

Single lens sensor and reference for auto-alignment

Shun-Xing Tang, Ya-Jing Guo, Dai-Zhong Liu, Lin Yang, Xiu-Qing Jiang, Zeng-Yun Peng,
and Bao-Qiang Zhu

Joint Laboratory of High Power Laser Physics, Shanghai Institute of Optics and Fine Mechanics, Chinese Academy of Sciences, Shanghai 201800, China

(Received 13 November 2017; accepted 19 December 2017)

Abstract

Auto-alignment is a basic technique for high-power laser systems. Special techniques have been developed for laser systems because of their differing structures. This paper describes a new sensor for auto-alignment in a laser system, which can also serve as a reference in certain applications. The authors prove that all of the beam transfer information (position and pointing) can theoretically be monitored and recorded by the sensor. Furthermore, auto-alignment with a single lens sensor is demonstrated on a simple beam line, and the results indicate that effective auto-alignment is achieved.

Keywords: auto-alignment; high-power laser

1. Introduction

In high-power laser systems, such as NOVA, OMEGA, NIF, and SG-II, an auto-alignment system is very important because thousands of mirrors exist in hundreds of meters of beam lines^[1–6]. As high-power laser systems have developed from the MOPA-based to four-path concept, auto-alignment systems have been developed to meet the special requirements as laser systems have become more complicated. Moreover, the auto-alignment technique is continually developing as new equipment and tools are applied^[7–15]. The NIF is a typical four-path high-power laser system, which in its early years used a grating reference for alignment, and after years of development, a no-grating scheme has been applied^[13, 14].

Auto-alignment processing loops always start with determining the current position and pointing angle of the beam, which requires a sensor in order to obtain the beam position displacement and pointing deviation angle from the reference (some type of mark). Second, the system must decide how much the mirror should be adjusted by means of analyzing the image acquired by the sensor. Then, the mirror is adjusted by driving motors for the corresponding steps, and the new beam position and pointing angle are verified by the sensor. This loop will stop when both the beam position and pointing angle meet the system requirements. Previous alignment methods typically required two optical

sensors, one for the beam position and the other for its pointing angle. In certain situations, considering space or budget limitations, such as in outer space or vacuum chambers^[16], high temperatures or cryogenic environments, and high radiation situations, the sensor needs to be very small or lightweight. We propose a sensor with only one lens, one plate, and one camera, which improves on the previous methods by including a type of sensor with one camera^[17]. Because this method is so simple and stable, it can not only operate as a sensor, but also serve as an effective reference.

2. Setup of single lens alignment sensor and reference

The single lens alignment sensor is designed on the basis of the ‘ghost image concept’, and consists of a lens, parallel plate, and camera (see Figure 1). The normals of the plate and camera surfaces should be parallel to the lens axis. When placing the camera on the focal plane of the second-order ghost image of the input beam led by the plate, the camera will detect both the beam profile and focal spot in one image. With a special coat on the plate, the ‘ghost’ is significantly brightened, and the brightness is sufficiently strong compared to that of the beam profile. In comparison with the two-sensor auto-alignment method, we refer to the beam profile image as near-field (or more accurately, quasi-near-field), and the ghost image as far-field.

Based on the matrix optics theory, we analyze the sensor operation. The transfer array from the lens to the camera for

Correspondence to: Y.-J. Guo, 390 Qinghe Road, Jiading, Shanghai 201800, China. Email: gracegg@siom.ac.cn

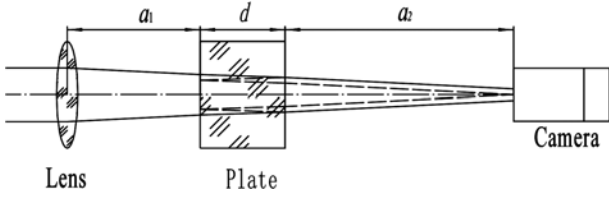


Figure 1. Scheme of the single lens alignment sensor and reference.

the original beam should be

$$\begin{bmatrix} 1 - \frac{a_1 + a_2}{f} - \frac{d}{fn} & a_1 + a_2 + \frac{d}{n} \\ -\frac{1}{f} & 1 \end{bmatrix}, \quad (1)$$

where a_1 is the distance from the lens to the plate's front surface, a_2 is the distance from the camera to the plate's rear surface, d is the plate thickness, n is the plate refractivity, and f is the lens focus length.

Furthermore, the transfer array of the ghost beam should be

$$\begin{bmatrix} 1 - \frac{a_1 + a_2}{f} - \frac{3d}{fn} & a_1 + a_2 + \frac{3d}{n} \\ -\frac{1}{f} & 1 \end{bmatrix}. \quad (2)$$

Because the camera is located at the focal spot of the lens, the sensor parameters should satisfy the following correlation:

$$a_2 = f - a_1 - 3d/n. \quad (3)$$

In this case, the transfer array should be rewritten as

$$\begin{bmatrix} 2d/fn & f - 2d/n \\ -1/f & 1 \end{bmatrix}, \quad (4)$$

and

$$\begin{bmatrix} 0 & f \\ -1/f & 1 \end{bmatrix}. \quad (5)$$

These are functions of f , n , d , which means that the plate position (a_1) does not contribute anything to the transfer array.

Taking the lens center and axis as the alignment reference, the optics array of the input laser beam should be written as

$$A_{\text{in}} = \begin{bmatrix} r_X & r_Y \\ \theta_X & \theta_Y \end{bmatrix}, \quad (6)$$

where r_X and r_Y are horizontal and vertical displacement, respectively, of the laser beam center on the input surface of the lens from the lens center, while θ_X and θ_Y are the azimuth

and altitude deviation, respectively, of the beam pointing direction from the lens axis. Then, we can determine the near-field and far-field positions on the camera:

$$\begin{cases} x_{\text{FF}} = f\theta_X \\ x_{\text{NF}} = 2dr_X/fn + f\theta_X - 2d\theta_X/n, \end{cases} \quad (7)$$

$$\begin{cases} y_{\text{FF}} = f\theta_Y \\ y_{\text{NF}} = 2dr_Y/fn + f\theta_Y - 2d\theta_Y/n, \end{cases} \quad (8)$$

where $(x_{\text{FF}}, y_{\text{FF}})$ is the far-field center on the camera, and $(x_{\text{NF}}, y_{\text{NF}})$ is the near-field center on the camera.

Camera image acquisition provides an image including both the near-field and far-field, and we can determine the input beam position and pointing angle from the image as follows:

$$\begin{cases} r_X = x_{\text{FF}} + (x_{\text{NF}} - x_{\text{FF}})fn/2d, \\ \theta_X = x_{\text{FF}}/f, \end{cases} \quad (9)$$

and

$$\begin{cases} r_Y = y_{\text{FF}} + (y_{\text{NF}} - y_{\text{FF}})fn/2d, \\ \theta_Y = y_{\text{FF}}/f. \end{cases} \quad (10)$$

If the sensor is installed as a reference, the target position can be described as

$$A_{\text{ref}} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}. \quad (11)$$

In this case, suppose that the camera sensor center is located accurately on the lens axis and the surfaces of the plate are parallel, then the far-field and near-field should be in the center of the image acquired by the camera. The mirrors are driven for alignment until the far-field and near-field centers move to the image center with an acceptable error.

3. Optical parameter analysis in the sensor

In order to perform alignment of a beam path, we need to know the beam aperture (A), near-field tolerance (maximum deviation from reference D_c), and position alignment accuracy requirement (R_{NF}), while for the pointing angle, we need to know the far-field tolerance (θ_c) and pointing angle alignment accuracy requirement (R_{FF}). The reference and sensor must meet all of the requirements, which need to be considered in order to determine the sensor parameters. When designing the sensor, there are certain basic rules for laser system beam alignment that should be obeyed.

The correlation between the sensor parameters and the alignment concerned specifications is analyzed in this section. As illustrated in Figure 1 and discussed above, the sensor parameters include the lens parameters (focal length

Table 1. Correlation between sensor parameters and alignment concerned specifications.

Item	Correlation	Symbol implication	
D_c	$D_c^+ (f - 2d/n)\theta_c < MR_c - 2dA/f$ $D_c < D - A$	f – focal length of lens D – diameter of lens; d – thickness of plate	M – size in pixels of camera A – beam aperture; D_c – near-field tolerance (max deviation from reference)
R_{NF}	$fR_c/(2dDA)$	n – refractive index	R_{NF} – position alignment accuracy
θ_c	$D_c + (f - 2d/n)\theta_c < MR_c - 2dD/f$	r_1 – reflectivity at front side of plate	θ_c – far-field tolerance (max deviation from reference)
R_{FF}	R_c/f .	r_2 – reflectivity at rear side of plate	R_{FF} – pointing angle alignment accuracy
Contrast	$r_1 r_2 [dA^2 / (1.22\lambda f^2)]^2 = 1-20^*$	λ – wavelength of laser beam R_c – pixel size of camera	

*Note: vertical stability of the mirrors is not as good as in the horizontal direction; during all the processes, the motors are never driven for vertical adjustment.

f and diameter D), plate parameters (thickness d , refractive index n , and reflectivity at front side r_1 and rear side r_2) and camera parameters (pixel size R_c and sensor size M). Most of the time, optical systems are designed with axial symmetry; therefore, we simply discuss one dimension.

The near-field size on the camera is

$$D_{NF} = 2dA/f. \quad (12)$$

By using the ideal divergence angle of the laser beam, the far-field spot size on the camera is

$$D_{FF} = 2.44f\lambda/A. \quad (13)$$

Considering the worst situation, the position and pointing angle limits add up at the same side of the lens axis, so the camera's minimal size should be

$$M_{\min} = D_c + (f - 2d/n)\theta_c + D_{NF}. \quad (14)$$

In order to distinguish the far-field from near-field image, the far-field brightness should be 1 to 20 times that of the near-field. In most cases, as a result of optical system aberration, far-field brightness cannot be ideal; therefore, we estimate the focal spot size as D_{FF} . Based on the analysis, we get the correlation between the sensor parameters and the alignment concerned specifications, as is shown in Table 1.

4. Beam alignment with single lens sensor

4.1. Experimental setup

As illustrated in Figure 2, a fiber output laser source @1053 nm is connected to a collimator, and the beam is expanded to $\sim\varphi$ 100 mm. We use a serrated aperture to select a 33.4-mm diameter beam (calibrated at the lens front surface) for alignment (see Figure 3). The mirrors for alignment are 88 mm × 120 mm in size, operating at 45°. The sensor includes a lens ($f = 954$ mm@1053 nm, $D = 100$ mm), two pieces of plates (working together as

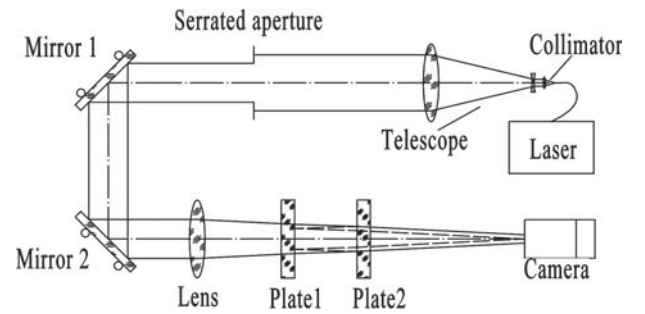


Figure 2. Experimental setup using sensor for alignment.

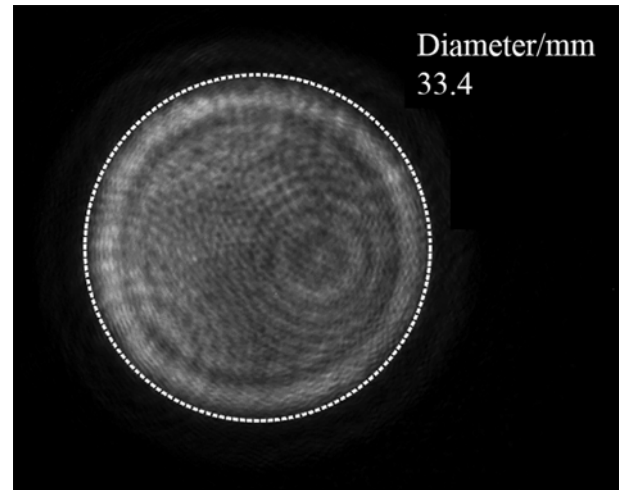


Figure 3. Laser beam profile for alignment.

one plate, using the plate 1 rear surface with a coating of reflectivity $r_1 = 10\%$ and front surface of plate 2 with a coating of reflectivity $r_2 = 10\%$, $n = 1$, because the ghost is reflected between air gaps) and a camera ($R_c = 8.3$ $\mu\text{m}/\text{pixel}$, size 782 pixel × 582 pixel).

The optics are roughly adjusted, as shown in Figure 2, and then the lens, plates and camera are adjusted, as described in Section 1. In the experiment, the single plate is replaced

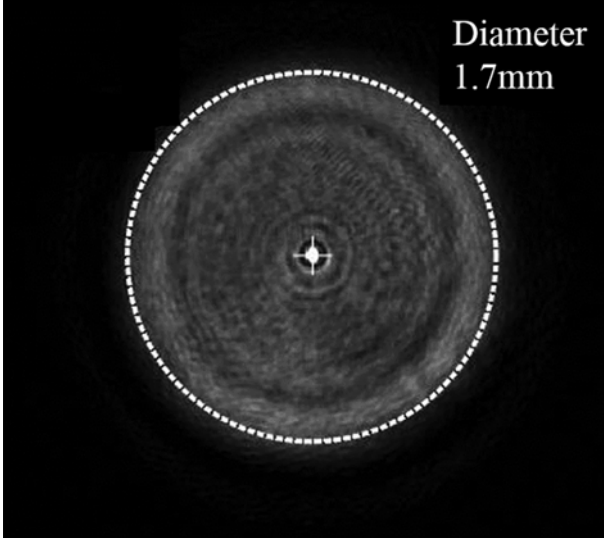


Figure 4. Near-field plus far-field alignment image captured by the sensor.

by two plates, simply because such a single plate with two sides of 10% coating is not often used in our laboratory, and needs to be processed specially for a certain designed alignment system, as described in Section 2. The alignment image captured by the sensor after adjustment is shown in Figure 4.

4.2. Response function of alignment system

In order to prepare for the alignment task, the sensor will ‘teach’ the alignment mirrors how to carry out alignment work, or determine the response function of the alignment system:

$$\begin{bmatrix} N_X \\ N_Y \\ F_X \\ F_Y \end{bmatrix} = \begin{bmatrix} r_{NX_M1X} & r_{NX_M1Y} & r_{NX_M2X} & r_{NX_M2Y} \\ r_{NY_M1X} & r_{NY_M1Y} & r_{NY_M2X} & r_{NY_M2Y} \\ r_{FX_M1X} & r_{FX_M1Y} & r_{FX_M2X} & r_{FX_M2Y} \\ r_{FY_M1X} & r_{FY_M1Y} & r_{FY_M2X} & r_{FY_M2Y} \end{bmatrix} \begin{bmatrix} M_{1X} \\ M_{1Y} \\ M_{2X} \\ M_{2Y} \end{bmatrix}, \quad (15)$$

where N_X (N_Y) is the near-field displacement on the camera (in pixels) in the horizontal (vertical) direction caused by mirror 1 and mirror 2 adjustment (counted in steps), while F_X (F_Y) is the far-field displacement. Furthermore, M_{1X} (M_{1Y}) represents the adjustment steps of mirror 1 in the horizontal (vertical) direction, while M_{2X} (M_{2Y}) is the mirror 2 adjustment steps. When the mirror mount is designed to be orthogonal, Equation (15) can be

$$\begin{bmatrix} N_X \\ N_Y \\ F_X \\ F_Y \end{bmatrix} = \begin{bmatrix} r_{NX_M1X} & 0 & r_{NX_M2X} & 0 \\ 0 & r_{NY_M1Y} & 0 & r_{NY_M2Y} \\ r_{FX_M1X} & 0 & r_{FX_M2X} & 0 \\ 0 & r_{FY_M1Y} & 0 & r_{FY_M2Y} \end{bmatrix} \begin{bmatrix} M_{1X} \\ M_{1Y} \\ M_{2X} \\ M_{2Y} \end{bmatrix}. \quad (16)$$

In order to demonstrate the alignment loop by means of one-dimensional alignment, the horizontal direction or x -direction response function can be written as

$$\begin{bmatrix} N_X \\ F_X \end{bmatrix} = \begin{bmatrix} r_{NX_M1X} & r_{NX_M2X} \\ r_{FX_M1X} & r_{FX_M2X} \end{bmatrix} \begin{bmatrix} M_{1X} \\ M_{2X} \end{bmatrix}. \quad (17)$$

In order to determine the response array of the alignment system, we can check each array element by adjusting one by one the dimensions of each mirror (see Figure 5). Taking r_{NX_M1X} and r_{FX_M1X} as an example, first, we record an alignment image at the starting position, before the motor drives mirror 1 in the horizontal direction. Second, we drive mirror 1 in the horizontal direction by a certain number of steps each time (for example, 20 steps) and record the corresponding alignment image until sufficient images are obtained. Finally, we determine the center of the near-field and far-field for each image, and find the relationship (r_{NX_M1X} and r_{FX_M1X}) between the mirror 1 adjustment steps and the near-field and far-field center positions (in pixels).

With each element of the response array, taking the average of different adjustment directions, we obtain the response function for the horizontal direction as follows:

$$\begin{bmatrix} N_X \\ F_X \end{bmatrix} = \begin{bmatrix} -1.137 & 1.087 \\ -1.157 & 1.125 \end{bmatrix} \begin{bmatrix} M_{1X} \\ M_{2X} \end{bmatrix}, \quad (18)$$

where N_X and N_Y are described in pixels, and M_{1X} and M_{2X} are described in steps.

After determining the response array, we can establish how to drive the mirrors when we obtain an alignment image (near-field and far-field center displacement from reference) by the sensor.

4.3. Performance of sensor

As the mirror mount experiences a motor empty back problem vertically, while working effectively in the horizontal direction, which is not the most important issue, we simply carry out horizontal alignment to test the sensor’s performance.

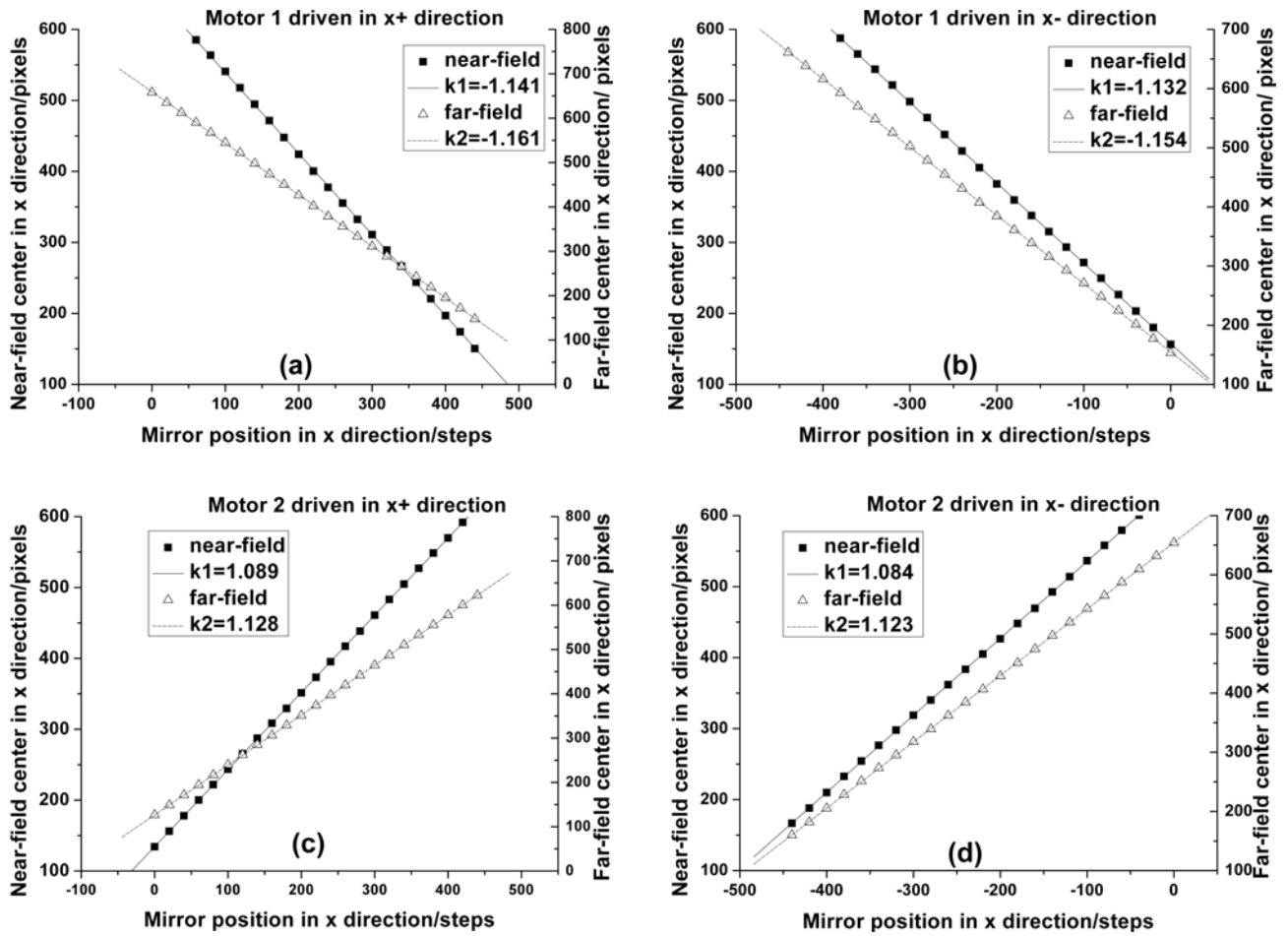


Figure 5. Near-field and far-field center changes as mirror is adjusted in different horizontal directions ($x + / x -$).

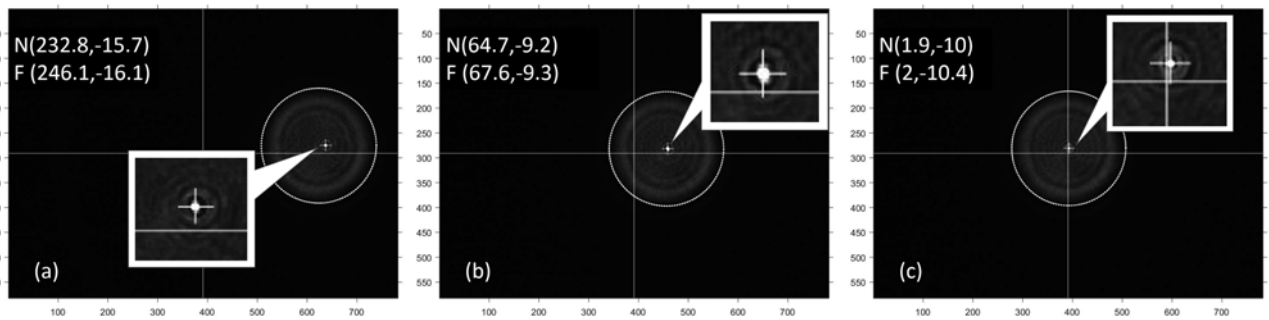


Figure 6. (a) Initial alignment image; (b) alignment image after first alignment process; (c) alignment image after second alignment process.

First, the image records the initial beam position of the beam (Figure 6(a)), and calculates the offset of the near-field center (232.8 pixels) and far-field center (246.1 pixels) from the reference (we take the camera center as the reference). According to Equation (18), the motor steps should be driven

by -247 steps for mirror 1 and -473 steps for mirror 2 in the horizontal direction. However, we simply adjust three-quarter steps of these, namely -185 and -355 steps, for the purpose of reducing the out-of-step error, and then record the new position (Figure 6(b)): 64.7 pixels for near-field

and 67.6 pixels for far-field). Second, we calculate all of the remaining steps in the same manner, namely -32 steps for mirror 1 and -93 steps for mirror 2 in the horizontal direction. Following alignment image acquisition, we verify the result, which is only 1.9 pixels for near-field and 2.0 pixels for far-field deviation from the reference (Figure 6(c)).

The alignment accuracy is determined by both the controlling accuracy of the mirror mounts and sensor sensitivity. In the example discussed above, the mirror mount calibrated response is almost 1 pixel per step, which means that the controlling accuracy cannot be better than 1 pixel. Furthermore, the sensor cannot be better than 1 pixel, which is equal to $8.3 \mu\text{m}/954 \text{ mm} = 8.7 \mu\text{rad}$ for the pointing angle alignment, and $8.3 \mu\text{m}/1.7 \text{ mm} = 0.5\%$ or 0.16 mm for the 33.4 mm diameter beam for beam position alignment.

5. Conclusion

A single lens alignment sensor is designed on the basis of the ‘ghost image concept’. The working principle and performance analysis are demonstrated based on the theory of matrix optics. The design rules and alignment processing are defined, and an alignment example is carried out in order to demonstrate how the sensor works. The test results indicate that the sensor can operate effectively in the beam alignment process. The experimentally designed sensor performance is stable and can meet the alignment accuracy with approximately 0.5% for the position and $17.4 \mu\text{rad}$ for the pointing angle. Adjusting the focal length, plate thickness, and camera type can meet improved accuracy requirements.

Acknowledgements

The authors appreciate Zengyun Peng, Huibin Yang, Haidong Zhu, and Zhixiang Zhang for sharing certain equipment with us when carrying out the experiments.

References

1. T. R. Boehly, D. L. Brown, R. S. Craxton, R. L. Keck, J. P. Knauer, J. H. Kelly, T. J. Kessler, S. A. Kumpan, S. J. Loucks, S. A. Letzring, F. J. Marshall, R. L. McCrory, S. F. B. Morse, W. Seka, J. M. Soures, and C. P. Verdon, *Opt. Commun.* **1–6**, 133 (1997).
2. C. A. Haynam, R. A. Sacks, P. J. Wegner, M. W. Bowers, S. N. Dixit, G. V. Erbert, G. M. Heestand, M. A. Hennesian, M. R. Hermann, K. S. Jancaitis, K. R. Manes, C. D. Marshall, N. C. Mehta, J. Menapace, M. C. Nostrand, C. D. Orth, M. J. Shaw, S. B. Sutton, W. H. Williams, C. C. Widmayer, R. K. White, S. T. Yang, and B. M. Van Wonerghem, *Appl. Opt.* **16**, 46 (2007).
3. W. Zheng, X. Wei, Q. Zhu, F. Jing, D. Hu, J. Su, K. Zheng, X. Yuan, H. Zhou, W. Dai, W. Zhou, F. Wang, D. Xu, X. Xie, B. Feng, Z. Peng, L. Guo, Y. Chen, X. Zhang, L. Liu, D. Lin, Z. Dang, Y. Xiang, and X. Deng, *High Power Laser Sci. Eng.* **4**, e21 (2016).
4. G. Yanqi, C. Zhaodong, Y. Xuedong, M. Weixin, Z. Baoqiang, and L. Zunqi, *11th Conference on Lasers and Electro-Optics Pacific Rim (CLEO-PR)*. Busan, South Korea (2015), p. 1.
5. M. L. Andre, *2nd Annual International Conference on Solid State Lasers for Application to Inertial Confinement Fusion*. Paris, France (1996), p. 38.
6. L. Zunqi, W. Shiji, F. Dianyuan, Z. Jianqiang, Y. Yi, Z. Jian, C. Xijie, M. Weixin, Z. Dakui, S. Liqing, Z. Qingchun, X. Deyan, S. Weixing, C. Shaohe, C. Qinghao, P. Zengyun, L. Fengqiao, L. Liangyu, H. Guanlong, X. Zhenhua, and T. Xianzhong, *Chin. J. Lasers* **10B**, 6 (2001).
7. E. S. Bliss, R. G. Ozarski, D. W. Myers, J. B. Richards, C. D. Swift, R. D. Boyd, R. E. Hugenberger, L. G. Seppala, J. Parker, and E. H. Dryden, *9th Symposium on Engineering Problems of Fusion Research*. Chicago, USA (1981), p. 1242.
8. E. S. Bliss, S. J. Boege, R. D. Boyd, D. T. Davis, R. D. Demaret, M. Feldman, A. J. Gates, F. R. Holdener, C. F. Knopp, R. D. Kyker, C. W. Lauman, T. J. McCarville, J. L. Miller, V. J. Miller-Kamm, W. E. Rivera, J. T. Salmon, J. R. Severyn, S. K. Sheem, S. W. Thomas, C. E. Thompson, D. Y. Wang, M. F. Yoeman, R. A. Zacharias, C. Choccol, J. Hollis, D. Whitaker, J. Brucker, L. Bronisz, and T. Sheridan, *3rd International Conference on Solid State Lasers for Application to Inertial Confinement Fusion*. Monterey, USA (1998), p. 285.
9. R. D. Boyd, E. S. Bliss, S. J. Boege, R. D. Demaret, M. Feldman, A. J. Gates, F. R. Holdener, J. Hollis, C. F. Knopp, T. J. McCarville, V. J. Miller-Kamm, W. E. Rivera, J. T. Salmon, J. R. Severyn, C. E. Thompson, D. Y. Wang, and R. A. Zacharias, *SPIE Conference on Optical Manufacturing and Testing III*. Denver, USA (1999), p. 496.
10. Y.-Q. Gao, B.-Q. Zhu, D.-Z. Liu, X.-F. Liu, and Z.-Q. Lin, *Appl. Opt.* **8**, 48 (2009).
11. J. D. Lindl and E. I. Moses, *Phys. Plasmas* **5**, 18 (2011).
12. D. Liu, R. Xu, and D. Fan, *Chin. Opt. Lett.* **2**, 92 (2004).
13. S. C. Burkhart, E. Bliss, P. Di Nicola, D. Kalantar, R. Lowe-Webb, T. McCarville, D. Nelson, T. Salmon, T. Schindler, J. Villanueva, and K. Wilhelmsen, *Appl. Opt.* **8**, 50 (2010).
14. K. Wilhelmsen, A. Awwal, G. Brunton, S. Burkhart, D. McGuigan, V. M. Kamm, R. Leach, Jr., R. Lowe-Webb, and R. Wilson, *Fusion Engng Design* **12**, 87 (2012).
15. R. Krappig and R. Schmitt, *Conference on Photonic Instrumentation Engineering IV*. San Francisco, USA (2017), p. 11.
16. W. Wu, L. Bi, K. Du, J. Zhang, H. Yang, and H. Wang, *High Power Laser Sci. Eng.* **5**, e9 (2017).
17. M. Charles, Laser beam centering and pointing system. U.S. Patent 8,934,097 (Jan. 13, 2015).