

$$\vec{F}_{\rm scat}(r,\theta,z) = \frac{n_m}{c} C_{\rm pr} \langle \vec{S} \rangle_z,$$
(8)

where $\langle \bar{S} \rangle_z = I(r, \theta, z) \hat{z} = 0.5 n_m \epsilon_0 c |\psi(r, \theta, z)|^2 \hat{z}$ is the longitudinal component of the time-averaged value of the Poynting vector and $C_{\rm pr}$ is the cross-section pressure of the particle. For isotropic and non-absorbing particles, $C_{\rm pr}$ is equal to the scattering cross section $C_{\rm scat}$:



Fig. 4. Numerical calculations of Poynting vectors associated to the POVBs with topological charge l = -2 for two different values of the exponent coefficient γ : (a1)–(a5) $\gamma = 1$ and (b1)–(b5) $\gamma = 1.5$. Background distributions show normalized intensity patterns of the POVBs at (varying) distances z = 100, 200, 300, 400, and 500 mm. Blue arrows highlight the magnitude and direction of the transverse components of the Poynting vectors in the *x*-*y* plane. (c1)–(c3) Numerical calculations of the optical forces on a test polystyrene sphere suspended in water exerted by the three POVBs studied in Figs. 1 and 2. (c1) Maximum scattering force as a function of the propagation distance *z*. (c2) and (c3) Transverse gradient force from the POVB, calculated at two selected distances (c2) z = 200 mm and (c3) 500 mm.

$$C_{\rm pr} = C_{\rm scat} = \frac{8}{3}\pi k^4 a^6 \left(\frac{m^2 - 1}{m^2 + 2}\right)^2,$$
 (9)

with $m = n_p/n_m$ being the ratio between the refractive index of the particle n_p and that of the medium n_m . The other force, i.e., the gradient force, is related to the Lorentz force induced by the electromagnetic field on the dipole. In the steady state, the time-averaged gradient force reduces to [64,65]

$$\vec{F}_{\text{grad}}(r,\theta,z) = \frac{2\pi n_m a^3}{c} \left(\frac{m^2 - 1}{m^2 + 2}\right) \nabla I(r,\theta,z).$$
(10)

Figures 4(c1)-4(c3) present the scattering and gradient forces from the three POVBs studied earlier (Figs. 1 and 2), calculated numerically according to Eqs. (8) and (10). Specifically, we examined the case of polystyrene spheres (mass density 1050 kg/m^3) suspended in water, with the parameters in the simulations chosen as $n_p = 1.592$, $n_m = 1.33$, and a = 20 nm. The scattering force, which acts mainly along the beam propagation direction, is shown in Fig. 4(c1), and the maximum scattering force exerted by the three POVBs follows the corresponding beam peak intensity evolution (see solid white lines in Fig. 2), reaching the highest value near the focal distance and then oscillating asymptotically for a long distance. On the other hand, the gradient force acts in the transverse direction and determines the ability of POVBs to trap a particle. Numerical results show that the gradient force associated with a higher value of γ is much larger than for the other two cases with a lower value of γ , especially after a long propagation

distance [see Figs. 4(c2) and 4(c3)]. Physically, the increased gradient force is mediated by the pin-like feature of the vortex beams, as the hollow-core POVB gets focused closer to the size of the particle, thus guaranteeing a better trapping capability. We believe that our numerical study on the optical forces provides a guide for employing the POVBs in experiments of optical trapping applications, including three-dimensional particle manipulation [66].

7. CONCLUSION

In this work, we have experimentally demonstrated pin-like optical vortex beams and investigated their energy flow properties by numerically calculating the Poynting vectors and the optical radiation forces. These vortex beams are generated by modulating both the amplitude and the phase profile of an input laser beam through a spatial phase structure composed of a radially symmetric power-law phase chirp profile and an OAM phase term with an arbitrary topological charge. A POVB initially exhibits an autofocusing evolution and reaches the maximum intensity, and then it displays a reshaping of the amplitude pattern into a high-order Bessel-like beam whose annular mainlobe width and hollow-core radius change during propagation. An appropriate design of the initial amplitude based on the theoretical analysis allows control of the beam peak intensity along with the propagation range. Moreover, we have also shown that the transverse power flux initially flows radially from the beam sub-lobes toward the beam center to form the vortex structure and then localizes and rotates with the higher values of the Poynting vectors concentrated in the main lobe of the annular beam. Finally, we have studied the optical radiation forces associated with these vortex pins and shown their dependence on the design parameters for the POVBs. These specially designed beams can lead to optimal optical forces for trapping and manipulating a nanoparticle under test. Moreover, this research expands the understanding of free-space generation of antidiffracting optical vortex beams and builds up a connection between singular optics and structured light, which may find applications in different areas such as optical communication and quantum information technologies.

Funding. National Key Research and Development Program of China (2017YFA0303800); National Natural Science Foundation of China (11674180, 61575098, 91750204); 111 Project in China (B07013); NSERC Discovery and Strategic grants in Canada; MESI in Quebec; 66 Postdoctoral Science Grant of China.

Acknowledgment. We thank Ze Zhang for assistance. R.M. is affiliated with UESTC as an adjoining faculty.

Disclosures. The authors declare no conflicts of interest.

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