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GBaII探测地球上空 90~100 km 气辉 MTF 研究

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摘要:分别利用 He-Ne 激光 632.8 nm、O₂(0-1) 867.7 nm 和 O(¹S) 557.7 nm 谱线作为光源,研究了地基气辉成像干涉仪的光学传递函数,给出了优化设计、理论计算和实际拍摄图片的 MTF 值。优化设计 MTF 的所有值均在 0.3 以上,部分视场 MTF 高于 0.6;对 557.7 nm 和 867.7 nm 波长的气辉,理论计算的 MTF 分别为 0.508 和 0.510;由室内外实验拍摄获取的 GBaII 成像干涉图得出的 MTF 值分别大于 0.84、0.58、0.24,与国际著名的星载风成像干涉仪 WINDII 的 0.35 MTF 值相当。

关键词:地基气辉成像干涉仪;光学传递函数;干涉成像;气辉;光学仪器

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0 引言

地球上空高层大气(80~300 km)区域的微弱气辉、大气重力波、大气潮汐、夜光云、电离层闪电等现象大多出现在 80~120 km 的中间层和低热层(Mesosphere and Lower Thermosphere, MLT)区域,MLT 区域是一个辐射、动力学和化学过程相互耦合的复杂区域。高空大气波的振幅在这里达到峰值,产生非线性相互作用和耗散,极大影响全球范围内大气的动量、能量、成分的分布和流动。MLT 区域 100 km 附近电离层的等离子体电子分布出现峰值突变,这对通讯和广播造成严重影响,甚至讯号中断。MLT 区域的金属离子层分布也严重影响卫星、飞行器的通讯信号。为了更多更好地了解诸如此类的自然现象,人们通常使用星载、机载、地基等主动和被动探测方式来获取大气的风速、温度、浓度等物理信息,这些观测方式中成本相对较低的是地基被动遥感探测方式^[1-5]。国际上,地基的光谱气辉温度成像器(Spectral Airglow Temperature Imager, SATI)^[6-7]和高分辨率多普勒成像仪(High Resolution Doppler Imager, HRDI)^[8]均根据多原子分子振转谱线的强度差异,利用法布里珀罗干涉(Fabry - Péro interferometer, FPI)滤光片的“转动谱线测温法”获取高层大气的温度,而星载的风成像干涉仪(Wind Imaging Interferometer, WINDII)^[9]利用广角迈克尔逊干涉仪(Michelson Interferometer, MI)的“四强度法”探测高层大气温度和风速。中科院空间中心搭建了我国第一台 FPI 在国家天文台兴隆站进行观测^[10],西安交通大学利用广角 MI 对火星风场进行研究^[11]。本课题组研制了一台揉合“转动谱线测温法”和“四强度法”原理于一体的地基气辉成像干涉仪(Ground-Based Airglow Imager Interferometer, GBaII)样机,成功探测了地球上空 90~100 km 的大气风速、温度^[12-16]和体发射率^[17]。GBaII 使用地球上空 98 km 处的 O(¹S) 557.7 nm 单线气辉和 94 km 处的 O₂(0-1)带 867.7 nm 附近的 12 条间距很小的谱线作为探测光源,将具备空间光谱扫描能力的窄带 FPI 的“转动谱线测温法”与具备视场展宽能力的广角 MI“四强度测温法”相结合,从长时间曝光的气辉成像干涉图中获取地球上空 90~100 km 的大气风速、温度、体发射率等信息。

判断成像系统的像质优劣可用瑞利判据、中心点亮度、分辨率、点列图和光学传递函数(Modulation Transfer Function, MTF)等方式,而 MTF 是判断像质优劣的定量指标^[18-20]。MTF 是成像系统所成的像对

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被摄原物的还原比例,其值在0~1之间。因为GBAII是针对强度很弱的气辉既要成像还要发生干涉,其MTF就成为GBAII设计、研制和测试过程中一个非常重要的指标,本文针对GBAII的MTF开展研究。

1 GBAII优化设计的MTF

1.1 GBAII光学系统

GBAII的光学成像结构如图1所示,它由锥形镜收光系统、广角MI的相位调制系统、窄带干涉滤光片、CCD和3个透镜等5部分组成。图1顶部的锥形镜能保证光线的高通量,光线经锥形镜侧面反射,以一定角度入射到透镜1,再经MI、透镜2、透镜3后,出射的准直光束以一定离轴角进入干涉滤光片,通过干涉滤光片的光线由离轴角决定其空间光谱的分离,从CCD所拍摄气辉的成像干涉图来获取大气的温度和风速。实际光路中根据透镜焦距需要,GBAII分别用了3个透镜组合来等效图1所示的3个透镜,如图2所示,其中图2最右侧是激光光源,可以替换不同波长,用于室内定标等实验。GBAII的视场角为 $\pm 6^\circ$,通过超广角、消色散、热补偿等条件优化出来的广角MI的基准光程差7.495 cm,所用CCD像素为 512×512 ,单像素大小 $20 \mu\text{m}$,GBAII选用峰值波长为557.7 nm、867.7 nm和630.0 nm窄带滤光片。

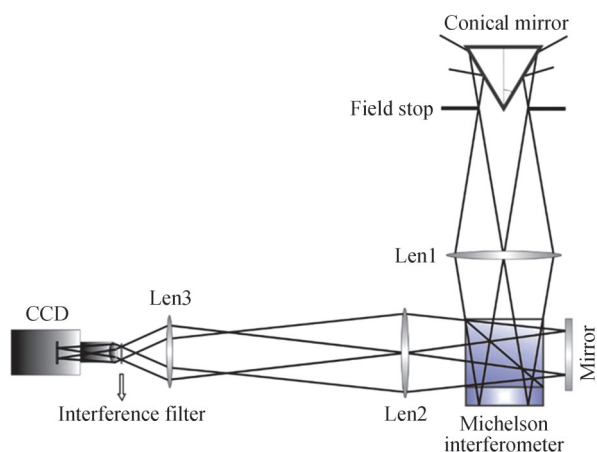


图1 GBAII光学系统示意图

Fig. 1 GBAII's simulate optical system

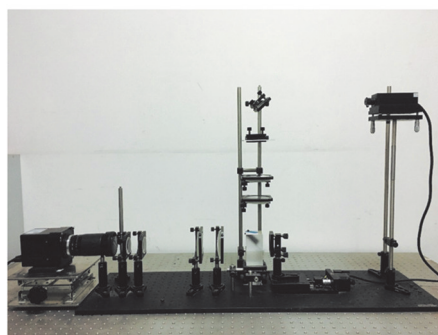


图2 GBAII光学系统实物图

Fig. 2 GBAII's optical components

1.2 GBAII优化设计的MTF

通过Code-V软件对图1所示的GBAII进行优化设计,得出GBAII的点列图如图3所示,采用 4×4 作为一个bin, 0° 视场时弥散斑直径约为 $60 \mu\text{m}$,在 $2^\circ \sim 9.5^\circ$ 视场内,弥散斑控制在 $80 \sim 90 \mu\text{m}$ 之间,极限分辨率为 6.25 lp/mm 。由于GBAII所用CCD的成像单元尺寸为 $20 \mu\text{m}$,4个bin则为 $80 \mu\text{m}$,这个弥散斑没有超过CCD的探测范围;点列图结果显示在0.4和0.7视场时弥散斑略有减小到 $40 \mu\text{m}$ 左右,说明还有一定的慧差,全视场时大约 $100 \mu\text{m}$,且有一定像散。

利用Code-V设计GBAII整个光学系统的MTF结果如图4所示,对波长为557.7 nm、630.0 nm和867.7 nm等3条气辉谱线,其MTF的所有值均在0.3以上,部分视场MTF高于0.6,但也看出全视场中的MTF子午分支和弧矢分支差别较大,主要由像散造成。如果采用 2×2 作为一个bin则极限分辨率为 12.5 lp/mm ,GBAII的MTF所有值均在0.3以上,部分视场在0.6以上。从这些MTF的设计结果可见GBAII满足较高的成像要求。

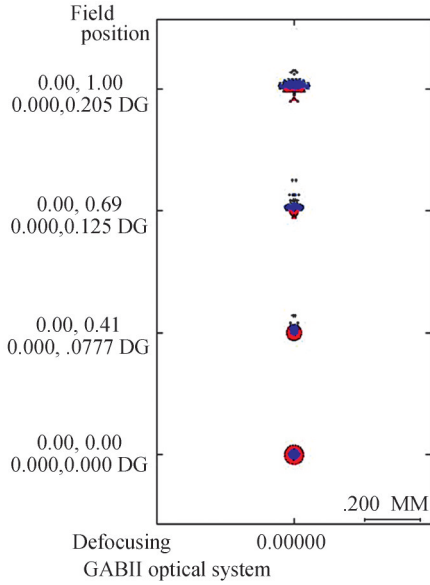


图3 GBAII的点列图
Fig. 3 Spot diagram of GBAII

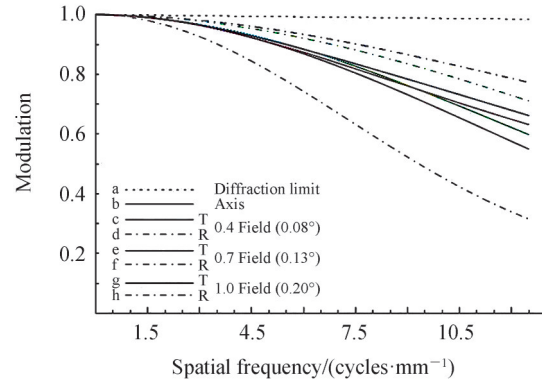


图4 GBAII整个光学系统的MTF
Fig. 4 MTF diagram of GBAII

1.3 理论计算GBAII的MTF

根据傅里叶光学中线性光学系统调制传递函数的性质,GBAII的MTF的理论计算是图1所示的光学元件透镜1、MI、透镜2、透镜3、滤光片和CCD等6个部分的MTF之积。

$$MTF(f) = MTF_{\text{len1}}(f) \cdot MTF_{\text{Michelson}}(f) \cdot MTF_{\text{len2}}(f) \cdot MTF_{\text{len3}}(f) \cdot MTF_{\text{filter}}(f) \cdot MTF_{\text{CCD}}(f) \quad (1)$$

以下分别计算式(1)中各部分的MTF值。对于透镜而言,虽然它的MTF与其孔径大小有关,孔径越大,透镜的MTF值就越大,透镜孔径的MTF因素与孔径的衍射效应有关,又与透镜的像差有关。一般说来,透镜的MTF值由商家给出,通常情况下为一个常数,取其为1。又由于该透镜的孔径与通光孔径大小相当,所以式(1)中将GBAII的3个透镜组的 MTF_{len} 均取值为1。

1.3.1 广角迈克尔逊干涉仪的MTF

GBAII的关键仪器之一是广角迈克尔逊干涉仪MI,GBAII采用中国K9玻璃且用大空气隙结构的MI。为了计算MI的MTF,需要把MI简化为正方形光瞳。根据边界条件,把GBAII入射光的 x 和 y 维度限定在 $-a \leq x \leq a, -a \leq y \leq a$ 范围,设MI的入瞳函数为二维矩形函数

$$g(x, y) = \text{rect}\left(\frac{x}{2a}, \frac{y}{2a}\right) = \begin{cases} 1 & (-a \leq x \leq a, -a \leq y \leq a) \\ 0 & (\text{other}) \end{cases} \quad (2)$$

根据衍射受限系统,成像的点扩散函数仅决定于系统的光瞳函数 $g(x, y)$,且为光瞳函数的傅里叶变换;在相干照明下点扩散函数再进行一次傅里叶变换即为MTF。因为光瞳内MTF有值,光瞳外MTF为0,况且式(2)的二维矩形函数是对称的,所以只考虑一维情况下MI的归一化传递函数为

$$MTF_{\text{Michelson}}(f_x) = \text{rect}\left(\frac{\lambda d_{i1} f_x}{2a}\right) = \begin{cases} 1 & (0 \leq \lambda d_{i1} f_x \leq 2a) \\ 0 & (\text{other}) \end{cases} \quad (3)$$

式中, λ 是入射光的波长, d_{i1} 是与图1中透镜组2的截止频率对应的焦距, f_x 是空间频率。

1.3.2 干涉滤光片的MTF

设GBAII所用圆形干涉滤光片的底面中心为坐标原点,在横截面上取互相垂直的 x, y 方向,设滤光片厚度为1,当入射光沿主光轴方向到达滤光片时,则出射光瞳直径为 $2b$ 的圆形光瞳函数为

$$p(x, y) = \text{circ}\left(\frac{\sqrt{x^2 + y^2}}{b}\right) \quad (4)$$

对式(4)进行傅里叶变换并归一化,得到滤光片的传递函数

$$\text{MTF}_{\text{circ}} = \left| \text{FT} \{ p(x, y) \} \right| = \left| \frac{J_1(2\pi b \lambda d_{i2} \sqrt{f_x^2 + f_y^2})}{b \lambda d_{i2} \sqrt{f_x^2 + f_y^2}} \right| = \left| \frac{J_1(2\pi b \lambda d_{i2} \rho)}{b \lambda d_{i2} \rho} \right| \quad (5)$$

式中, $\rho = \sqrt{f_x^2 + f_y^2}$, d_{i2} 是与图1中透镜组3的截止频率对应的焦距, J_1 是一阶贝塞尔函数。鉴于滤光片的光瞳函数具有圆域对称性,所以式(5)也只考虑一个方向的空间频率,于是干涉滤光片的一维归一化的传递函数为

$$\text{MTF}_{\text{filter}} = \left| \frac{J_1(2\pi b \lambda d_{i2} f_x)}{b \lambda d_{i2} f_x} \right| \quad (6)$$

1.3.3 CCD的MTF

CCD采样包含像元积分和离散抽样两过程,其MTF是这两部分之积。假设光敏面CCD的单个像素元尺寸为 $w \times w$,则单个像元脉冲响应函数可表示为

$$l(x, y) = \text{rect}\left(\frac{x}{w}, \frac{y}{w}\right) \quad (7)$$

将式(7)进行傅里叶变换并归一化,得到CCD单个像素元的传递函数

$$\text{MTF}_{\text{ccd}} = \left| \text{FT} \{ l(x, y) \} \right| = \left| \text{sinc}(w f_x, w f_y) \right| \quad (8)$$

鉴于CCD成像时还需在CCD像面上抽样采样,假设 x, y 方向的采样间距均为 l ,采样函数为

$$\text{Samp}(x, y) = \text{rect}\left(\frac{x}{l}, \frac{y}{l}\right) \quad (9)$$

将式(9)进行傅里叶变换并归一化,得到采样的传递函数

$$\text{MTF}_{\text{samp}} = \text{FT} \{ \text{Samp}(x, y) \} = \left| \text{sinc}(l f_x, l f_y) \right| \quad (10)$$

因此,CCD的 MTF_{CCD} 是CCD单像素元的 MTF_{ccd} 与采样 MTF_{samp} 之积

$$\text{MTF}_{\text{CCD}} = \text{MTF}_{\text{ccd}} \cdot \text{MTF}_{\text{samp}} = \left| \text{sinc}(w f_x, w f_y) \right| \cdot \left| \text{sinc}(l f_x, l f_y) \right| \quad (11)$$

1.3.4 GBAlI的计算MTF

综合式(1)、(3)、(5)和(11),由于MI矩形、FPI圆形函数都具对称性,空间频率 $f_x = f_y = f$,将二维MTF简化为一维来计算,则GBAlI的MTF表达式为

$$\text{MTF}(f) = \text{rect}\left(\frac{\lambda d_{i1} f}{2a}\right) \cdot \left| \frac{J_1(2\pi b \lambda d_{i2} f)}{b \lambda d_{i2} f} \right| \cdot \left| \text{sinc}(w f) \right| \cdot \left| \text{sinc}(l f) \right| \quad (12)$$

根据超广角、消色散、热补偿条件优化出来的广角GBAlI的相关结构和尺寸^[5],将 $a = 25 \text{ mm}$, $d_{i1} = 18.89 \text{ cm}$, $b = 20 \text{ mm}$, $d_{i2} = 1 \text{ mm}$, $w = 0.02 \text{ mm}$, $l = 0.0146 \text{ mm}$, $\lambda_1 = 557.7 \text{ nm}$, $\lambda_2 = 867.7 \text{ nm}$ 带入式(12),画出GBAlI的MTF曲线如图5所示。从图5可见,对557.7 nm和867.7 nm波长的气辉,MTF分别为0.508和0.510,对应奈奎斯特频率分别为20 lp/mm和16 lp/mm。成像系统的MTF值越高,表明该系统的分辨率越高。对于我们研制的GBAlI,在低频处MTF值大于0.51,大于WINDII的0.35 MTF^[10]。

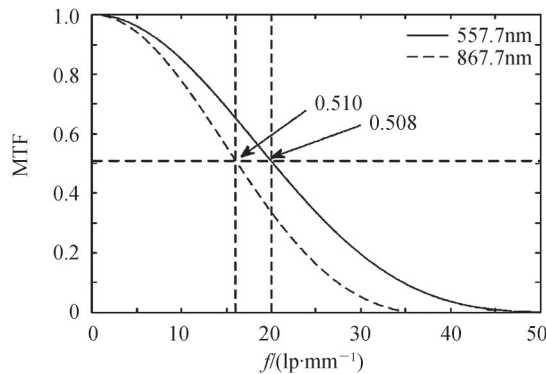


图5 GBAlI的MTF计算值
Fig. 5 Computational MTF curve of GBAlI

2 实验及讨论

GBAII样机研制成功后进行了多次拍摄。图6(a)是利用GBAII和波长632.8 nm的He-Ne激光器在实验室拍摄得到的干涉图,图6(b)是利用GBAII在西安理工大学教9楼顶(N34°13'22.21", E108°59'38.14")拍摄地球上空94 km的O₂(0-1) 867.7 nm气辉的成像干涉图(图中白点是星星),图6(c)是利用GBAII在临潼仁宗庙(N34°19'56.57'', E109°16'53'')山顶拍摄地球上空98 km的O(¹S) 557.7 nm气辉的成像干涉图。

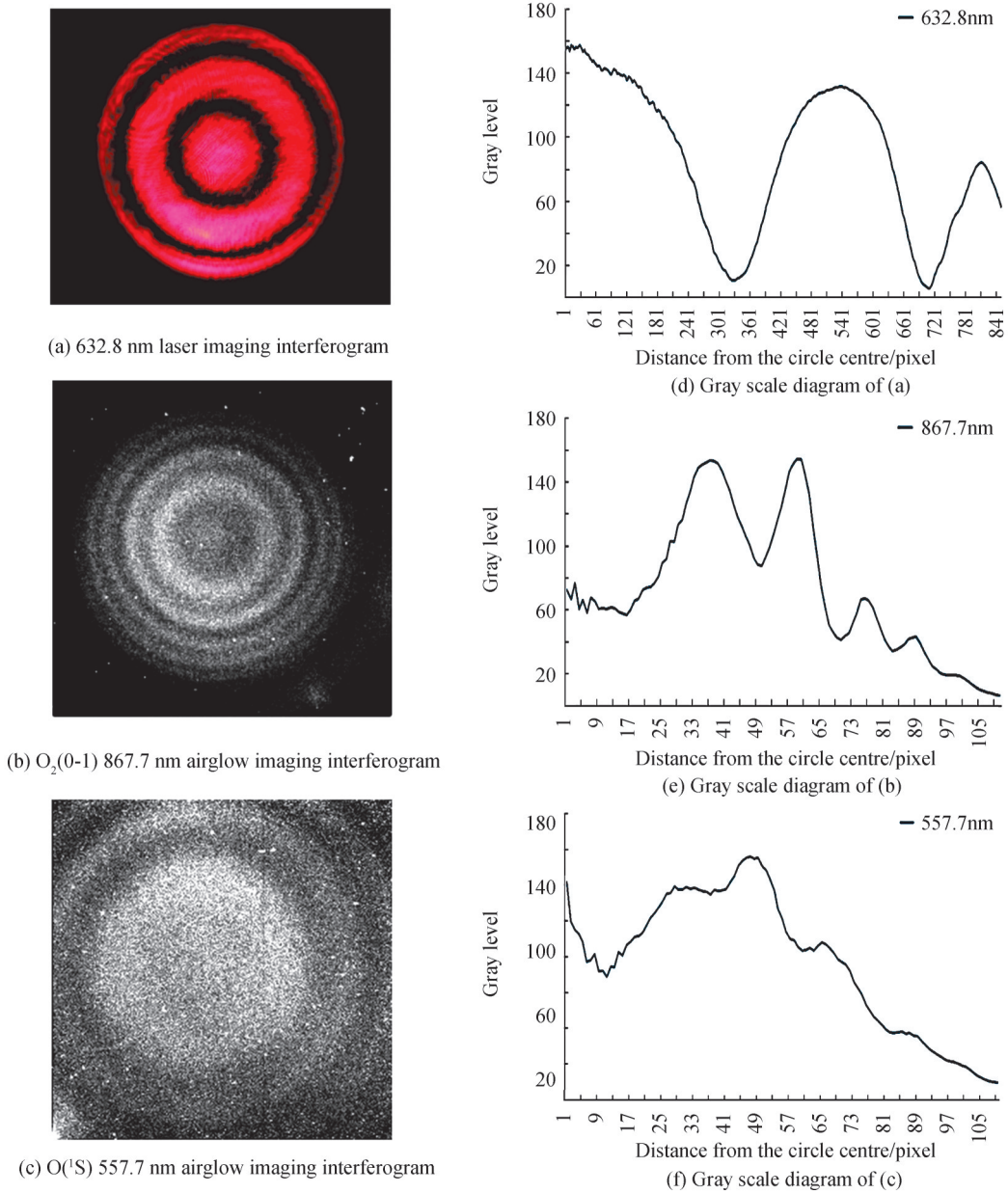


图6 GBAII拍摄所得的成像干涉图和其灰度值,所用光源分别是632.8 nm激光,867.7 nm气辉,557.7 nm气辉
Fig.6 Imaging interference fringes and gray level distribution of GBAII. The light sources used in the interferogram are 632.8 nm laser, O₂(0-1) 867.7 nm airglow and O(¹S) 557.7 nm airglow respectively

为了从实验图像中得到GBAII的MTF,先计算干涉条纹的对比度。对比度表征干涉图像的清晰程度,其值为

$$V = \frac{I_{\max} - I_{\min}}{I_{\max} + I_{\min}} \quad (13)$$

式中, I_{\max} 和 I_{\min} 为干涉条纹的最大和最小强度。通过 GBII 拍摄图 6(a)~(c) 所示的成像干涉图像, 利用 C++ 编程逐点读取图像的灰度值, 对应得到干涉条纹灰度值的分布如图 6(d)~(f) 所示, 其中横坐标是干涉圆环上各点到圆心的距离, 纵坐标是灰度值; 根据式 (13), 取图 6(d) 的第二个亮环与第二个暗环的灰度值, 得到图 6(a) 的最大对比度为 0.84; 取图 6(e) 的第二个暗环与第二个亮环的灰度值, 得到图 6(b) 的对比度为 0.58; 取图 6(f) 的第二个亮环与第三个亮环的灰度值, 得到图 6(c) 的对比度为 0.24。

鉴于成像系统的 MTF 等于像的对比度 (V_i) 除以物的对比度 (V_o): $MTF(f) = V_i/V_o$ 。事实上被摄物体的对比度 V_o 不等于 1 而小于 1, 所以对 632.8 nm 激光、867.7 nm 和 557.7 nm 气辉, 用 GBII 拍摄得到的成像干涉图的 MTF 实验值分别大于 0.84、0.58 和 0.24。

由于 GBII 观测的是地球上空 90~100 km 的气辉扩展光源, 从实验的 MTF 值来看, GBII 对双原子 O_2 分子的振转谱线的成像效果优于单原子 O 气辉。O(¹S) 557.7 nm 和 $O_2(0-1)$ 867.7 nm 气辉的强度都很低, GBII 在地面上需要通过长时间曝光方式获得气辉的成像干涉条纹。从结果上来看, GBII 室外实验得到两条气辉谱线的 MTF 结果与实验室 632.8 nm 氦氖激光的 MTF 有一定差距, 可以通过后期 GBII 的进一步优化来改进。

3 结论

地基气辉成像干涉仪 GBII 用于探测地球上空 90~100 km 处的大气风速和温度。本文研究了 GBII 成像系统的 MTF。通过 Code-V 对 GBII 系统的优化设计结构表明, 奈奎斯特频率处于子午方向的 MTF 为 0.43, 全视场弧矢方向的 MTF 为 0.18, 中心视场处 MTF 值为 0.31; 对波长为 557.7 nm、630.0 nm 和 867.7 nm 等 3 条气辉谱线, 其 MTF 的所有值均在 0.3 以上, 部分视场 MTF 高于 0.6。通过傅里叶光学规律对 GBII 的 MTF 进行理论计算后, 得出 GBII 整体系统的 MTF 表达式, 代入 GBII 在超广角、消色散、热补偿条件下的相关参数, 对波长为 867.7 nm 和 557.7 nm 的气辉, 在奈奎斯特频率处的 MTF 分别为 0.510 和 0.508; 在实验室内外分别利用 632.8 nm He-Ne 激光器、 $O_2(0-1)$ 867.7 nm 和 O(¹S) 557.7 nm 气辉作为光源, 拍摄得到 GBII 的成像干涉图, 得到实验 MTF 值分别大于 0.84、0.58、0.24。

可以看出 GBII 优化设计、理论计算和实际拍摄图片的 MTF 值有一定偏差, 用激光作为光源 GBII 的实验值 MTF 值最大, 对 557.7 nm 气辉谱线的实验 MTF 稍小, 软件优化 MTF 值居中。总体来看, GBII 的 MTF 值与 WINDII 的 0.35 MTF 相当。通过本文研究 GBII 的 MTF 值可见, GBII 对双原子 O_2 分子的振转谱线成像效果好于单原子 O 气辉, 以后要开发 GBII 用于多原子的气辉测试, 改进对单原子气辉谱线的成像效果。这些研究为 GBII 进一步探测高层大气风速、温度、体发射率等物理量提供了理论保证。

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MTF Study of GBAII for Detecting Airglow 90~100 km above the Earth

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Abstract: Ground-Based Airglow Imaging Interferometer (GBAII) is a ground-based wind field detection prototype developed by our research group that integrates the principles of "rotational spectral line temperature measurement" and "four-intensity method". The imaging interferogram of airglow 90~100 km above the earth can be obtained by taking long time exposure of 200 s. Then the information of atmospheric wind speed, temperature and volume emissivity over the Earth can be obtained from the imaging interference fringe. Modulation Transfer Function (MTF) is a very important index in the design, development and testing of ground-based airglow imaging interferometer GBAII, which can characterize the imaging quality of GBAII. In this paper, the modulation transfer function of ground-based airglow imaging interferometer is studied. By using He-Ne laser wavelength of 632.8 nm, O₂(0-1) 867.7 nm and O(¹S) 557.7 nm as light sources, the MTF values of the optimized design, theoretical calculation and actual images are given. Firstly, the optical imaging structure of GBAII consists of five parts: a tapered mirror light receiving system, a wide-angle MI phase modulation system, a narrowband interference filter, a CCD and three lenses. The optical structure of GBAII is optimized by Code V, and the point sequence diagram of GBAII was obtained. 4×4 was used as a bin, and the diameter of dispersion spot was about 60 μm at 0° field of view, and 80~90 μm at 2°~9.5° field of view, and the limit resolution was 6.25 lp/mm. For the three airglow lines with wavelength 557.7 nm, 630.0 nm and 867.7 nm, all the MTF values are above 0.3, and some of the MTF values are higher than 0.6. However, it can also be seen that the MTF

meridional branch and sagittal branch differ greatly in the full field of view, mainly caused by astigmatism. Secondly, according to Fourier optical theory, the MTF expression of GBII optical system is obtained by calculating the MTF of wide-angle Michelson interferometer, interference filter and CCD. The MTF curve of GBII is given by substituting the MTF expression of GBII into the relevant structure and size of GBII optimized by ultra-wide Angle, thermal compensation and achromatic conditions. For airglow wavelengths at 557.7 nm and 867.7 nm, the MTF value is 0.508 and 0.510, corresponding to Nyquist frequencies of 20 lp/mm and 16 lp/mm, respectively. For the GBII developed by our researcher group, the MTF value is greater than 0.51 at low frequency, which is greater than 0.35 MTF of international famous wind imaging interferometer WINDII. Thirdly, in order to obtain the experimental MTF value of GBII, it is necessary to take imaging interferogram through GBII first, and use software to read gray value of image point by point to calculate contrast of interference fringes. The MTF of GBII imaging system is equal to the contrast of the image divided by the contrast of the object, where, the contrast of the subject is not equal to but less than 1. He-Ne laser spectrum line of 632.8 nm, O₂(0-1) 867.7 nm and O(¹S) 557.7 nm were used as light sources respectively to obtain the indoor and outdoor imaging interferogram of GBII. The experimental MTF of different wavelengths was obtained according to contrast of imaging interferogram. The MTF value of GBII is greater than 0.8, 0.58 and 0.24 at the wavelength of 632.8 nm laser, O₂(0-1) 867.7 nm and O(¹S) 557.7 nm airglow, respectively. Based on the MTF value of GBII studied in this paper, the experimental MTF values show that GBII has better imaging effect on the vibration spectra of diatomic O₂ molecules than that of single atomic O airglow. Since the intensity of O(¹S) 557.7 nm and O₂(0-1) 867.7 nm airglow is very low, the imaging interference fringes of GBII airglow need to be obtained by long time exposure on the ground. In terms of the results, the MTF results of the two airglow spectra obtained by GBII outdoor experiment have a certain gap with that of the laboratory 632.8 nm He-Ne laser, which can be improved by further optimization of GBII later. It can be seen from the above results that the MTF value of GBII optimized design, theoretical calculation and actual image has a certain deviation. When laser is used as the light source, the experimental MTF value of GBII is the largest, and the experimental MTF value of 557.7 nm airglow spectrum line is slightly smaller, and the MTF value of software optimization is in the middle. Overall, the MTF result of GBII theory and experiment is better than 0.35 MTF of WINDII. The study of MTF of GBII can provide technical basis for GBII to successfully detect atmospheric wind field parameters. The research results can provide accurate technical basis for GBII to successfully detect physical quantities such as wind speed, temperature and volume emissivity in the upper atmosphere, and also lay a theoretical and experimental foundation for the development of similar instruments in China.

Key words: Ground-based airglow imager interferometer; Modulation transfer function; Interferometric imaging; Airglow; Optical instrument

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