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石墨烯表面涡旋光束的局域动力学特性分析

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摘要: 结合角谱展开方法和矢量势方法, 推导了拉盖尔-高斯涡旋光束在石墨烯表面反射后的电磁场分量显式表达式。分析了光束的入射角和拓扑荷数, 以及石墨烯-衬底系统的费米能量和磁场对涡旋光束在石墨烯表面反射后局域动力学特性的影响。数值结果表明, 石墨烯表面反射涡旋光束的能量、动量、自旋/轨道角动量密度分布随着光束入射角和拓扑荷数的变化发生显著变化。同时, 改变石墨烯-衬底系统的费米能量和磁场可以有效调节反射涡旋光束的局域动力学特性。为基于涡旋光束局域动力学特性对石墨烯的表征以及基于石墨烯对涡旋光束的调控奠定了理论基础。

关键词: 涡旋光束; 石墨烯; 能量; 动量; 自旋角动量; 轨道角动量

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0 引言

近年来, 石墨烯因具有优异的光学、电学和力学特性而受到了国内外研究学者的广泛关注^[1-3]。石墨烯是由单层碳原子紧密堆积成二维蜂窝状晶格结构的一种碳质新材料, 其电导率由费米能量决定, 而电导率通过施加偏置电压或外部电场在较宽范围内进行调谐^[4]。石墨烯一个独特的性质是其反射特性由精细结构常数和本征参数决定^[5-6], 这些参数通过静电掺杂改变费米能级来进行调制^[7-9]。石墨烯的这种电光调制效应作为增强光与物质相互作用的新手段^[10], 对于理解电磁波和光在石墨烯表面的反射特性有着非常重要的作用^[11-12]。MERANO M 推导得到了石墨烯的非涅尔系数^[13], 并基于该系数研究了石墨烯表面反射高斯光束的 Goos-Hänchen (GH) 位移和 Imbert-Fedorov (IF) 位移^[14]。随后, ZHUO Linqing 等研究了石墨烯表面反射涡旋光束的 IF 位移^[15], 结果表明, 通过调节石墨烯的费米能量, 可有效控制涡旋光束的 IF 位移。

另一方面, 涡旋光束由于其独特的物理性质和新颖的物理效应及其极具潜力的应用前景也受到越来越广泛的关注, 已成为光学和光电子学领域的研究热点之一^[16]。作为一种特殊形式存在的电磁波, 具有特定振幅、相位和偏振态分布的涡旋光束不仅具有能量, 而且具有动量和角动量。角动量包括由偏振螺旋决定的自旋角动量和由相位螺旋决定的轨道角动量。能量、动量和角动量作为描述涡旋光束与物质相互作用过程中局域动力学特性的几个重要物理量, 有助于揭示物质新的物理效应和特性。国内外众多学者已对自由空间中以及聚焦情况下涡旋光束的能量、动量和角动量进行了深入研究^[17-22]。CUI Zhiwei 等研究了涡旋光束反射和折射情况下的局域动力学特性^[23]。本文对石墨烯中涡旋光束局域动力学特性进行了研究。

1 理论模型

如图 1 所示, 考虑涡旋光束从空气入射到石墨烯-衬底系统表面的反射, 设空气中的折射率为 n_0 , 石墨烯衬底的折射率为 n_1 。石墨烯-衬底分界面位于全局坐标系 (x, y, z) 中, z 轴垂直于分界面并指向石墨烯衬底, 位于衬底顶部的单层石墨烯在 $z=0$ 的位置, 沿 z 轴方向施加静磁场 B 。 (x_i, y_i, z_i) 和 (x_r, y_r, z_r) 分别表示入射

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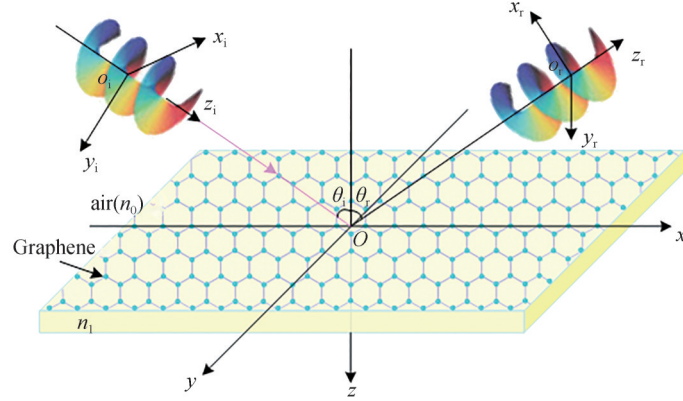


图1 涡旋光束从空气入射到石墨烯-衬底系统表面反射示意图

Fig. 1 Illustration of the reflection a vortex beam illuminating from air onto the surface of a graphene-substrate system

光束坐标系和反射光束坐标系, θ_i 和 θ_r 分别表示中心波矢量的入射角和反射角。

1.1 石墨烯界面的菲涅尔反射系数

对于如图1所示的石墨烯-衬底系统, 根据边界条件, 可得到石墨烯界面的菲涅尔反射系数为^[24]

$$\begin{cases} r_{pp} = \frac{\alpha_+^T \alpha_+^L + \beta}{\alpha_+^T \alpha_+^L + \beta} \\ r_{ss} = -\frac{\alpha_+^T \alpha_+^L + \beta}{\alpha_+^T \alpha_+^L + \beta} \\ r_{ps} = r_{sp} = -2\sqrt{\frac{\mu_0}{\epsilon_0}} \frac{k_{iz} k_{iz} \sigma_H}{\alpha_+^T \alpha_+^L + \beta} \end{cases} \quad (1)$$

式中, $\alpha_{\pm}^L = (k_{iz} \epsilon \pm k_{iz} \epsilon_0 + k_{iz} k_{iz} \sigma_L / \omega) / \mu_0$, $\alpha_{\pm}^T = k_{iz} \pm k_{iz} + \omega \mu_0 \sigma_T$, $\beta = \mu_0 k_{iz} k_{iz} \sigma_H^2 / \epsilon_0$, $k_{iz} = k_i \cos \theta_i$, $k_{iz} = k_i \cos \theta_r$, ϵ_0 和 μ_0 分别为真空中的介电常数和磁导率, ϵ 为基底系统的介电常数, σ_H , σ_L 和 σ_T 分别表示霍尔电导率、纵向电导率和横向电导率。当所施加的磁场强度足够大时, 霍尔电导率可以表示为^[24]

$$\sigma_H = 2(2n_c + 1) \operatorname{sgn}[B] \frac{e^2}{2\pi\hbar} \quad (2)$$

式中, $n_c = \operatorname{Int}[\mu_F^2 / 2\hbar e |B| v_F^2]$ 为朗道能级数, v_F 和 μ_F 分别为费米速度和费米能量。

1.2 石墨烯表面反射涡旋光束的矢量分析

众所周知, 满足傍轴近似方程的拉盖尔-高斯(Laguerre-Gaussian, LG)光束是一种典型的涡旋光束。当径向模数 $p = 0$ 时, 在坐标系 (x_i, y_i, z_i) 中, $z_i = 0$ 处拉盖尔高斯涡旋光束的标量角谱表达式为^[23]

$$\tilde{u}_i(k_{ix}, k_{iy}) = \left[\frac{\omega_0(-ik_{ix} + k_{iy})}{\sqrt{2}} \right]^l \frac{\omega_0^2}{4\pi} \exp\left[-\frac{\omega_0^2(k_{ix}^2 + k_{iy}^2)}{4} \right] \quad (3)$$

式中, l 为 LG 涡旋光束的角向模数, 也称为拓扑荷数, ω_0 为光束初始平面处的束腰半径, k_{ix} 和 k_{iy} 分别表示波矢 k_i 在 x 和 y 方向的分量, $k_i = k_0 = 2\pi/\lambda_0$ 为光束在自由空间中的波数, λ_0 为入射光束的波长。利用坐标系之间的变换, 得到反射涡旋光束在坐标系 (x_r, y_r, z_r) 中的角谱表述^[25]

$$\begin{bmatrix} \tilde{u}_r^H \\ \tilde{u}_r^V \end{bmatrix} = \begin{bmatrix} r_{pp} - \frac{k_{ry}(r_{ps} - r_{sp}) \cot \theta_i}{k_0} & r_{ps} + \frac{k_{ry}(r_{pp} + r_{ss}) \cot \theta_i}{k_0} \\ r_{sp} - \frac{k_{ry}(r_{pp} + r_{ss}) \cot \theta_i}{k_0} & r_{ss} - \frac{k_{ry}(r_{ps} - r_{sp}) \cot \theta_i}{k_0} \end{bmatrix} \begin{bmatrix} \tilde{u}_i^H \\ \tilde{u}_i^V \end{bmatrix} \quad (4)$$

式中, $\tilde{u}_i^H = \alpha \tilde{u}_i$ 和 $\tilde{u}_i^V = \beta \tilde{u}_i$ 分别为光束水平偏振分量和垂直偏振分量对应的角谱, α 和 β 为极化系数, \tilde{u}_i 为反射光束的标量角谱, 可通过对入射涡旋光束的标量角谱施加边界条件 $k_{rx} = -k_{ix}$ 和 $k_{ry} = k_{iy}$ 得到, 即

$$\tilde{u}_r = \tilde{u}_i(-k_{rx}, k_{ry}) = \left[\frac{\omega_0(i k_{rx} + k_{ry})}{\sqrt{2}} \right]^l \frac{\omega_0^2}{4\pi} \exp \left[-\frac{\omega_0^2(k_{rx}^2 + k_{ry}^2)}{4} \right] \quad (5)$$

为了在布儒斯特角附近获得较为准确的结果,将菲涅尔反射系数 r_{mn} ($m = p, s; n = p, s$) 在 $k_{rx} = 0$ 处作泰勒级数展开并取一阶近似,施加边界条件 $k_{rx} = -k_{rx}$, 得到^[26]

$$r_{mn} = r_{mn} \left[1 - \frac{k_{rx}}{k_0} \frac{\partial \ln r_{mn}}{\partial \theta_i} \right] \quad (6)$$

将式(6)代入式(4),忽略二阶项,便可以得到修正后的反射涡旋光束角谱表达式。然后,根据式(7)进行傅里叶变换

$$\begin{bmatrix} u_r^H(x_r, y_r, z_r) \\ u_r^V(x_r, y_r, z_r) \end{bmatrix} = \iint \begin{bmatrix} \tilde{u}_r^H(k_{rx}, k_{ry}) \\ \tilde{u}_r^V(k_{rx}, k_{ry}) \end{bmatrix} \exp \left[i \left(k_{rx} x_r + k_{ry} y_r - \frac{k_{rx}^2 + k_{ry}^2}{2k_r} z_r \right) \right] dk_{rx} dk_{ry} \quad (7)$$

得到

$$\begin{cases} u_r^H = A_r^H u_r \\ u_r^V = A_r^V u_r \end{cases} \quad (8)$$

其中

$$\begin{aligned} A_r^H = & \alpha r_{pp} + \beta r_{ps} - \left(\alpha r_{pp} \frac{\partial \ln r_{pp}}{\partial \theta_i} + \beta r_{ps} \frac{\partial \ln r_{ps}}{\partial \theta_i} \right) \frac{1}{k_0} \left[-\frac{l(ix_r - y_r)}{x_r^2 + y_r^2} + \frac{ik_r x_r}{z_{R,r} + iz_r} \right] + \\ & \left[\alpha(r_{sp} - r_{ps}) + \beta(r_{pp} + r_{ss}) \right] \frac{\cot \theta_i}{k_0} \left[-\frac{l(iy_r + x_r)}{x_r^2 + y_r^2} + \frac{ik_r y_r}{z_{R,r} + iz_r} \right] \end{aligned} \quad (9)$$

$$\begin{aligned} A_r^V = & \alpha r_{sp} + \beta r_{ss} - \left(\alpha r_{sp} \frac{\partial \ln r_{sp}}{\partial \theta_i} + \beta r_{ss} \frac{\partial \ln r_{ss}}{\partial \theta_i} \right) \frac{1}{k_0} \left[-\frac{l(ix_r - y_r)}{x_r^2 + y_r^2} + \frac{ik_r x_r}{z_{R,r} + iz_r} \right] - \\ & \left[\alpha(r_{pp} + r_{ss}) + \beta(r_{ps} - r_{sp}) \right] \frac{\cot \theta_i}{k_0} \left[-\frac{l(iy_r + x_r)}{x_r^2 + y_r^2} + \frac{ik_r y_r}{z_{R,r} + iz_r} \right] \end{aligned} \quad (10)$$

$$u_r = \left[\frac{\sqrt{2}}{\omega_0} \left(\frac{-x_r + iy_r}{1 + iz_r/z_{R,r}} \right) \right]^l \frac{1}{1 + iz_r/z_{R,r}} \exp \left[-\frac{(x_r^2 + y_r^2)/\omega_0^2}{1 + iz_r/z_{R,r}} \right] \quad (11)$$

式中, $k_r = k_0$ 为反射光束在自由空间中的波数, $z_{R,r} = k_r \omega_0^2 / 2$ 为反射光束的瑞利距离。

在傍轴近似条件下,采用基于洛伦兹规范的矢量势方法,反射涡旋光束的电场和磁场可写为^[27]

$$E_r = ik_r Z_r \left[u_r^H \hat{x}_r + u_r^V \hat{y}_r + \frac{i}{k_r} \left(\frac{\partial u_r^H}{\partial x_r} + \frac{\partial u_r^V}{\partial y_r} \right) \hat{z}_r \right] \exp(ik_r z_r) \quad (12)$$

$$H_r = ik_r \left[-u_r^V \hat{x}_r + u_r^H \hat{y}_r - \frac{i}{k_r} \left(\frac{\partial u_r^V}{\partial x_r} - \frac{\partial u_r^H}{\partial y_r} \right) \hat{z}_r \right] \exp(ik_r z_r) \quad (13)$$

式中, $Z_r = \sqrt{\mu_0/\epsilon_0}$ 。将 u_r^H 和 u_r^V 分别对 x_r 和 y_r 求导,得到

$$\begin{cases} \frac{\partial u_r^H}{\partial x_r} = \left[\frac{\partial A_r^H}{\partial x_r} \right] u_r + A_r^H \left[\frac{\partial u_r}{\partial x_r} \right] \\ \frac{\partial u_r^H}{\partial y_r} = \left[\frac{\partial A_r^H}{\partial y_r} \right] u_r + A_r^H \left[\frac{\partial u_r}{\partial y_r} \right] \end{cases} \quad (14)$$

$$\begin{cases} \frac{\partial u_r^V}{\partial x_r} = \left[\frac{\partial A_r^V}{\partial x_r} \right] u_r + A_r^V \left[\frac{\partial u_r}{\partial x_r} \right] \\ \frac{\partial u_r^V}{\partial y_r} = \left[\frac{\partial A_r^V}{\partial y_r} \right] u_r + A_r^V \left[\frac{\partial u_r}{\partial y_r} \right] \end{cases} \quad (15)$$

式中,

$$\frac{\partial A_r^H}{\partial x_r} = -\left(\alpha r_{pp} \frac{\partial \ln r_{pp}}{\partial \theta_i} + \beta r_{ps} \frac{\partial \ln r_{ps}}{\partial \theta_i}\right) \frac{1}{k_0} \left[\frac{il}{(x_r - iy_r)^2} + \frac{ik_r}{z_{R,r} + iz_r} \right] + [\alpha(r_{sp} - r_{ps}) + \beta(r_{pp} + r_{ss})] \frac{\cot \theta_i}{k_0} \left[-\frac{l}{(y_r + ix_r)^2} \right] \quad (16)$$

$$\frac{\partial A_r^H}{\partial y_r} = -\left(\alpha r_{pp} \frac{\partial \ln r_{pp}}{\partial \theta_i} + \beta r_{ps} \frac{\partial \ln r_{ps}}{\partial \theta_i}\right) \frac{1}{k_0} \left[\frac{l}{(x_r - iy_r)^2} \right] + [\alpha(r_{sp} - r_{ps}) + \beta(r_{pp} + r_{ss})] \frac{\cot \theta_i}{k_0} \left[\frac{il}{(y_r + ix_r)^2} + \frac{ik_r}{z_{R,r} + iz_r} \right] \quad (17)$$

$$\frac{\partial A_r^V}{\partial x_r} = -\left(\alpha r_{sp} \frac{\partial \ln r_{sp}}{\partial \theta_i} + \beta r_{ss} \frac{\partial \ln r_{ss}}{\partial \theta_i}\right) \frac{1}{k_0} \left[\frac{il}{(x_r - iy_r)^2} + \frac{ik_r}{z_{R,r} + iz_r} \right] - [\alpha(r_{pp} + r_{ss}) + \beta(r_{ps} - r_{sp})] \frac{\cot \theta_i}{k_0} \left[-\frac{l}{(y_r + ix_r)^2} \right] \quad (18)$$

$$\frac{\partial A_r^V}{\partial y_r} = -\left(\alpha r_{sp} \frac{\partial \ln r_{sp}}{\partial \theta_i} + \beta r_{ss} \frac{\partial \ln r_{ss}}{\partial \theta_i}\right) \frac{1}{k_0} \left[\frac{l}{(x_r - iy_r)^2} \right] - [\alpha(r_{pp} + r_{ss}) + \beta(r_{ps} - r_{sp})] \frac{\cot \theta_i}{k_0} \left[\frac{il}{(y_r + ix_r)^2} + \frac{ik_r}{z_{R,r} + iz_r} \right] \quad (19)$$

$$\frac{\partial u_r}{\partial x_r} = \left[\frac{l(x_r + iy_r)}{x_r^2 + y_r^2} - \frac{k_r x_r}{z_{R,r} + iz_r} \right] u_r \quad (20)$$

$$\frac{\partial u_r}{\partial y_r} = \left[\frac{l(y_r - ix_r)}{x_r^2 + y_r^2} - \frac{k_r y_r}{z_{R,r} + iz_r} \right] u_r \quad (21)$$

1.3 结构光场动力学参量的描述

能量、动量、自旋角动量(Spin Angular Momentum, SAM)和轨道角动量(Orbital Angular Momentum, OAM)作为结构光场几个重要的动力学参量,有助于揭示结构光场和物质新的物理效应和特性。但是对于结构光场动力学参量的描述,基于经典力学和电磁理论建立的机械动力学理论存在着一定的局限性。采用经典的机械动量描述结构光场的动力学特性时缺乏清晰的物理意义,无法对自旋角动量和轨道角动量进行独立描述,不能解释结构光场与物质相互作用时局部动量的传递和光对物质施加的辐射压力^[28]。理论研究表明,在量子力学和相对论场论范畴内,采用正则方法建立的光场动力学理论可以很好的解决上述问题。对于均匀各向同性媒质中的结构光场,电磁场对偶形式的能量、正则动量、自旋角动量和轨道角动量密度的定义分别为^[28]

$$W = \frac{1}{4} (\epsilon |E|^2 + \mu |H|^2) \quad (22)$$

$$P = \frac{1}{4\omega} \text{Im} [\epsilon E^* \cdot (\nabla) E + \mu H^* \cdot (\nabla) H] \quad (23)$$

$$S = \frac{1}{4\omega} \text{Im} [\epsilon E^* \times E + \mu H^* \times H] \quad (24)$$

$$L = r \times P \quad (25)$$

式中, E 和 H 为光场的电场和磁场, ω 表示光束的角频率, ϵ 和 μ 分别为光场所在空间中介质的介电常数和磁导率, $\text{Im}[\cdot]$ 表示虚部,上标“*”代表复共轭,符号 $A \cdot (\nabla) B$ 定义为 $A \cdot (\nabla) B = A_x \nabla B_x + A_y \nabla B_y + A_z \nabla B_z$ 。上述定义的正则动量和角动量具有清晰的物理解释,即动量密度与场相位的局部梯度成正比;自旋角动量密度是光场的内禀属性,与光场的偏振态有关;轨道角动量与光场的传输路径和空间相位结构有关。

2 结果分析

将式(12)和(13)代入式(22)~(25),编写程序进行数值模拟,分析石墨烯表面涡旋光束的局域动力学特性。本文着重分析光束的入射角和拓扑荷数,以及石墨烯-衬底系统的费米能量和磁场对涡旋光束在石墨烯表面反射后局域动力学特性的影响。若无特殊说明,计算参数取值为:涡旋光束的波长 $\lambda_0 = 632.8 \text{ nm}$,拓扑荷数 $l = 2$,束腰半径 $w_0 = 1.0\lambda_0$,极化参数 $(\alpha, \beta) = (1, i)/\sqrt{2}$,入射角 $\theta_i = 45^\circ$;石墨烯衬底的折射率 $n_1 = 1.517$,费米能量 $\mu_F = 0.25 \text{ eV}$,费米速度 $v_F = 1 \times 10^6 \text{ m/s}$,电子电量 $e = 1.6 \times 10^{-19} \text{ C}$,磁场强度 $B = 6 \text{ T}$;观察平面所在位置 $z_r = \lambda_0$,观察点坐标为 $x_r = y_r = \lambda_0$ 。

图2是入射角对涡旋光束在石墨烯表面反射后能量、动量、自旋角动量和轨道角动量密度的影响分布,其中 $\theta_i = 59.1^\circ$ 为布儒斯特角。从图中可以看出,随着入射角的增大,能量密度和动量密度呈现出相似的变化规律。能量、动量、自旋角动量和轨道角动量密度分布在布儒斯特角附近均发生了突变。当入射角小于布儒斯特角时,能量密度和动量密度呈现出环形的非均匀分布,而当入射角大于布儒斯特角时,能量密度和动量密度逐渐呈现出月牙形的轮廓。相较于能量、动量和轨道角动量密度,自旋角动量密度呈现出完全不同的轮廓,且入射角的改变对自旋角动量密度的影响较为显著。当入射角增加到 $\theta_i = 75^\circ$ 时,自旋角动量呈现出与其它动力学特性量类似的月牙型分布。当入射角小于布儒斯特角时,轨道角动量密度呈现出环形分布,峰值强度的位置随着入射角的改变呈现出较大变化。

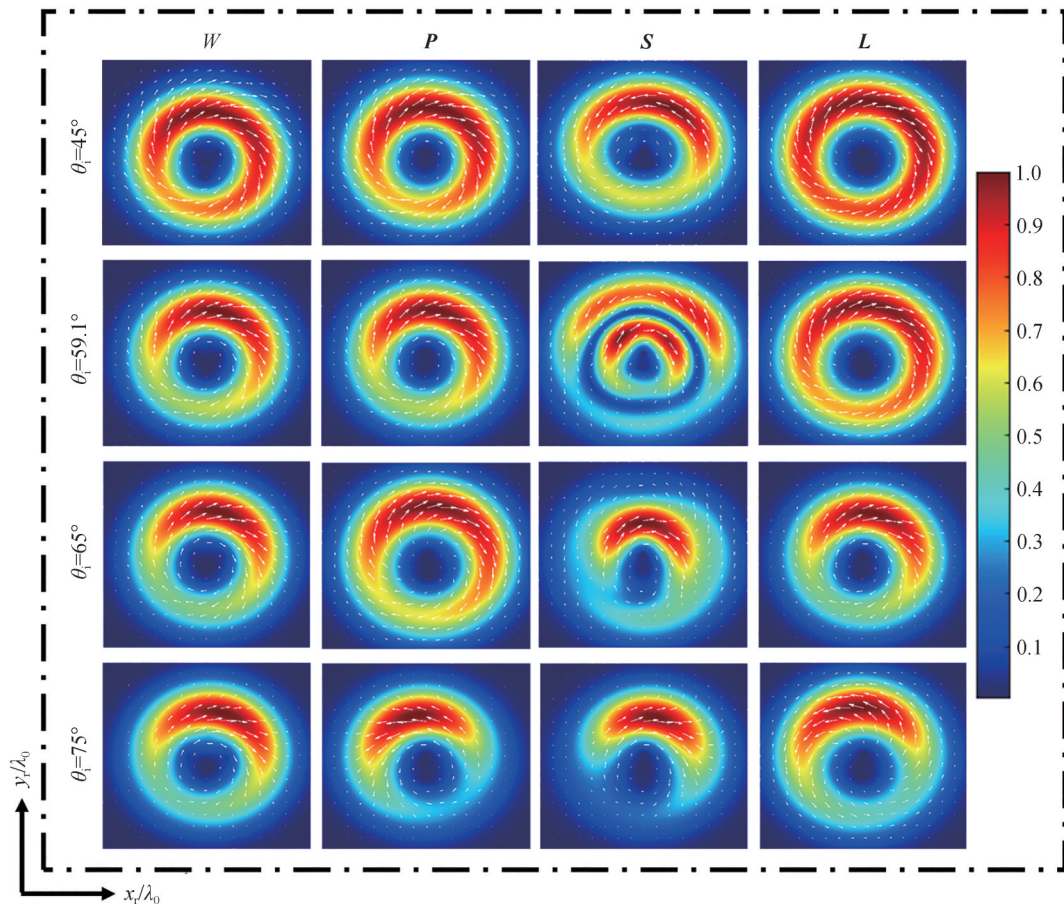


图2 入射角对涡旋光束在石墨烯表面反射后能量、动量、自旋角动量和轨道角动量密度的影响

Fig. 2 Effect of the incident angle on the energy, momentum, SAM and OAM densities of the vortex beams reflected from a graphene-substrate interface

图3是拓扑荷数对涡旋光束在石墨烯表面反射后能量、动量、自旋角动量和轨道角动量密度的影响分布图。从图中可以看出,当拓扑荷数 l 增大时,能量密度和动量密度中心环的半径增大,即逐渐向外扩展,且峰值的位置发生较大改变。随着拓扑荷数 l 的增大,自旋角动量密度的分布由环形分布转变为两瓣的月牙形分布,轨道角动量密度的圆环半径逐渐增大,且峰值位置发生较大改变。进一步观察可以发现,能量密度和动量密度的方向均呈现出顺时针方向的旋转,不同拓扑荷数 l 下的自旋角动量密度与轨道角动量密度的旋转方向总是相反的。

图4给出的是费米能量对涡旋光束在石墨烯表面反射后能量、动量、自旋角动量和轨道角动量密度的影响分布图。从图中可以看出,当入射角 $\theta_i < 50^\circ$ 时,费米能量对反射光束的能量密度影响较小,当入射角 $\theta_i > 50^\circ$ 时,反射光束的能量密度呈现先增大后减小的趋势。动量密度和轨道角动量密度变化趋势相似,均随着入射角的增大而增强,从 $\theta_i = 60^\circ$ 开始迅速增大,且当 $\theta_i < 70^\circ$ 时,费米能量越小,动量密度和轨道角动量密度越小;当 $\theta_i > 70^\circ$ 时,费米能量越小,动量密度和轨道角动量密度越大。自旋角动量密度呈现先减小

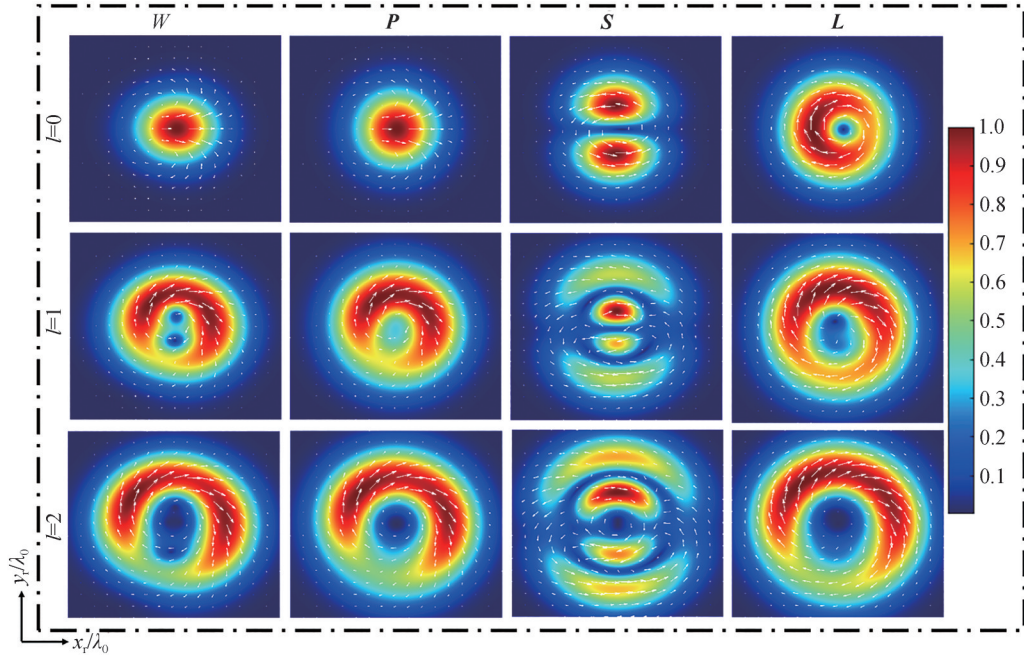


图3 拓扑荷数对涡旋光束在石墨烯表面反射后能量、动量、自旋角动量和轨道角动量密度的影响
Fig. 3 Effect of the topological charge on the energy, momentum, SAM and OAM densities of the vortex beams reflected from a graphene-substrate interface

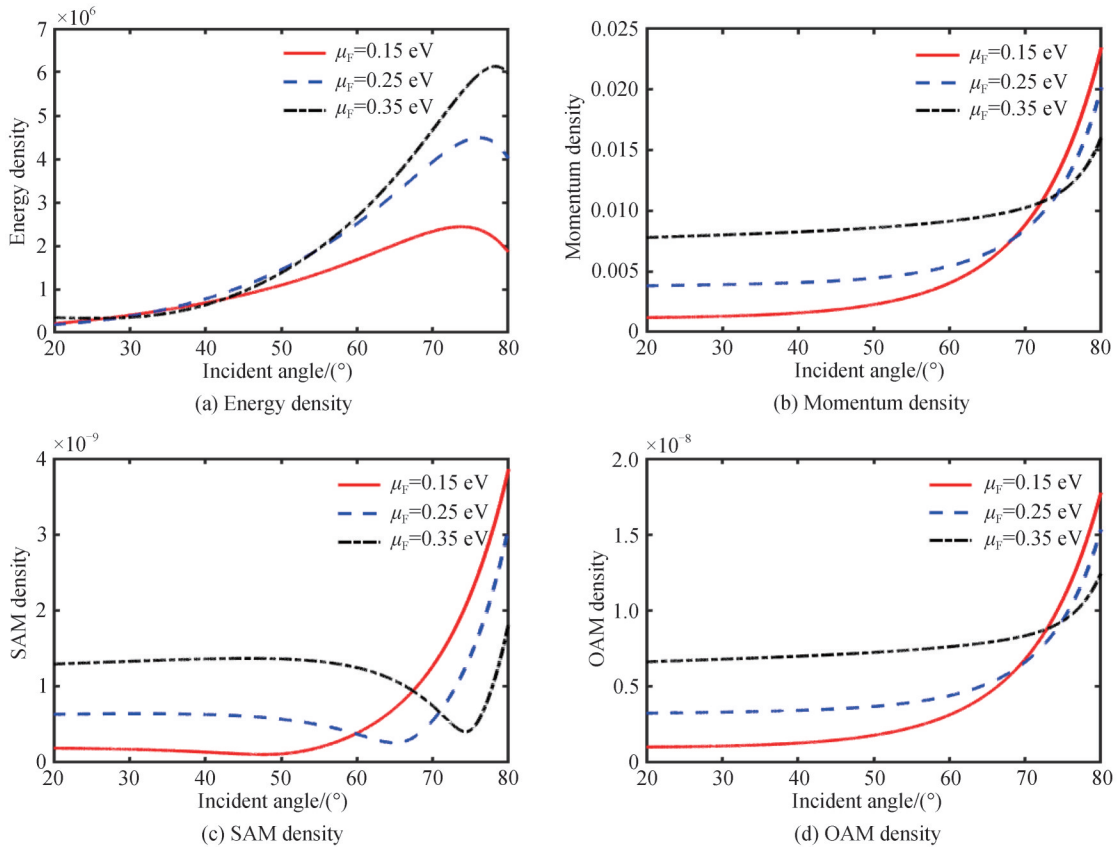


图4 费米能量对涡旋光束在石墨烯表面反射后能量、动量、自旋角动量和轨道角动量密度的影响
Fig. 4 Effect of the Fermi energy on the energy, momentum, SAM and OAM densities of the vortex beams reflected from a graphene-substrate interface

后增大的趋势,谷值随着费米能量的增大而增大,且费米能量越大,达到谷值的所对应的入射角也越大。达到谷值前,费米能量越小,自旋角动量密度越小,达到谷值后,费米能量越小,自旋角动量密度越大。

图5是磁场对涡旋光束在石墨烯表面反射后能量、动量、自旋角动量和轨道角动量密度的影响分布图。从图中可以看出,当入射角 $\theta_i < 50^\circ$ 时,磁场强度对反射光束的能量密度影响较小,当入射角 $\theta_i > 50^\circ$ 时,反射光束的能量密度呈现先增大后减小的趋势,且磁场强度越小,峰值越大。动量密度和轨道角动量密度呈现相似的变化趋势,均随着入射角的增大而增强,且从 $\theta_i = 60^\circ$ 开始迅速增大,当 $\theta_i > 75^\circ$ 后,磁场强度对反射光束的动量密度和轨道角动量密度影响较小。自旋角动量密度呈现先减小后增大的趋势,谷值随着磁场强度的增强而减小,且磁场强度越强,达到谷值的所对应的入射角越小。达到谷值前,磁场强度越小,自旋角动量密度越大,达到谷值后,磁场强度越大,自旋角动量密度越大。

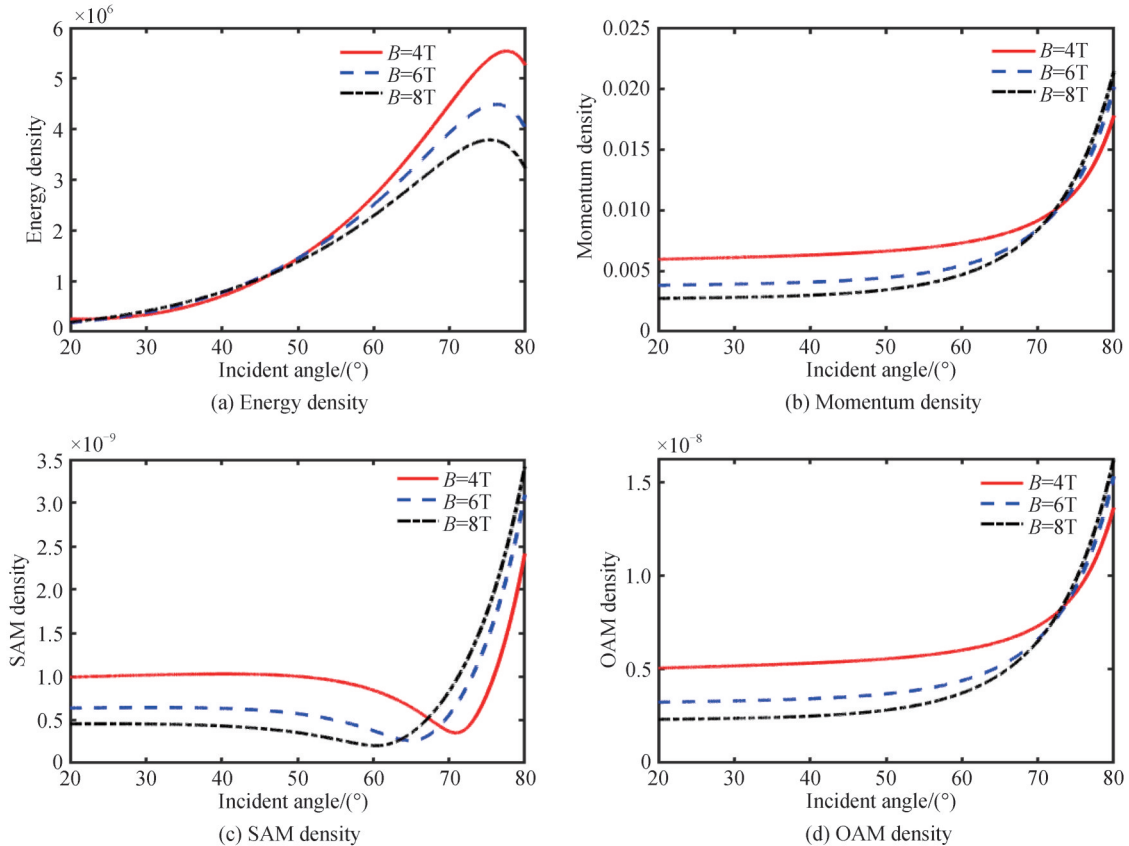


图5 磁场对涡旋光束在石墨烯表面反射后能量、动量、自旋角动量和轨道角动量密度的影响

Fig. 5 Effect of the magnetic field on the energy, momentum, SAM and OAM densities of the vortex beams reflected from a graphene-substrate interface

3 结论

理论分析和数值模拟研究了石墨烯表面涡旋光束的局域动力学特性。建立了LG涡旋光束从空气入射到石墨烯-衬底系统表面反射的全矢量理论模型,推导出了LG涡旋光束在石墨烯表面反射后电场和磁场分量的解析表达式。通过数值模拟,分析了光束参数和石墨烯材料参数对反射涡旋光束局域动力学特性的影响。数值结果表明,石墨烯表面反射涡旋光束的能量、动量、自旋/轨道角动量密度分布在布儒斯特角附近发生突变。光束拓扑荷数的增大使能量、动量和自旋/轨道角动量密度的分布向外扩展,峰值位置发生较大改变。当入射角较小时,费米能量和磁场对反射涡旋光束的能量密度影响较小;当入射角度较大时,费米能量越大或磁场越小,能量密度越大。动量和轨道角动量密度随费米能量和磁场的变化呈现相似的变化趋势,当 $\theta_i < 70^\circ$ 时,费米能量越小或磁场越大,动量和轨道角动量密度越小。自旋角动量密度随费米能量和磁场的变化随着入射角的增大呈现先减小后增大的趋势,费米能量越大或磁场越小,达到谷值的所对应的入射角越大。本文建立的理论模型和推导得到的电磁场分量表达式可用于计算石墨烯表面涡旋光束的螺旋度和手性,研究基于石墨烯对涡旋光束螺旋度和局域手性的调控,为新型光电子器件的设计等技术提供理论基础与技术支撑。

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Local Dynamical Characteristics of Vortex Beams on the Graphene Surface

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Abstract: Graphene, a one-atom-thick layer of carbon atoms arranged in a hexagonal honeycomb lattice,

has attracted intensive attention and extensive investigation because of its striking electronic and optical properties. Especially, the reflection coefficients of graphene are determined by the fine structure constant and intrinsic parameters, which can be tuned by altering the Fermi level. Such interesting feature makes graphene a good candidate for tuning the optical properties of structured light. On the other hand, structured light beams with vortex phase have become a research hotspot in optics and optoelectronics due to their unique physical properties and novel physical effects, as well as various promising potential applications. It is well known that the complex amplitude of a vortex beam comprises a phase $\exp(i\ell\varphi)$, where ℓ is an integer often called the topological charge and φ is the azimuthal angle. A common example of the vortex beams is the Laguerre–Gaussian (LG) beams. As a special type of electromagnetic wave, the LG vortex beams can carry energy, momentum, and angular momentum, which can be classified into Spin Angular Momentum (SAM) and Orbital Angular Momentum (OAM). As well known, energy, momentum, SAM, and OAM are the main dynamical characteristics of light and play a crucial role in understanding the light–matter interactions. There has been a recent study on the dynamical characteristics of vortex beams reflected from an air–glass interface. However, to the best of our knowledge, the local dynamical characteristics of vortex beams reflected from a graphene–substrate interface have not been reported. Compared to the conventional air–glass interface, graphene–substrate interface may reveal many other important and interesting features of the vortex beams upon reflection. Meanwhile, the dynamical characteristics of reflected vortex beams are of great importance in understanding the optical properties of graphene. In this work, we investigate the dynamical characteristics of the vortex beams impinging on graphene–substrate surfaces. Firstly, the Fresnel reflection coefficients of the graphene–substrate system in the presence of an imposed magnetic field are briefly given. The proposed expressions of the Fresnel reflection coefficients are characterized by the parameters of refraction angle, permittivity of the substrate, permittivity and permeability in vacuum, and the longitudinal, transverse and Hall conductivities. Among these parameters, the Hall conductivity, a very important parameter of the graphene–substrate system, is quantized in multiples of the fine structure constant and is described by the number of occupied Landau levels, the imposed magnetic field, the Fermi energy and the Fermi velocity. Then, a theoretical model that takes into full account the vectorial nature of electromagnetic fields is established to describe the LG vortex beams reflected from a graphene–substrate interface. In this model, starting from the expression of the vortex beam on the initial plane in the source plane and utilizing the Fourier transform, the angular spectrum amplitude of the LG vortex beam is obtained. The angular spectrums of the reflected beam are related to angular spectrums of the incident beam by means of a matrix considering boundary conditions and Taylor series expansion. Utilizing the angular spectrum representation, the horizontal and vertical components of the reflected LG vortex beam are derived. Further, introducing vector potential and using a Lorenz gauge, the explicit analytical expressions for the electric and magnetic field vectors of the reflected LG vortex beam are obtained. Based on the derived formulas, the energy, momentum, SAM, and OAM of the LG vortex beams reflected from a graphene–substrate interface are examined. The effects of the incidence angle, topological charge, Fermi energy, and magnetic field on these dynamical quantities are analyzed. The results show that the energy, momentum, SAM, and OAM density distributions change abruptly near the Brewster angle. With the increasing of topological charge, the distributions of these dynamical quantities in the transverse plane gradually go away from the center and the peak position changes greatly. When the incident angle is small, the Fermi energy and magnetic field have little effect on the energy density of the reflected vortex beam. When the incident angle is greater than a certain angle, which is 50° for the case considered, the greater the Fermi energy or the smaller the magnetic field, the greater the energy density. The momentum and OAM density distributions show a similar trend with the change of Fermi energy and magnetic field. When $\theta_i < 70^\circ$, the smaller the Fermi energy or the larger the magnetic field, the smaller the momentum and OAM densities. As the incident angle increases, the SAM density first decreases gradually, reaches its minimum value, and then increases rapidly. The larger the Fermi energy or the smaller the magnetic field, the larger the incident angle corresponding to the minimum value of the SAM density. These findings lay a foundation for the characterization of graphene based on the local dynamical characteristics of vortex beams, and are of great significance for promoting the theoretical and applied research on the tunable optical properties of vortex beam with graphene.

Key words: Vortex beams; Graphene; Energy; Momentum; Spin angular momentum; Orbital angular momentum

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