

# Highly birefringent photonic crystal fibers with flattened dispersion and low confinement loss\*

CAO Ye (曹晔), LI Rong-min (李荣敏)\*\*, and TONG Zheng-rong (童峥嵘)

*Key Laboratory of Film Electronics and Communication Devices, Key Laboratory of Intelligent Computing and Novel Software Technology, School of Computer and Communication Engineering, Tianjin University of Technology, Tianjin 300384, China*

(Received 24 August 2012)

©Tianjin University of Technology and Springer-Verlag Berlin Heidelberg 2013

A highly birefringent index-guiding photonic crystal fiber (PCF) with flattened dispersion and low confinement loss is proposed by introducing two small air holes with the same diameter in the core area. The fundamental mode field, birefringence, confinement loss, effective mode area and dispersion characteristic of the fibers are studied by the full-vector finite element method (FEM). Simulation results show that a high birefringence with the order of  $10^{-3}$  and a low confinement loss of 0.001 dB/km are obtained at 1550 nm. Furthermore, flattened chromatic dispersion from 1450 nm to 1590 nm is obtained.

**Document code:** A **Article ID:** 1673-1905(2013)01-0045-4

**DOI** 10.1007/s11801-013-2336-8

The photonic crystal fiber (PCF) is a new kind of optical fiber with photonic crystal structure. There are many unique optical characteristics in the PCF, such as endless single mode, low loss, flexible dispersions, adjustable non-linear and high birefringence<sup>[1-5]</sup>. The PCF has attracted a lot of interest during past years, and quickly develops in aspect of optical fiber communication, optical fiber sensing and optical passive devices<sup>[6-8]</sup>.

Highly birefringent fiber is used in many sensing applications and some other applications in which light is required to maintain a linear polarization station. In the conventional highly birefringent fiber, the core is mixed with GeO<sub>2</sub>, the confinement loss can increase in the nuclear radiation environment, the nuclear explosion tolerance is low, and the temperature stability performance is bad. However, highly birefringent PCF is made up with pure silica materials. Different structures can be designed to improve the properties of the fiber. It has some incomparable advantages compared with the conventional highly birefringent fiber. The structures of the highly birefringent PCF can be designed flexibly, by introducing air holes with different sizes to the cladding, or changing the core or the cladding air holes shape<sup>[9-11]</sup>. We can get the highly birefringent PCF with outstanding performance. The dispersion properties of PCF are significantly different from those of conventional fibers for the novel clad-

ding structure. It consists of an array of micrometer-sized air holes allowing for flexible tailoring of the dispersion curves. To achieve the near-zero flattened dispersion in PCF, several designs have been proposed<sup>[12,13]</sup>. By introducing the elliptical air holes in the core area, a highly birefringent PCF with flattened dispersion and low effective mode area was presented by Hu<sup>[12]</sup>, but the confinement loss is increased, and it makes process difficult for introducing the elliptical air holes. Highly nonlinear bending-insensitive birefringent PCF was presented by Huseyin<sup>[14]</sup>. Although the confinement loss is low, the dispersion is not flat. By introducing the elliptical air holes in the cladding, a highly birefringent PCF with flattened dispersion and low effective mode area was presented by Liang<sup>[15]</sup>, but the confinement loss is increased, and it makes the light signal transmission difficult for introducing the elliptical air holes.

In this paper, we employ the index-guiding PCF structure with uniform air-silica lattice, and a highly birefringent index-guiding photonic crystal fiber with flattened dispersion and low confinement loss is proposed by introducing two small air holes with the same diameter in the core area. The fundamental mode field, birefringence, confinement loss, effective mode area and dispersion characteristic of the fiber are studied by the full-vector finite element method (FEM). A high birefringence with the order of  $10^{-3}$  and the low con-

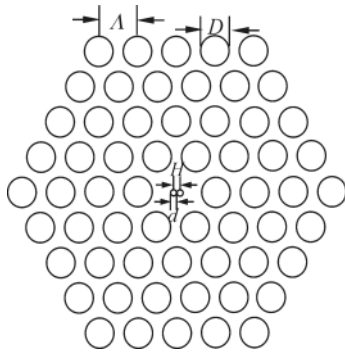
\* This work has been supported by the National Natural Science Foundation of China (No. 61107052).

\*\* E-mail: lirongmin1108@163.com

finement loss of 0.001 dB/km are obtained at wavelength 1550 nm by adjusting the diameters of the two small air holes. Furthermore, flattened chromatic dispersion from 1450 nm to 1590 nm is obtained.

FEM is an algorithm that can solve mathematics and physics problems based on variational principle. PCF with any irregular section shape and refractive index under any combination material can be solved well by FEM which has higher calculation accuracy in analyzing mode field. In this work, we have employed full-vector finite element method to investigate key modal properties of the proposed index-guided PCF.

Fig.1 shows the cross-section of the PCF. Two small air holes with the same diameter  $d$  are introduced into the core area for more high birefringence. The pitch of the two small air holes is  $H$ . At the same time, in order to reduce the confinement loss, four rings of air holes are considered, the diameter of the air holes is  $D$ , the air hole pitch is  $A=2.11 \mu\text{m}$  and  $D/A = 0.73$ . In this paper, the refractive index of the silica background is  $n = 1.45$ .

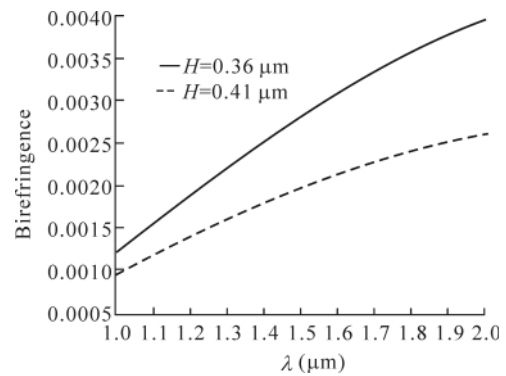


**Fig.1 Cross-section of the proposed PCF structure**

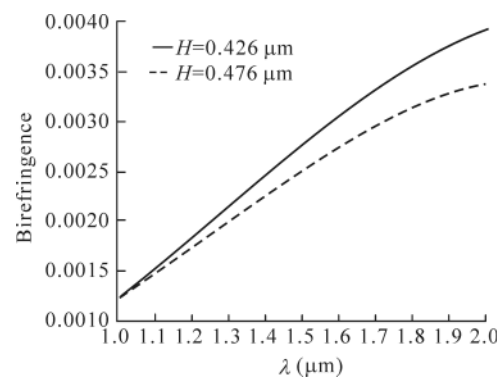
Fig.2 shows the birefringence of the fiber as a function of wavelength at different pitches of the two small air holes as  $H=0.36 \mu\text{m}$  and  $H=0.41 \mu\text{m}$  when the small air hole diameter is  $d=0.36 \mu\text{m}$ . It can be found that the birefringence increases with the increase of wavelength, and at the same wavelength, the smaller the air hole pitch  $H$ , the bigger the birefringence. At wavelength of  $\lambda=1550 \text{ nm}$ , while the pitches of the two small air holes are  $0.36 \mu\text{m}$  and  $0.41 \mu\text{m}$ , the birefringences are  $2.5 \times 10^{-3}$  and  $2.1 \times 10^{-3}$ , respectively.

Fig.3 shows the birefringence of the fiber as a function of wavelength at different pitches of the two small air holes as  $H=0.426 \mu\text{m}$  and  $H=0.476 \mu\text{m}$  when the small air hole diameter is  $d=0.426 \mu\text{m}$ . It can be found that the birefringence increases with the increase of wavelength. At wavelength of  $\lambda=1550 \text{ nm}$ , while the pitches of the two small air holes are  $0.426 \mu\text{m}$  and  $0.476 \mu\text{m}$ , the birefringences are  $3.0 \times 10^{-3}$  and  $2.7 \times 10^{-3}$ , respectively.

Figs.4 and 5 show the total dispersion of the  $\text{HE}_{11}^x$  mode and the  $\text{HE}_{11}^y$  mode of the fiber as a function of wavelength

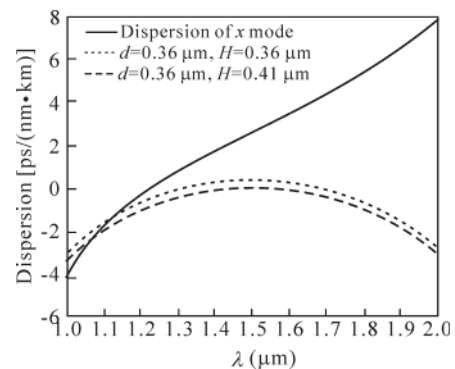


**Fig.2 Birefringence of the fiber as a function of wavelength when  $d=0.36 \mu\text{m}$**

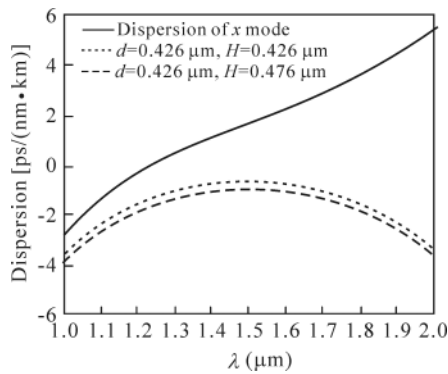


**Fig.3 Birefringence of the fiber as a function of wavelength when  $d=0.426 \mu\text{m}$**

with the small air hole diameter of  $d=0.36 \mu\text{m}$  and  $d=0.426 \mu\text{m}$ . It can be observed that from 1150 nm to 1850 nm, the total dispersion is less than  $2 \text{ ps}/(\text{nm} \cdot \text{km})$ . When  $d=0.36 \mu\text{m}$  and  $H=0.41 \mu\text{m}$ , the flattened dispersion from 1450 nm to 1590 nm is obtained, and the total dispersion is about  $-0.08 \text{ ps}/(\text{nm} \cdot \text{km})$ . That is in the single-mode optical fiber communication band place, which contains the short wavelength bands (1460 nm–1530 nm), the regular wavelength bands (1530 nm–1565 nm) and the long wavelength bands (1565 nm–1625 nm).

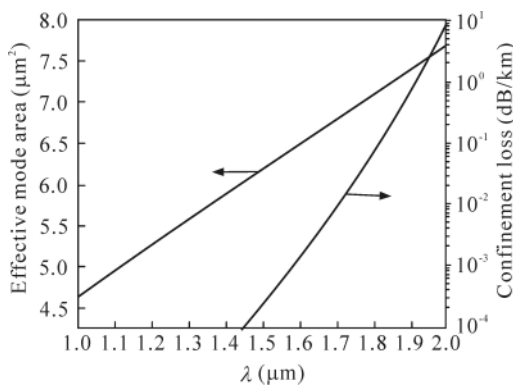


**Fig.4 Total dispersion of the  $\text{HE}_{11}^x$  mode and the  $\text{HE}_{11}^y$  mode of the fiber as a function of wavelength when  $d=0.36 \mu\text{m}$**

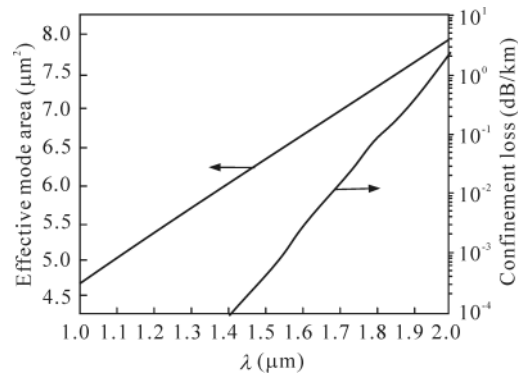


**Fig.5 Total dispersion of the  $HE_{x_{11}}$  mode and the  $HE_{y_{11}}$  mode of the fiber as a function of wavelength when  $d = 0.426 \mu\text{m}$**

A highly birefringent index-guiding PCF with flattened dispersion and low confinement loss is obtained by introducing two small air holes in the core area. The effective mode areas and the confinement losses of the  $y$ -polarized fundamental mode as a function of wavelength at  $d=0.36 \mu\text{m}$ ,  $H=0.36 \mu\text{m}$  and  $d=0.426 \mu\text{m}$ ,  $H=0.426 \mu\text{m}$  are shown in Figs.6 and 7, respectively. At wavelength of  $\lambda=1550 \text{ nm}$ , the birefringences are  $2.5 \times 10^{-3}$  and  $3.0 \times 10^{-3}$ , respectively, which are higher than those of the reported design<sup>[12]</sup>. It should be noted that the effective mode area is small, e.g. at  $\lambda=1550 \text{ nm}$ , the effective mode area of the  $y$ -polarized fundamental mode is as small as  $6 \mu\text{m}^2$  and  $6.5 \mu\text{m}^2$ , respectively. We also observe the remarkable low confinement loss of the proposed structure, e.g. at  $\lambda=1550 \text{ nm}$ , the confinement loss is  $0.006 \text{ dB/km}$  and  $0.001 \text{ dB/km}$ , respectively, which are lower than the reported  $0.01 \text{ dB/km}$ <sup>[12]</sup> and  $0.019 \text{ dB/km}$ <sup>[20]</sup>. The confinement loss is increased for introducing the elliptic air hole. Compared with introducing the elliptic air hole, the process of introducing circular air hole is easier.

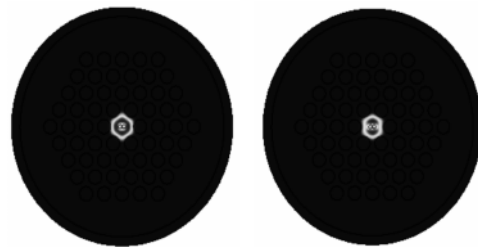


**Fig.6 Effective mode area and confinement loss of the  $y$ -polarized fundamental mode as a function of wavelength at  $d=0.36 \mu\text{m}$  and  $H=0.36 \mu\text{m}$**



**Fig.7 Effective mode area and confinement loss of the  $y$ -polarized fundamental mode as a function of wavelength at  $d=0.426 \mu\text{m}$  and  $H=0.426 \mu\text{m}$**

Fig.8 shows the normalized electric field distribution of the  $y$ -polarized fundamental mode at wavelength  $\lambda=1550 \text{ nm}$ . It is easy to find that the fundamental mode field energy is completely constrained in the core area.



(a)  $d=0.36 \mu\text{m}$ ,  $H=0.36 \mu\text{m}$  (b)  $d=0.426 \mu\text{m}$ ,  $H=0.426 \mu\text{m}$

**Fig.8 Normalized electric field distributions of the  $y$ -polarized fundamental mode at wavelength  $\lambda=1550 \text{ nm}$**

In this paper, a highly birefringent index-guiding PCF with flattened dispersion and low confinement loss is proposed by introducing two small air holes with the same diameter in the core area. The fundamental mode field, birefringence, confinement loss, effective mode area and dispersion characteristic of the fiber are studied by the full-vector FEM. The birefringence reaches the order of  $10^{-3}$  at the wavelength of  $1550 \text{ nm}$  by adjusting the parameters of the air holes, which is higher by about two orders of magnitude than the regular polarization maintaining fiber. At the same time, a low effective mode area of  $6 \mu\text{m}^2$  and low confinement loss of  $0.001 \text{ dB/km}$  are obtained. Furthermore, the flattened dispersion from  $1450 \text{ nm}$  to  $1590 \text{ nm}$  is obtained, and the total dispersion is about  $-0.08 \text{ ps}/(\text{nm} \cdot \text{km})$ , which is useful for the light signal transmission. Such a design provides a new approach to get a highly birefringent PCF with flattened dispersion and low confinement loss, and the fiber has a broad prospect of applications in the polarization control, nonlinear optics, dispersion control, etc.

## References

- [1] J. C. Knight, T. A. Braks, P. St. J. Russell and D. M. Atkin, *Optics Letters* **21**, 1549 (1996).
- [2] T. A. Birks, J. C. Knight and P. St. J. Russell, *Optics Letters* **22**, 961 (1997).
- [3] T. A. Braks, D. Mogilevtsev, J. C. Knight and P. St. J. Russell, *IEEE Photonics Technology Letters* **11**, 676 (1999).
- [4] W. J. Wadsworth, J. C. Knight, A. Ortigosa-Blanch, J. Arriaga, E. Silvestre and P. St. J. Russell, *Electronics Letters* **36**, 53 (2000).
- [5] A. Ferrando, E. Silvestre, J. J. Miret and P. Andres, *Optics Letters* **25**, 790 (2000).
- [6] HAN Ting-ting, LIU Yan-ge and WANG Zhi, *Journal of Optoelectronics • Laser* **23**, 215 (2012). (in Chinese)
- [7] I. Fsaifes, S. Cordette, A. Tonello, V. Couderc, C. Lepers, C. Ware, P. Leproux and C. Buy-Lesvigne, *IEEE Photonics Technology Letters* **22**, 1367 (2010).
- [8] YU Xing-yan, ZHOU Ya-xun, XU Yin-sheng, WANG Xun-si, ZHANG Pei-qing, TAO Guang-ming and DAI Shi-xun, *Journal of Optoelectronics • Laser* **23**, 915 (2012). (in Chinese)
- [9] ZHANG Shan-shan, ZHANG Wei-gang, LIU Zhuo-lin and LI Xiao-lan, *Journal of Optoelectronics • Laser* **22**, 685 (2011). (in Chinese)
- [10] M. Delgado-Pinar, A. Diez, S. Torres-Peiro, M. V. Andres, T. Pinheiro-Ortega and E. Silvestre, *Optics Express* **17**, 6931 (2009).
- [11] Z. Wu, D. X. Yang, L. Wang, L. Rao, L. Zhang, K. Chen, W. J. He and S. Liu, *Optics Laser Technology* **42**, 387 (2010).
- [12] D. J. J. Hu, P. P. Shum, C. Lu and G. Ren, *Optics Communications* **282**, 4072 (2009).
- [13] K. Saitoh, N. Florous and M. Koshiba, *Optics Express* **13**, 8365 (2005).
- [14] Huseyin Ademgil, Shyqyri Haxha and Fathi Abdel Malek, *Engineering* **2**, 608 (2010).
- [15] J. Liang, M. Yun, W. Kong, X. Sun, W. Zhang and S. Xi, *Optik* **122**, 2151 (2011).
- [16] S. S. A. Obayya, B. M. A. Rahman and K. T. V. Grattan, *Optoelectronics* **152**, 241 (2005).
- [17] J. Ju, W. Jin and M. S. Demokan, *IEEE Photonics Technology Letters* **15**, 1375 (2003).
- [18] S. Haxha and H. Ademgil, *Optical Communication* **281**, 278 (2008).
- [19] A. Ferrando, E. Silvestre, J. J. Miret and P. Andres, *Optical Express* **9**, 687 (2001).
- [20] S. S. Mishra and Vinod K. Singh, *Optik* **122**, 1975 (2011).
- [21] C. D. Ru and W. G. Zhu, *Applied Optics* **49**, 1682 (2010).