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可调谐太赫兹超材料吸波器研究进展

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摘要: 太赫兹超材料吸波器具有吸收强、厚度薄、质量轻等优点, 已被广泛应用于隐身材料、频率选择表面、太赫兹成像、通信传感等方面。但是, 基于金属结构的传统太赫兹超材料吸波器一旦完成加工后, 它的吸收性能是固定不变的。为解决这一问题, 研究人员通过引入活性超材料设计了可调谐太赫兹超材料吸波器。结合可调谐太赫兹超材料吸波器的国内外研究现状, 分类阐述了几类典型的可调谐太赫兹超材料吸波器, 重点对单频带、多频带、宽频带以及可切换双功能太赫兹超材料吸波器的相关研究工作进行了梳理与总结, 并对其未来发展趋势进行了分析。

关键词: 光电子学; 可调谐吸波器; 太赫兹波; 活性超材料

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Research progress of tunable terahertz metamaterial absorbers

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Abstract: Terahertz metamaterial absorber has the advantages of strong absorption, thin thickness and light weight, and has been widely used in stealth materials, frequency selective surfaces, terahertz imaging, communication sensing, and so on. However, as for the traditional terahertz metamaterial absorbers based on metal-patch, once they are processed, their absorption performance will be unchangeable. To solve this problem, researchers have designed tunable terahertz absorbers by adding active metamaterials. Combined with the research status of tunable terahertz metamaterial absorbers at

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home and abroad, this paper classifies and expounds several typical of tunable terahertz metamaterial absorbers, focusing on the research work of single-band, multi-band, broadband, and switchable dual-function terahertz metamaterial absorbers, and finally analyzes their future development trends.

Key words: optoelectronics; tunable absorber; terahertz wave; active metamaterial

0 引言

太赫兹 (THz) 波在 20 世纪 80 年代中后期被正式命名, 它是指频率范围在 0.1~10 THz 之间、波长在 0.03~3 mm 之间的电磁波。太赫兹频段既不能仅用光学理论来解释, 也不能只用微波理论来研究, 因此形成了太赫兹空隙 (THz gap)^[1,2]。近几十年来, 超快激光技术的发展为太赫兹脉冲提供了可靠、稳定的激发光源, 使得太赫兹技术的应用研究得到迅速发展, 太赫兹技术成为 21 世纪重要的科学技术之一。随着研究的不断深入, 不断设计制备出许多太赫兹功能器件, 如吸波器^[3,4]、滤波器^[5-7]、偏振转换器^[8,9]、超透镜^[10,11]、传感器^[12,13]等, 尤其是超材料吸波器具有吸收强、厚度薄、质量轻等优点, 并且可以“量需定制”。超材料是根据具体的应用需求, 通过对自然界中常规物质进行合理的人工参数设计来获得与原物质不同的具有超常物理性质的“新材料”^[14-17]。这种通过改变超材料的结构参数来影响整个器件吸收效果的方法, 极大程度上增加了吸波器设计的灵活性。超材料完美吸波器是由 Landy 等^[18]于 2008 年首次提出, 他们利用开口谐振环、介质层和金属线作为基元实现了在微波频段的完美吸收, 不受传统吸波厚度限制, 尺寸较小。这项开创性工作很快激发了其他频率领域的相关工作, 其中对太赫兹波频段的研究也逐渐开展^[19-22], 其经典结构是金属-介质-金属 (MDM) 的三明治结构。但是基于金属的吸波器一旦完成结构的加工, 其吸收性能往往是固定不变的。如果有其他频率的吸波需求, 就必须重新进行设计和加工, 很大程度上限制了吸波器的发展和应用。

为解决这一问题, 研究人员设计加工了可调谐太赫兹超材料吸波器, 这类吸波器可以在不改变本身结构参数的基础上, 利用结构中所添加活性材料的可调性质来实现吸收性能的动态调节。例如, 石墨烯的电导率与其费米能级有关, 费米能级可以通过外界电压来控制; VO₂ 的电导率与温度有关, 可以随着温度变化实现绝缘态向金属态的转变。此外还可以通过电、热、光激发^[23-26]等方式调控材料的性质, 从而实现太赫兹超材料吸波器的可调谐特性。可调谐太赫兹超材料吸波器可以广泛应用于隐身材料、频率选择表面、太赫兹成像、通信传感、光学调控等方面。随着国内外研究的不断深入, 为了适用更多更宽的吸波需求, 已从最初的单频带可调谐太赫兹吸波器扩展到多频带和宽频带可调谐太赫兹吸波器。

近年来, 可切换多功能太赫兹吸波器逐渐成为研究的重点方向。本文结合国内外研究现状对可调谐太赫兹超材料吸波器的发展和趋势进行分析与探讨。

1 可调谐太赫兹超材料吸波器的发展

2008 年, Tao 等^[27]设计了一种基于三层结构的太赫兹超材料吸波器。如图 1(a), 该吸波器最上层是作为谐振单元的金属结构, 中间是介质层, 最下层是金属底板; 图 1(b) 表明在 TE 和 TM 两种偏振模式下, 该结构都可以在 1.6 THz 频率处实现高达 99.9% 的吸收率。对加工后的器件进行实验测试, 实验结果表明在 1.6 THz 频率处该结构仍具有 96% 的高吸收率。自此, 太赫兹频段吸波器的研究与设计受到国内外的广泛关注。

2015 年, Wang 等^[28]提出了具有多频带吸收效果的太赫兹超材料吸收器, 由四个尺寸不同的金属方环、

介质层和金属底层组成, 如图 1(c) 所示。该吸波器在 0.777、1.13、1.53、2.06 THz 频率处的吸收率分别达到 99.41%、97.53%、99.06% 和 95.59%。通过对吸波器四个吸收频率处进行电场分析, 得出吸收器的吸收机理是四种不同尺寸金属方环激发共振频率的重叠。所以每一个吸收频率可以通过改变相应金属方环的尺寸来实现灵活调控, 如图 1(d) 所示。这种设计理念可以在多频带吸波器的设计方面进行拓展, 如通过增加金属环实现五频带吸波。

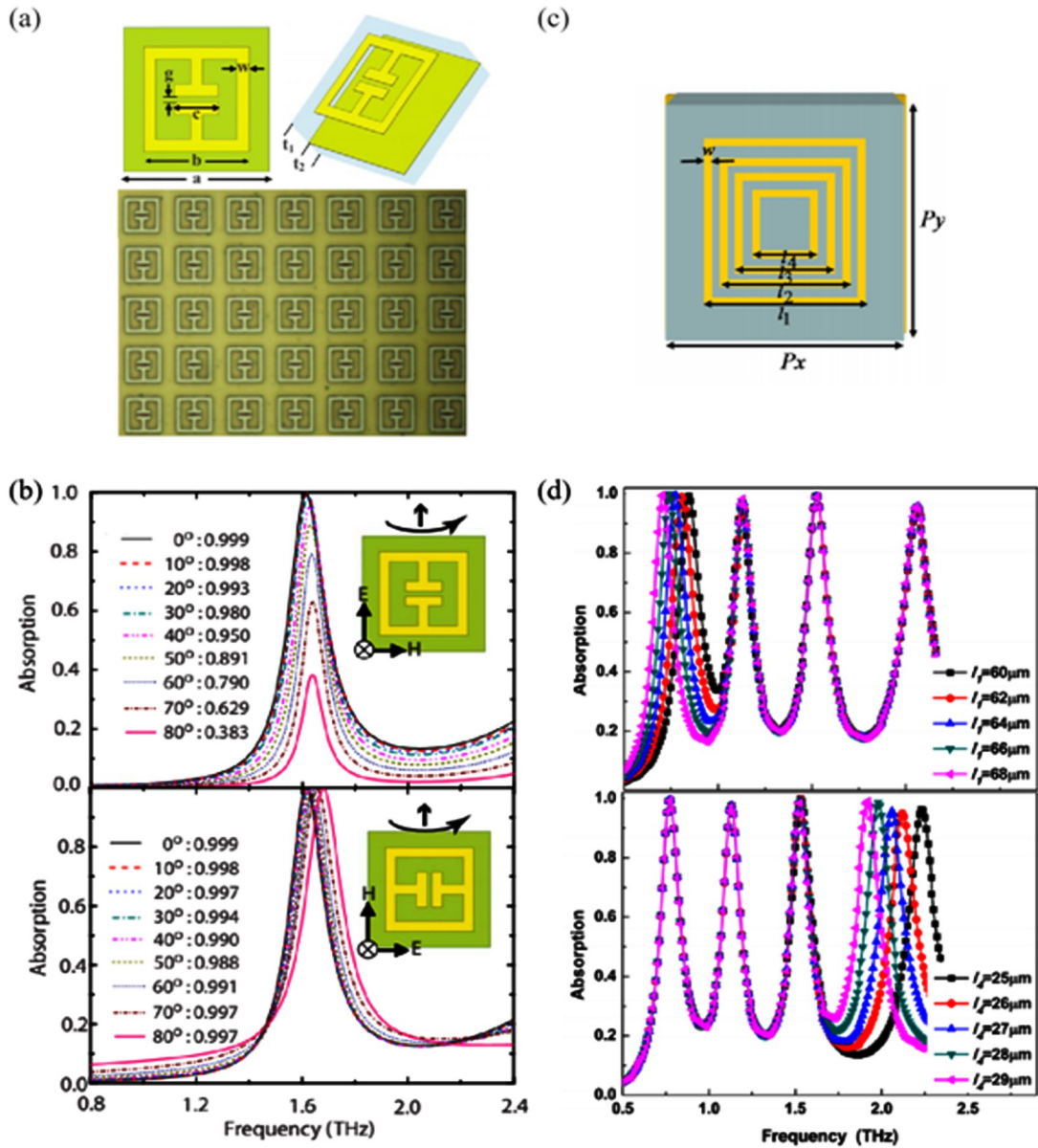


图 1 基于金属贴片的太赫兹吸波器。Tao 等^[27]提出的基于三层结构的太赫兹超材料吸波器的 (a) 结构示意图与 (b) 在 TE 和 TM 偏振模式下不同入射角时的吸收曲线; Wang 等^[28]提出的具有多频带吸收效果的太赫兹超材料吸收器的 (c) 结构示意图与 (d) 吸收曲线随着长度 l_1 和 l_4 的可调谐变化

Fig. 1 Terahertz absorber based on metal-patch. (a) Schematic diagram of structure and (b) the absorption curve at different incident angles under TE and TM polarization of the terahertz metamaterial absorber based on three-layer structure proposed by Tao *et al*^[27]; (c) Schematic diagram of structure and (d) the tunable changes of absorption curves depend on length l_1 and l_4 of the terahertz metamaterial absorber with multiband absorption proposed by Wang *et al*^[28]

从仿真设计上来说,上述基于金属方环的吸波器可以称为吸收频率可调谐的太赫兹超材料吸波器,它可以通过调整单个金属环的尺寸来实现对吸收频率的位置移动。但是这类吸波器一旦完成加工制备,其结构尺寸就固定了,只能满足固定频率的吸波需求。如果需要改变吸收频率的位置或者强度,就必须重新进行设计和加工。为解决这一问题,研究人员引入了活性材料(如 VO_2 、石墨烯、狄拉克半金属等)来设计可调谐太赫兹超材料吸波器。这类吸波器不需要改变其结构参数,而是利用组成材料的可调性质来实现吸波器的可调谐特性。图2给出了可调谐太赫兹超材料吸波器的发展历程:单频带可调谐太赫兹超材料吸波器^[34-45],多频带可调谐太赫兹超材料吸波器^[46-63],宽频带可调谐太赫兹超材料吸波器^[64-84]和可切换双功能太赫兹超材料吸波器^[32, 33, 85-101]等。

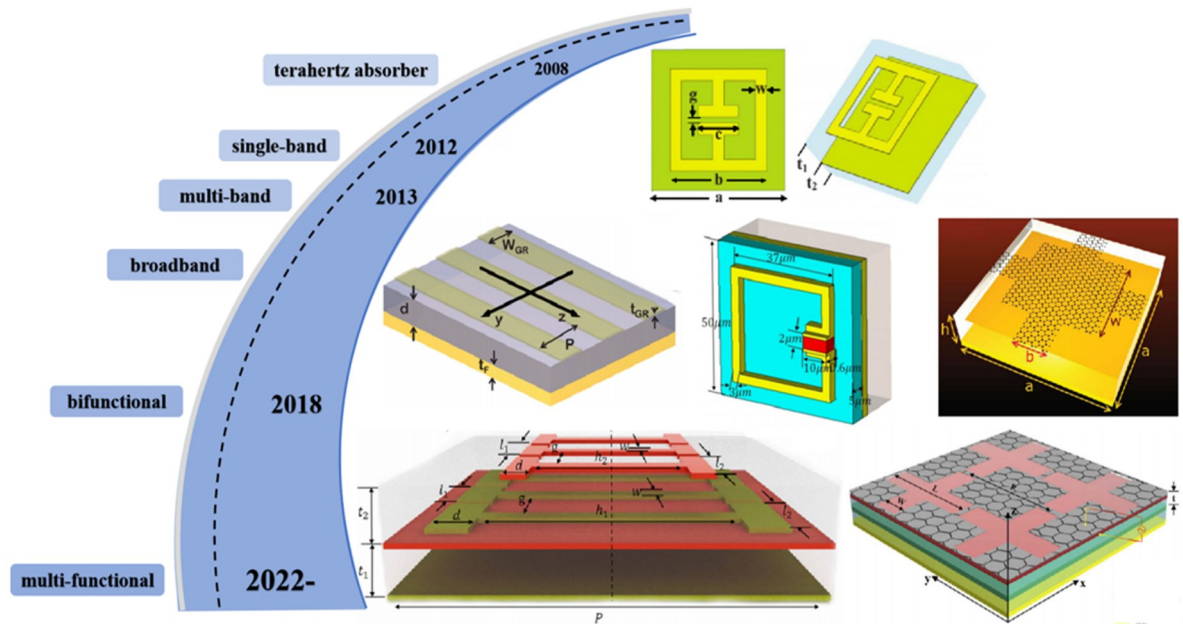


图2 可调谐太赫兹超材料吸波器发展历程图^[27, 29-33]

Fig. 2 Research history of tunable terahertz metamaterial absorber^[27, 29-33]

1.1 单频带可调谐太赫兹超材料吸波器

单频带可调谐太赫兹超材料吸波器只具有一个近乎完美吸收效果的吸收频率点,大多用于频率选择表面、通信传感等方面。通过调控组成材料的可调参数,吸波器实现了多个频率点的选择调谐功能,拥有较高的灵活性。对于传感方面的应用,由于金属具有较大的损耗,研究人员一直致力于提高吸波器的品质因子、灵敏度等指标。

2018年, Liu等^[34]提出一种基于狄拉克半金属的窄带可调谐太赫兹吸波器。如图3(a),该吸波器由带圆孔的光子晶体板(折射率为3.416)和狄拉克半金属板(BDSs)组成。由图3(b)可知,当狄拉克半金属的费米能级固定为65 meV时,仿真结果表明该吸波器在 $f_0 = 1.3898$ THz频率处实现了完美吸收,半高全宽 $\Delta f = 1.469 \times 10^{-2}$ THz,品质因子为94.6 ($Q = f_0/\Delta f$);在狄拉克半金属的费米能级从50 meV变化到80 meV的过程中,吸收频率可以实现从1.381 THz到1.395 THz频率范围的动态调节,这个过程中吸收率始终保持在95%以上。与之前的工作相比,这种设计不仅结构简单,而且结合狄拉克半金属材料实现了吸收频率的可调。

2019年, Huang等^[35]提出了一种基于混合材料的可调谐太赫兹超材料吸波器。如图3(c),该吸波器结构从上到下依次是石墨烯层、钛酸锶(STO)层、介质层和金属层,仿真结果表明该吸波器在0.43 THz频率处

实现了完美吸收。通过单独调节石墨烯和STO的相关参数, 这种吸波器能够分别实现吸收率和吸收频率的可调谐变化。在石墨烯的费米能级从0 eV增加到0.7 eV的过程中, 吸波器的吸收率实现了从35%到100%的动态调节, 如图3(d)所示; 当STO材料的温度从200 K变化到400 K时, 中心频率由0.30 THz移动到0.43 THz, 这个过程中吸收率始终保持在99%以上, 如图3(d)所示。该吸波器可以扩展到红外和可见光频段, 并在成像、传感和太阳能方面有重要的应用。表1为单频带可调谐太赫兹超材料吸波器的部分研究工作的汇总。

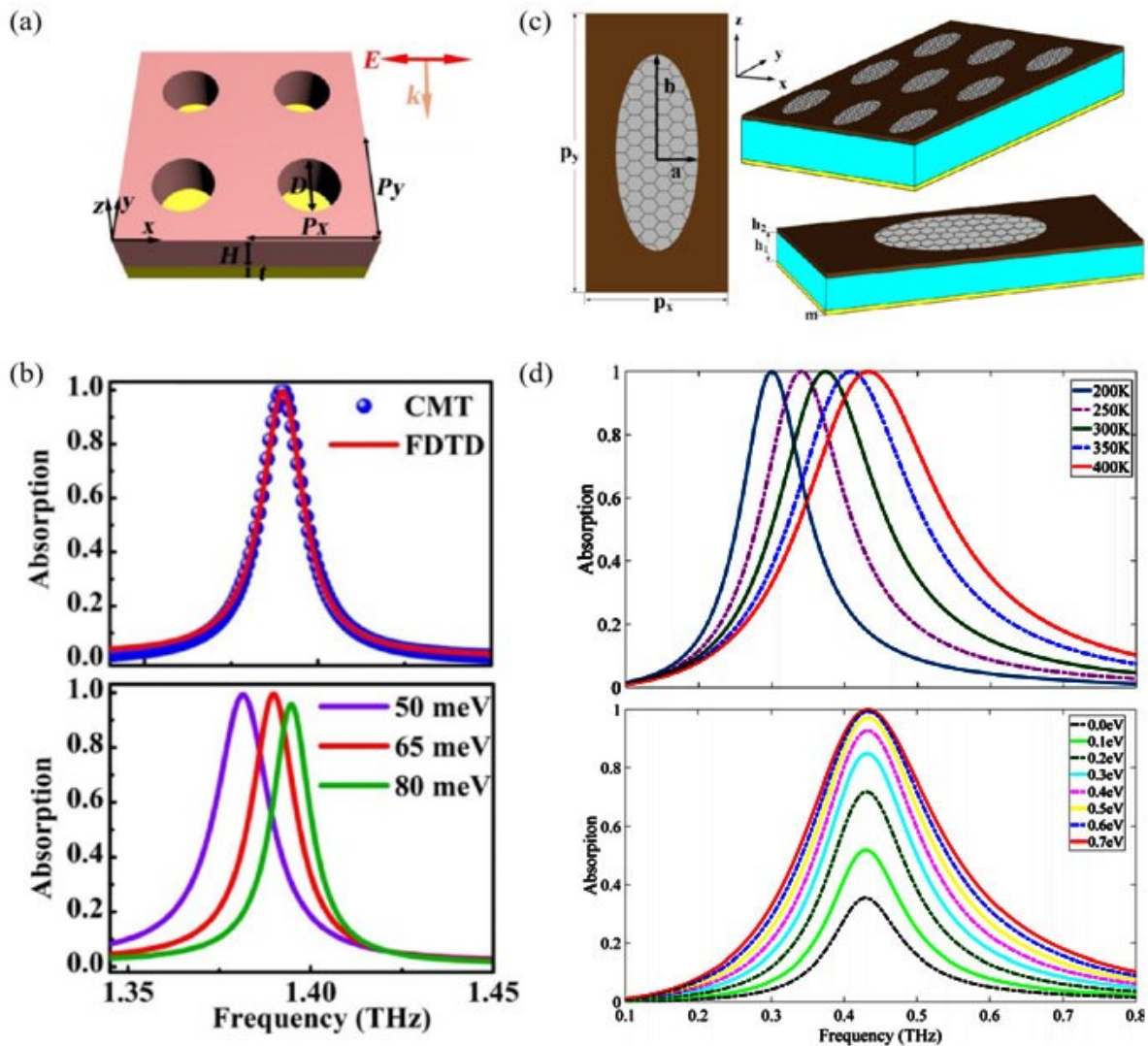


图3 单频带可调谐太赫兹超材料吸波器。Liu等^[34]提出的基于狄拉克半金属的窄带可调谐太赫兹吸波器的(a)结构示意图与(b)吸收曲线随着不同费米能级的可调谐变化; Huang等^[35]提出的基于混合材料的可调谐太赫兹超材料吸波器的(c)结构示意图与(d)吸收曲线随着不同温度和费米能级的可调谐变化

Fig. 3 Single-band tunable terahertz metamaterial absorber. (a) Schematic diagram of structure and (b) the tunable changes of absorption curves depend on different Fermi energy level of the narrow band tunable terahertz absorber based on Dirac semi-metal proposed by Liu *et al* ^[34]; (c) Schematic diagram of structure and (d) the tunable changes of absorption curves depend on different temperature and Fermi energy level of the tunable terahertz metamaterial absorber based on hybrid materials proposed by Huang *et al* ^[35]

表1 单频带可调谐太赫兹超材料吸波器汇总

Table 1 Summary of single-band tunable terahertz metamaterial absorber

Layer	Material	Parameter	Frequency	Absorptance	Function	Reference
3	Graphene	E_f : 0~0.6 eV	0.48~1.579 THz	>99%		[36]
3	Dirac semimetal	E_f : 65~85 meV	2.46~3.16 THz	>95%		[37]
4	Dirac semimetal Strontium titanate	E_f : 10~80 meV T : 300 K	3.265~4.82 THz	70%~99.9%	Single-band tunable terahertz metamaterial absorber	[38]
		T : 200~300 K E_f =40 meV	2.665~3.69 THz	>99%		
3	Strontium titanate	T : 200~400 K	1.71~2.48 THz	>99%		[39]
7	Liquid crystal	V : 0~saturation	red shift	>90%		[40]
4	InSb	T : 160~350 K	0.82~1.02 THz	>88.7%		[41]
3	Photoconductive silicon	σ : $1\sim 1\times 10^5$ S/m		0%~100%		[42]

notes V : bias voltage; T : temperature; E_f : Fermi energy level; σ : conductivity

1.2 多频带可调谐太赫兹超材料吸波器

多频带吸收的吸波器可以通过两种方法实现, 其一是垂直方向的多层结构叠堆, 每层结构使用不同的谐振单元, 通过合理设计每层结构之间的介质层厚度来达到多频带吸收效果^[46, 47]; 其二是水平方向谐振单元组合的方法, 在同一个平面内组合不同材料、不同形状、不同尺寸大小或不同旋转角度的谐振单元, 利用不同谐振单元激发吸收频率的叠加也可以实现多频带吸收效果^[48, 49]。多频带可调谐太赫兹超材料吸波器可以同时满足多个吸收频率的工作需求。

2017年, Chen等^[50]首先设计了一个具有三层结构的单频带可调谐太赫兹超材料吸波器, 该吸波器最上层是石墨烯层, 中间是介质层, 底层为金属层。当石墨烯的费米能级固定为0.9 eV时, 该吸波器在2.71 THz处的吸收率高达99.51%。然后Chen等通过将相同参数的“石墨烯-介质”结构重复叠加到原有结构上进而实现了双频带的吸波效果, 如图4(a)所示。双频带吸波器在1.99 THz和2.69 THz处分别具有98.94%和99.10%的高吸收率。在调整石墨烯的费米能级从0.6 eV变化到0.9 eV的过程中, 两个吸收频率的位置和吸收强度都发生了显著变化, 如图4(b)所示。

2019年, Zhang等^[51]设计了一个基于狄拉克半金属的双频带可调谐太赫兹超材料吸波器。如图4(c), 该吸波器由环形介质层和狄拉克半金属层组成。当狄拉克半金属的费米能级固定为75 meV时, 该吸波器在2.02 THz和2.49 THz处实现完美的吸收效果, 对应的吸收率均大于99%。由图4(d)可知, 在调整费米能级从55 meV变化到85 meV的过程中, 吸波器的吸收率实现了90%到99%的动态调节。表2为多频带可调谐太赫兹超材料吸波器的部分研究工作的汇总。

表 2 多频带可调谐太赫兹超材料吸波器汇总

Table 2 Summary of multi-band tunable terahertz metamaterial absorber

Layer	Material	Parameter	Frequency	Absorptance	Function	Reference
3	Graphene	E_f : 0.6~0.9 eV	7.1~8.7 THz 10.4~12.7 THz	>85%	Dual-band absorption	[52]
3	Dirac semimetal VO ₂	σ : 10~10 ⁵ S/m E_f =0.13 eV		6.5%~97.8% 10%~99.27% 9%~99.54%	Triple-band absorption	[53]
		E_f : 0.11~0.15 eV σ =10 ⁵ S/m	blue shift	>90%		
3	Strontium titanate	T : 200~500 K	blue shift	>95%	Dual-band absorption	[54]
7	Liquid crystal	V : 0~12 V	red shift	>80.1%	Dual-band absorption	[55]

notes V : bias voltage; T : temperature; E_f : Fermi energy level; σ : conductivity

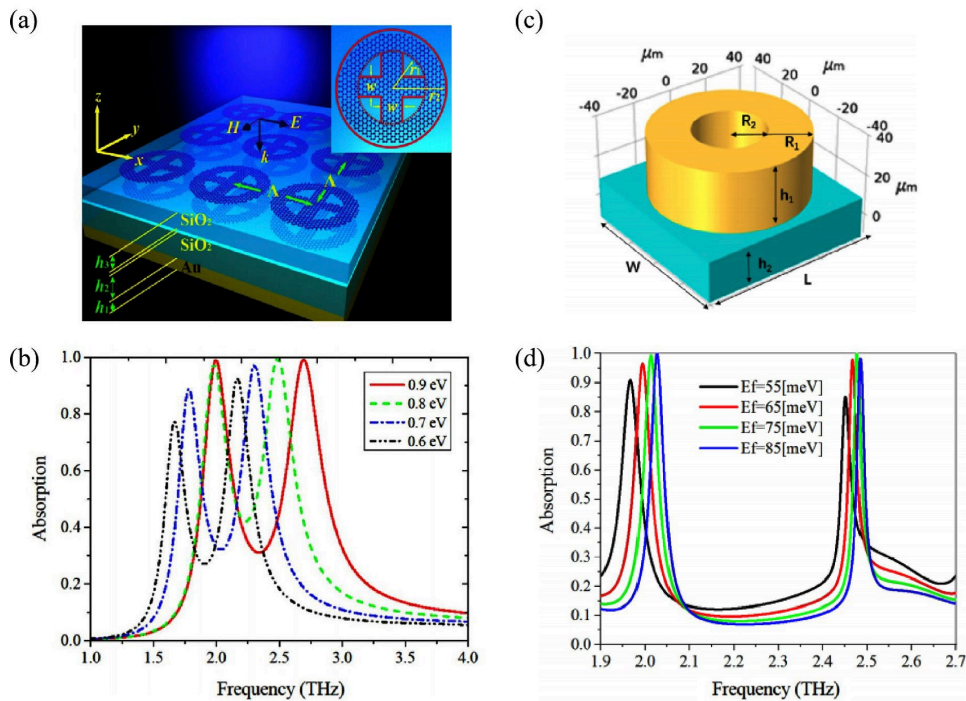


图 4 多频带可调谐太赫兹超材料吸波器。Chen 等^[50]提出的具有五层结构的双频带可调谐太赫兹超材料吸波器的 (a) 结构示意图与 (b) 吸收曲线随着不同费米能级的可调谐变化; Zhang 等^[51]提出的基于狄拉克半金属的双频带可调谐太赫兹超材料吸波器的 (c) 结构示意图与 (d) 吸收曲线随着不同费米能级的可调谐变化

Fig. 4 Multi-band tunable terahertz metamaterial absorber. (a) Schematic diagram of structure and (b) the tunable changes of absorption curves depend on different Fermi energy level of the double band tunable terahertz metamaterial absorber with five layers proposed by Chen *et al* ^[50]; (c) Schematic diagram of structure and (d) the tunable changes of absorption curves depend on different Fermi energy level of the double band tunable terahertz absorber based on Dirac semi-metal proposed by Zhang *et al* ^[51]

1.3 宽频带可调谐太赫兹超材料吸波器

与多频带吸波器的实现方法相似, 当不同谐振单元激发的吸收频率之间的距离较远时, 可以实现多个独

立的吸收频率的多频带吸收效果;而当距离较近时,多个吸收频率可以通过叠加来实现宽频带的吸收效果。宽频带可调谐太赫兹超材料吸波器目前主要研究的是如何扩展吸收带宽,以实现宽频带的频率响应。近五年来,随着研究人员的深入探索,这类研究成果不断得到突破。例如基于VO₂的宽频带可调谐太赫兹吸波器具有90%以上吸收率的吸收带宽达到了4.10 THz^[64]。

2018年, Song等^[65]提出了一个基于VO₂的窄带可调谐太赫兹吸波器。如图5(a)所示,其由十字型金棒、SiO₂介质层和VO₂层组成, SiO₂作为基底。当VO₂的电导率为 $2 \times 10^3 \Omega^{-1} \cdot \text{cm}^{-1}$ 时,该吸波器具有90%以上吸收率的吸收带宽达到了0.33 THz。由图5(b)可知,当VO₂的电导率从 $10 \Omega^{-1} \cdot \text{cm}^{-1}$ 变化到 $2 \times 10^3 \Omega^{-1} \cdot \text{cm}^{-1}$ 的过程中,吸收率可以实现30%到100%的动态调节。

2018年, Mou等^[66]设计了一个基于石墨烯的宽频带可调谐太赫兹吸波器。如图5(c),其由单层石墨烯同心双环阵列、SiO₂介质层和金层组成。当石墨烯的费米能级固定为0.5 eV时,该结构在1.18 THz到1.64 THz频率范围内的吸收率高达90%以上,吸收带宽达到了0.46 THz。在石墨烯的费米能级从0.35 eV变化到0.65 eV的过程中,保持80%以上吸收率的吸收频带从0.98~1.36 THz移动到1.36~1.94 THz,如图5(d)所示。表3为宽频带可调谐太赫兹超材料吸波器的部分研究工作的汇总。

表3 宽频带可调谐太赫兹超材料吸波器汇总

Table 3 Summary of broadband tunable terahertz metamaterial absorber

Layer	Material	Parameter	Frequency	Absorptance	Function	Reference
4	Dirac semimetal Strontium titanate	$E_f: 40 \sim 0 \text{ meV}$ $T=300 \text{ K}$	unchanged 1.43~1.58 THz	>80%	BW=0.65 THz (absorptance>80%)	[67]
		$T: 250 \sim 400 \text{ K}$ $E_f=45 \text{ meV}$	1.14~1.35 THz 1.51~1.76 THz	>80%		
3	Graphene	$E_f: 0 \sim 0.7 \text{ eV}$		1%~99%	BW=0.76 THz (absorptance>90%)	[68]
3	Graphene	$E_f: 0.6 \sim 1.0 \text{ eV}$	3.35~4.15 THz	>70%	BW=1.13 THz (absorptance>90%)	[69]
5	Graphene	$E_f: 0.7 \sim 1.1 \text{ eV}$	2.86~5.08 THz ~ 3.16~6.01 THz	>85%	BW=2.85 THz (absorptance>90%)	
4	Graphene VO ₂	$\sigma: 10 \sim 2 \times 10^5 \text{ S/m}$ $E_f=0.1 \text{ eV}$		28%~99%	BW=1.70 THz (absorptance>90%)	[70]
		$E_f: 0.1 \sim 0.6 \text{ eV}$ $\sigma=2 \times 10^5 \text{ S/m}$	Blue shift	>90%		
3	Dirac semimetal	$E_f: 40 \sim 80 \text{ meV}$	Blue shift		BW=2.70 THz (absorptance>90%)	[71]

Continued

Layer	Material	Parameter	Frequency	Absorptance	Function	Reference
3	VO ₂	σ : 200 ~ 2×10 ⁵ S/m		4%~100%	BW=4.10 THz (absorptance>90%)	[64]
5	Graphene Dirac semimetal	E_f : 0 ~ 1.7 eV E_f = 60 meV E_f : 10~100 meV E_f =1.7 eV	5~7.44 THz ~ 4.79~8.99 THz Blue shift	>80%	BW=4.20 THz (absorptance>90%)	[72]

notes T : temperature; E_f : Fermi energy level; σ : conductivity; BW; bandwidth

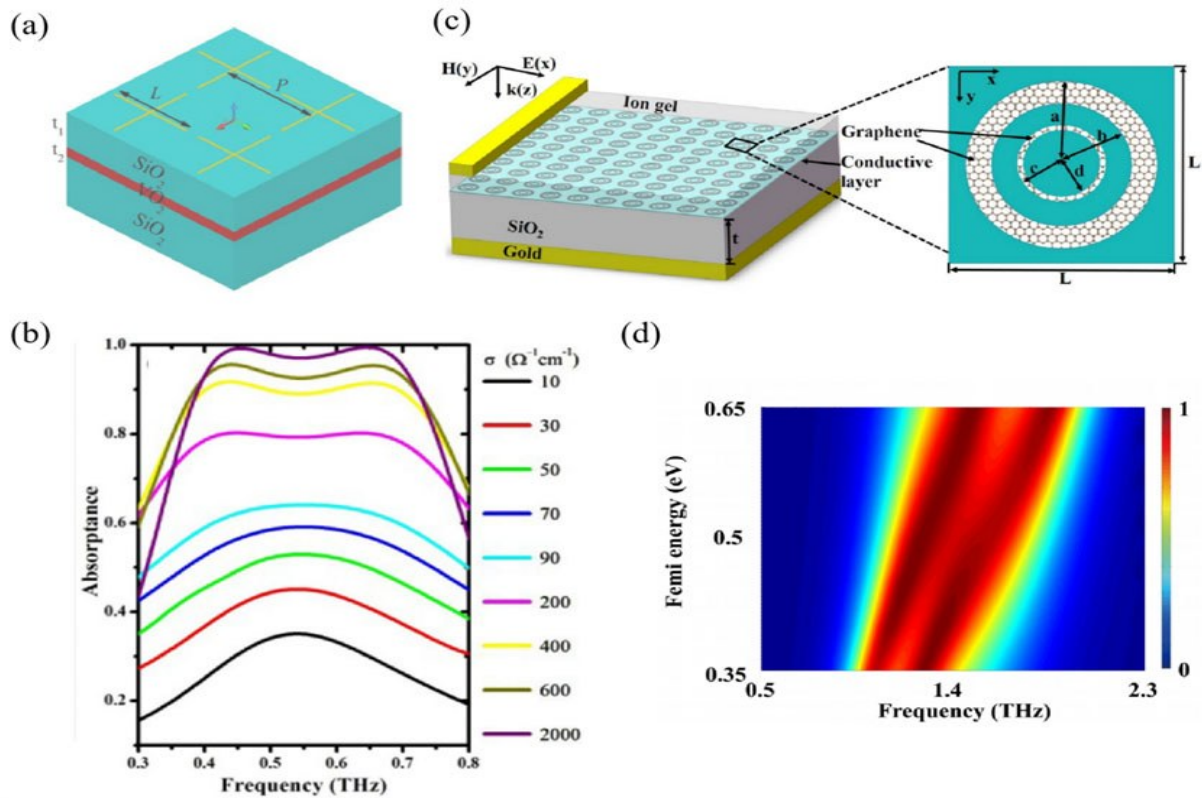


图5 宽频带可调谐太赫兹超材料吸波器。Song等^[65]提出的基于VO₂的窄带可调谐太赫兹吸波器的(a)结构示意图与(b)吸收曲线随着不同电导率的可调谐变化; Mou等^[66]提出的基于石墨烯的宽频带可调谐太赫兹吸波器的(c)结构示意图与(d)吸收曲线随着不同费米能级的可调谐变化

Fig. 5 Broadband tunable terahertz metamaterial absorber. (a) Schematic diagram of structure and (b) the tunable changes of absorption curves depend on different conductivity of the narrow band tunable terahertz absorber based on vanadium oxide proposed by Song *et al*^[65]; (c) Schematic diagram of structure and (d) the tunable changes of absorption curves depend on different Fermi energy level of the wide band tunable terahertz absorber based on graphene proposed by Mou *et al*^[66]

1.4 可切换双功能太赫兹超材料吸波器

VO₂的相变特性为可切换双功能太赫兹吸波器的设计提供了开阔的思路。当VO₂处于绝缘态时,它只起

到介质层的作用; 而当 VO_2 为金属态时, 它可以作为一层金属反射板, 位于 VO_2 下层的结构可以忽略不计, 所以可切换双功能太赫兹超材料吸波器可以看作是两类吸波器结构的堆叠。

2018年, Zhao等^[32]提出了一种具有双宽频带可切换的太赫兹超材料吸波器。该团队首先设计了一个基于金属结构的吸波器, 由I型金层阵列、介质层和底层金膜组成。仿真结果表明该吸波器在1.12~1.25 THz频率范围的吸收率高达90%以上。随后基于 VO_2 的相变特性提出了一种具有六层结构的可切换太赫兹吸波器, 如图6(a), 从上到下依次为I型 VO_2 层、介质层I、I型金层阵列、 VO_2 薄板、介质层II和底部金层。当 VO_2 处于绝缘态时, 该器件展现的是一个在0.76~0.86 THz频率范围内具有90%以上吸收率的宽带吸波器; 随着温度的升高, VO_2 切换为金属态的同时, 吸波器的吸收频带也切换到1.12~1.25 THz, 此时器件仍是具有90%以上吸收率的宽带吸波器, 如图6(b)所示。

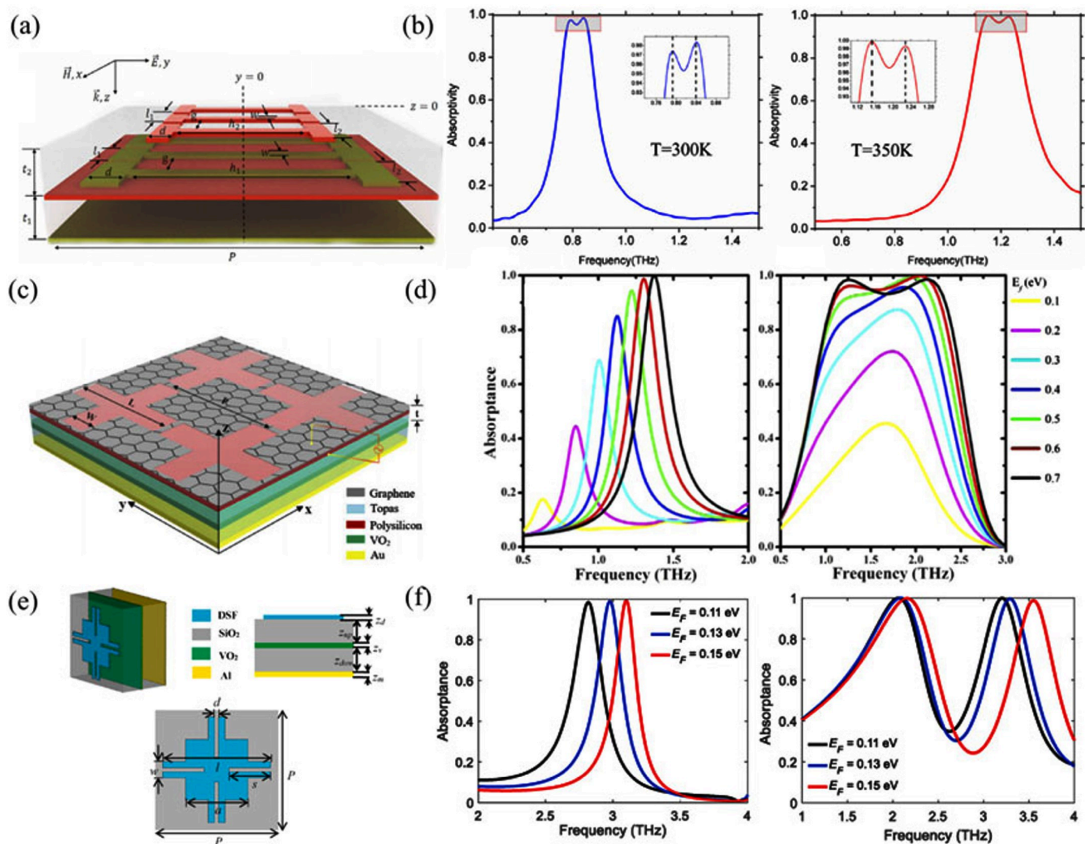


图6 可切换双功能可调谐太赫兹超材料吸波器。Zhao等^[32]提出的双宽频带可切换的太赫兹超材料吸波器的(a)结构示意图与(b)吸收曲线随着不同温度的可调谐变化; Zhang等^[33]提出的基于石墨烯和 VO_2 混合材料的宽频带和窄频带可切换双功能太赫兹吸收器的(c)结构示意图与(d)吸收曲线随着不同费米能级的可调谐变化; Li等^[85]提出的基于狄拉克半金属和 VO_2 混合材料的可切换双功能太赫兹吸波器的(e)结构示意图与(f)吸收曲线随着不同费米能级的可调谐变化

Fig. 6 Switchable bifunctional terahertz metamaterial absorber. (a) Schematic diagram of structure and (b) the tunable changes of absorption curves depend on different temperature of the double broadband switchable terahertz absorber proposed by Zhao *et al*^[32]; (c) Schematic diagram of structure and (d) the tunable changes of absorption curves depend on different Fermi energy level of the wide band and narrow band switchable dual function terahertz absorber based on graphene and vanadium dioxide composite proposed by Zhang *et al*^[33]; (e) Schematic diagram of structure and (f) the tunable changes of absorption curves depend on different Fermi energy level of the switchable bifunctional terahertz absorber based on Dirac semi metal and vanadium dioxide proposed by Li *et al*^[85]

2020年, Zhang等^[33]提出了一种基于石墨烯和VO₂混合材料的具有宽频带和窄频带的可切换双功能太赫兹吸波器。如图6(c), 该吸波器由五部分组成: 石墨烯阵列、topas介质层 I (介电常数为2.35)、VO₂薄膜、topas介质层 II 和底部金层。当石墨烯的费米能级固定为0.7 eV 并且VO₂处于金属态时, 器件为窄频带吸波器。窄频带吸波器的有效结构由上层石墨烯、topas介质层 I 和金属态的VO₂薄膜组成, 仿真结构表明它在1.37 THz处实现了吸收率为100%的完美吸收。当VO₂转变为绝缘态时, 器件切换为一个具有1.3 THz吸收带宽的宽带吸波器, 它在1.05~2.35 THz频率范围内具有90%以上的高吸收率。由图6(d)可知, 在石墨烯的费米能级从0.1 eV变化到0.7 eV的过程中, 两类吸波器的吸收频率和吸收率都可以实现动态调节。结果表明随着费米能级的增加, 窄频带吸波器的吸收频率向高频方向移动的同时伴随着吸收率的逐渐增加; 对于宽带吸波器来说, 随着费米能级的增加, 吸波器的吸收率实现了从45.5%到100%的动态调节。

2021年, Li等^[85]提出了一种基于狄拉克半金属和VO₂混合材料的可切换双功能太赫兹吸波器。如图6(e), 该吸波器由五部分组成: 狄拉克半金属层、SiO₂介质层 I、VO₂薄膜、SiO₂介质层 II 和底部金层。假设VO₂处于绝缘态和金属态的电导率分别是10 S·m⁻¹和5×10⁴ S·m⁻¹。仿真结果表明该器件可以通过控制VO₂的电导率, 实现单频带吸波器和双频带吸波器之间的功能切换。当狄拉克半金属的费米能级固定为0.11 eV 并且VO₂处于绝缘态时, 器件为在2.82 THz处具有98%吸收率的单频带吸波器。当VO₂切换到金属态时, 器件转变为双频带吸波器, 它在2.06 THz和3.21 THz处均实现了吸收率为99.9%的完美吸收。吸波器的可调谐特性可以通过改变狄拉克半金属的费米能级来实现。在费米能级从0.11 eV变化到0.15 eV的过程中, 两种类型吸波器的吸收频率都向高频方向移动, 同时均保持良好的吸收性能, 如图6(f)所示。表4为可切换双功能太赫兹超材料吸波器的部分研究工作的汇总。

表4 可切换双功能太赫兹超材料吸波器汇总

Table 4 Summary of switchable bifunctional terahertz metamaterial absorber

Layer	Material	Parameter	Frequency	Absorptance	Function	Reference
6	VO ₂	$\sigma: 0 \sim 10^5 \text{ S/m}$			Narrowband absorption switch to broadband absorption	[86]
		$\sigma: 40 \sim 2 \times 10^5 \text{ S/m}$ $E_f = 0.7 \text{ eV}$ $E_f: 0 \sim 0.7 \text{ eV}$ $\sigma = 40 \text{ S/m}$		20%~100%	BW=1.52 THz(absorptance>90%)	
5	Graphene VO ₂	$E_f: 0.5 \sim 1.0 \text{ eV}$ $\sigma = 2 \times 10^5 \text{ S/m}$	1~1.1 THz 2.2~2.65 THz 2.55~3.16 THz	>90%	triple-band absorption	[87]
		$\sigma: 200 \sim 2 \times 10^5 \text{ S/m}$ $E_f = 0.9 \text{ eV}$ $\sigma = 2 \times 10^5 \text{ S/m}$		>90%	six-band absorption switch to broadband absorption BW=3.83 THz(absorptance>90%)	[88]

Continued

Layer	Material	Parameter	Frequency	Absorptance	Function	Reference
		$E_f: 0 \text{ eV} \sim 1.0 \text{ eV}$ $\sigma = 200 \text{ S/m}$	blue shift	>85.1%	six-band absorption	
6	Graphene VO ₂	$\sigma: 0 \text{ S/m} \sim 2 \times 10^5 \text{ S/m}$ $E_f = 0.7 \text{ eV}$			broadband absorption switch to broadband absorption	
		$\sigma = 2 \times 10^5 \text{ S/m}$		>90%	BW=2.25 THz(absorptance>90%)	[89]
		$E_f: 0.01 \text{ eV} \sim 0.7 \text{ eV}$ $\sigma = 200 \text{ S/m}$		5.2%~ 99.8%	bandwidth=1.20 THz(absorptance> 90%)	
4	Graphene	$E_f: 150 \text{ meV} \sim 550 \text{ meV}$			broadband absorption switch to triple-band absorption	[90]
3	Photoconductive silicon	$\sigma: 1 \text{ S/m} \sim 5 \times 10^5 \text{ S/m}$	red shift		dual-band absorption switch to single-band absorption	[91]
5	Photoconductive silicon VO ₂	$\sigma(\text{Si}): 2.5 \times 10^4 \text{ S/m}$ $\sigma(\text{VO}_2): 2 \times 10^5 \text{ S/m}$		>90%	BW=4.66 THz(absorptance>90%)	
		$\sigma(\text{Si}): 8 \times 10^4 \text{ S/m}$ $\sigma(\text{VO}_2): 20 \text{ S/m}$		>90%	dual-band absorption	
		$\sigma(\text{Si}): 2.5 \times 10^4 \sim 3 \times 10^5 \text{ S/m}$ $\sigma(\text{VO}_2) = 20 \text{ S/m}$		4%~99%		
		$\sigma(\text{Si}): 2.5 \times 10^4 \sim 3 \times 10^5 \text{ S/m}$ $\sigma(\text{VO}_2) = 2 \times 10^5 \text{ S/m}$		60%~99%		[92]
		$\sigma(\text{VO}_2): 20 \sim 2 \times 10^5 \text{ S/m}$ $\sigma(\text{Si}) = 2.5 \times 10^4 \text{ S/m}$ $\sigma(\text{VO}_2): 20 \sim 2 \times 10^5 \text{ S/m}$ $\sigma(\text{Si}) = 8 \times 10^4 \text{ S/m}$		2%~99% 69%~99%		

notes T : temperature; E_f : Fermi energy level; σ : conductivity; BW: bandwidth

2 总结和展望

传统的基于金属贴片的太赫兹吸波器由于工作频率固定的局限性,限制了吸波器的实际应用。近年来,基于活性超材料的可调谐太赫兹吸波器得到了快速发展,这类吸波器通过组成材料的可调性质来实现整体结构功能的可调谐。随着研究的不断深入,相继设计和制备出许多单频带、多频带和宽频带的可调谐太赫兹超材料吸波器,但仍存在一些需要解决的问题,未来可调谐太赫兹超材料吸波器的发展趋势主要为:(1)研究便于集成的可调谐太赫兹超材料吸波器。目前对可调谐太赫兹超材料吸波器的研究主要为单一器件,与其他功能性太赫兹器件集成将成为其未来发展的重要方向;(2)研究调谐性能好的太赫兹超材料吸波器。即

在吸波性能好的前提下, 研究具有调谐范围广、调谐频率宽、调谐手段简单、调谐精度高等优势的太赫兹超材料吸波器; (3) 研究调谐方式简单易行的新型活性材料。将调谐方式简单易行的新型活性材料应用于太赫兹超材料吸波器, 将加速太赫兹超材料吸波器的实用化进程; (4) 研究先进的加工手段, 用于制备结构复杂的太赫兹超材料吸波器。目前提出的可调谐太赫兹超材料吸波器大多是基于混合材料的多层结构, 结构较为复杂, 加工难度大, 目前仍处于理论仿真阶段。因此加工制备技术的提高将成为后续研究的重点。

随着新材料的探索、可调谐特性的扩展、加工制备技术的提高, 相信可以设计并制备、应用越来越多的新型可调谐太赫兹超材料吸波器。

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