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强聚焦混合偏振矢量光束在瑞利粒子上产生的辐射力

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摘 要: 理论研究了强聚焦混合偏振矢量光束作用在瑞利粒子的辐射力, 推导出混合偏振矢量光束深聚焦在焦平面处产生辐射力的计算表达式, 数值模拟了焦平面附近轴向光束强度分布及数值孔径与径向系数对辐射力分布的影响. 结果表明, 强聚焦混合偏振矢量光束深聚焦后在焦平面附近产生的辐射力在一定情况下能够实现对瑞利粒子的三维捕获, 并且受数值孔径和径向系数的影响, 其中径向系数影响较为明显. 大量数据整合结果表明当径向系数大于 3 时, 才能实现与光阑数值孔径相匹配, 完成对焦平面附近瑞利粒子的三维捕获.

关键词: 物理光学, 混合偏振, 强聚焦, 瑞利粒子, 辐射力

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Radiation Forces on a Rayleigh Particle by Highly Focused Hybridly Polarized Vector Beams

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Abstract: The radiation force of highly focused hybridly polarized beams on a Rayleigh particle was theoretically studied and the expression was derived. The influence of numerical apertures of an objective and radial coefficient on the radiation force distribution and the longitudinal intensity distribution on the focal plane were numerically simulated. The numerical results show that radiation forces by highly focused hybridly polarized vector beams can be used to trap three-dimensional Rayleigh particles, and the trapping property is affected by the numerical aperture and radial coefficient obviously. Copious experimental data indicate that it can be done only when the radial coefficient is greater than 3.

Key words: Physical optics; Hybridly polarized; Highly focused; Rayleigh particle; Radiation forces

OCIS Codes: 140.7140; 020.7010; 020.1670; 010.3310

0 引言

光辐射压力是由于光子动量的改变而产生的, 作为光镊领域的先驱 Ashkin 在 1986 年成功地利用强度分布不均匀的单束激光产生光辐射压力^[1]. 之后, 研究者利用不同类型的光束成功实现了对不同类型粒子的光学捕获^[2], 如洛伦兹高斯光束^[3]、零阶贝塞尔高斯光束^[4]、高斯谢尔模型光束^[5]、柱对称矢量光束^[6-7], 先后捕获了原子、分子、纳米颗粒, 并成功应用于生物领域

中活生物细胞和 DNA 分子^[8]方面. 最近, 一种新型的随径向变化的混合偏振矢量光束由于其强聚焦^[9]后独特的性质^[10-11]成为研究热点. 2010 年, 南开大学汪喜林、王慧田等研究了更复杂的矢量光束^[10]. J. Pu 等在 2011 年对双环角向偏振光束经过环状大数值孔径透镜聚焦进行了详细的研究, 发现一个更长的焦深的亚波长量级的“光渠”^[12]. 径向偏振光独特的深聚焦性质已经在光镊、金属切割、提高分辨率等方面有着重要应用^[13]. 另外角向偏振光束经过高数值孔径具有聚焦光

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场不带有涡旋相位等独特的性质,在粒子操控等方面的应用有重要的意义^[14].

本文研究了混合偏振矢量光束经过大数值孔径透镜聚焦在瑞利粒子^[15]上产生的辐射压力^[16],推导出焦平面附近辐射力的表达式,数值模拟分析了径向系数和透镜的数值孔径对产生的辐射力的影响.

1 原理分析

假设入射波为一具有混合偏振态完全相干光,深聚焦原理如图 1.

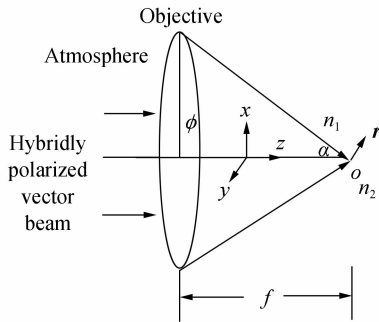


图 1 混合偏振光束经过环形光阑深聚焦系统
Fig. 1 The system of highly focused hybridly polarized vector beams through an annular aperture

透镜后的切趾函数^[17]可表示为

$$\begin{cases} A_x(r) = A(r) \exp [i(2n\pi \frac{r}{r_0} + \beta)] \\ A_y(r) = A(r) \exp [i(-2n\pi \frac{r}{r_0} + \beta)] \end{cases} \quad (1)$$

式中 n 为径向系数, f 为透镜焦距, θ 为光束收敛角, β 为初相位,它决定着入射光束偏振态, r_0 为矢量场的半径.

入射光束的径向系数 n 和初相位 β 对混合偏振矢量场偏振态的影响如图 2^[18].

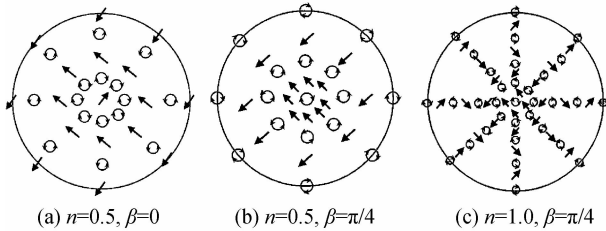


图 2 入射光束径向系数和初相位对混合偏振矢量场偏振态的影响
Fig. 2 The influence on hybridly polarized vector beams by the radial coefficient and initial phase

假设源平面处的入射光束的光强呈高斯分布,由于矢量场半径为 r_0 ,因此其电场可以表示为

$$A(r) = E_0 \text{circ} \left(\frac{r}{r_0} \right) \exp \left(-\frac{r^2}{\omega_0^2} \right) \quad (2)$$

式中 ω_0 是光束的半径, E_0 是常量.

假设入射光的功率为 p ,源平面处得强度分布为 $I_0(r)$,利用关系式^[19]

$$p = \iint I_0(r) ds \quad (3)$$

可以得到电场的振幅常量为

$$E_0 = \sqrt{\frac{2p}{\pi \cdot \omega_0^2 \cdot \left(1 - \exp \left(\frac{-2r_0^2}{\omega_0^2} \right) \right)}} \quad (4)$$

所以式(2)可以表示为

$$A(r) = \sqrt{\frac{2p}{\pi \cdot \omega_0^2 \cdot \left(1 - \exp \left(\frac{-2r_0^2}{\omega_0^2} \right) \right)}} \cdot \text{circ} \left(\frac{r}{r_0} \right) \exp \left(-\frac{r^2}{\omega_0^2} \right) \quad (5)$$

根据正弦条件 $r = f \cdot \sin \theta$ ^[20],透镜后的切趾函数为

$$\begin{cases} A_x(\theta) = \sqrt{\frac{2p}{\pi \cdot \omega_0^2 \cdot \left(1 - \exp \left(\frac{-2r_0^2}{\omega_0^2} \right) \right)}} \cdot \text{circ} \left(\frac{f \cdot \sin(\theta)}{r_0} \right) \exp \left(-\frac{f^2 \cdot \sin^2(\theta)}{\omega_0^2} \right) \cdot \exp \left[i \left(2n\pi \frac{f \cdot \sin(\theta)}{r_0} + \beta \right) \right] \\ A_y(\theta) = \sqrt{\frac{2p}{\pi \cdot \omega_0^2 \cdot \left(1 - \exp \left(\frac{-2r_0^2}{\omega_0^2} \right) \right)}} \cdot \text{circ} \left(\frac{f \cdot \sin(\theta)}{r_0} \right) \exp \left(-\frac{f^2 \cdot \sin^2(\theta)}{\omega_0^2} \right) \cdot \exp \left[i \left(-2n\pi \frac{f \cdot \sin(\theta)}{r_0} + \beta \right) \right] \end{cases} \quad (6)$$

基于 Richards 和 Wolf 提出得矢量衍射积分公式^[21-22],经过大数值孔径聚焦后在焦平面处的电场可表示为

$$\begin{cases} E_x(r, \varphi, z) = -\frac{k \cdot f}{2 \sqrt{n_1}} \cdot i \cdot \int_0^\vartheta \sin \theta \sqrt{\cos \theta} \cdot \exp(i k z \cos \theta) \{ A_x(\theta) J_0(k r \sin \theta) (\cos \theta + 1) + J_2(k r \sin \theta) (1 - \cos \theta) [A_x(\theta) \cos(2\varphi) + A_y(\theta) \sin(2\varphi)] \} d\theta \\ E_y(r, \varphi, z) = -\frac{k \cdot f}{2 \sqrt{n_1}} \cdot i \cdot \int_0^\vartheta \sin \theta \sqrt{\cos \theta} \cdot \exp(i k z \cos \theta) \{ A_y(\theta) J_0(k r \sin \theta) (\cos \theta + 1) + J_2(k r \sin \theta) (1 - \cos \theta) [A_x(\theta) \sin(2\varphi) - A_y(\theta) \cos(2\varphi)] \} d\theta \\ E_z(r, \varphi, z) = -\frac{k \cdot f}{\sqrt{n_1}} \cdot \int_0^\vartheta \sin^2 \theta \sqrt{\cos \theta} \cdot \exp(i k z \cos \theta) \{ J_1(k r \sin \theta) [A_x(\theta) \cos \varphi + A_y(\theta) \sin \varphi] \} d\theta \end{cases} \quad (7)$$

式中, r, φ, z 为观察点处柱坐标, $\vartheta = \sin^{-1}(NA/n_1)$ 为最大数值孔径角, k 为波数 $k = 2\pi \cdot n_1/\lambda$, n_1 为像空间的折射率.

基于式(7),可以得到电场的径向和角向分量为

$$\begin{cases} E_r(r, \varphi, z) = E_x(r, \varphi, z) \cos \varphi + E_y(r, \varphi, z) \sin \varphi \\ E_\varphi(r, \varphi, z) = -E_x(r, \varphi, z) \sin \varphi + E_y(r, \varphi, z) \cos \varphi \end{cases} \quad (8)$$

焦平面处的光强表达式为

$$I(r, z) = |E_r(r, \varphi, z)|^2 + |E_\varphi(r, \varphi, z)|^2 + |E_z(r, \varphi, z)|^2 \quad (9)$$

选取瑞利粒子作为捕获粒子^[23],可将其看做一电偶极子,根据瑞利散射理论来计算辐射力^[19]可将辐射力分为散射力和梯度力,散射力可表示为

$$F_{\text{scat}}(r, z) = \frac{n_1}{c} C_{\text{pr}} I(r, z) \mathbf{e}_z \quad (10)$$

式中 $c = \frac{1}{\sqrt{\epsilon_0 \mu_0}}$, $C_{\text{pr}} = \frac{8}{3} \pi (ka)^4 a^2 \left(\frac{m^2 - 1}{m^2 + 2} \right)^2$, a 为瑞利粒子的半径, $m = n_1 / n_2$, n_1 、 n_2 分别为周围介质和瑞利粒子的折射率. 由于大数值孔径聚焦具有退偏振效应^[24-25],焦平面处会产生轴向和径向的梯度力^[26],轴向梯度力^[27]表示为

$$F_{\text{grad}z}(r, z) = \frac{2\pi n_1 a^3}{c} \left(\frac{m^2 - 1}{m^2 + 2} \right) \frac{\partial}{\partial z} I(r, z) \quad (11)$$

径向梯度力表示为

$$F_{\text{grad}r}(r, z) = \frac{2\pi n_1 a^3}{c} \left(\frac{m^2 - 1}{m^2 + 2} \right) \frac{\partial}{\partial r} I(r, z) \quad (12)$$

2 数值模拟

根据式(10)~(12),数值模拟了混合偏振矢量光束经过大数值孔径聚焦后,在瑞利粒子上产生的辐射力,如果没有特殊说明,参量选取为: $\lambda = 532 \text{ nm}$, $\beta = 0$, $f = 0.00125 \text{ m}$, $\omega_0 = 0.002 \text{ m}$, $r_0 = 0.0025 \text{ m}$, $p = 2 \text{ W}$, $n_1 = 1.332$, $n_2 = 1.592$, $a = 26.6 \text{ nm}$.

焦平面附近轴向光强分布如图3所示. 由于混合偏振矢量光束为柱对称矢量光束,其横向光强分布具有圆对称性,因此只模拟了在 $x-z$ 平面上焦平面附近光强分布. 从图3可以看出 $n=1$ 时,在焦点附近形成光强分布呈椭圆形的光斑, $n=1.6$ 时,在沿轴方向上形成一半值全宽能量分布均匀的“光针”,其附近获得最大焦深约为 5λ . 随着径向系数的变大,如图3(c)、

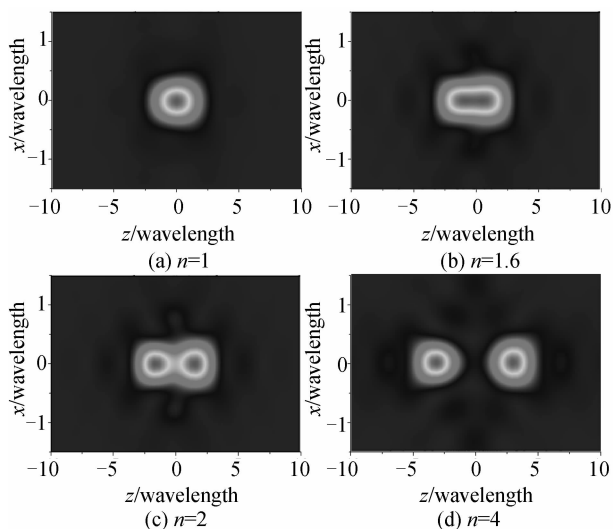


图3 入射光束径向参数对光强分布的影响

Fig. 3 The influence of light intensity distribution by radial parameters of incident beam

(d),焦点附近光强形状逐渐由椭圆变成圆环,且焦环半径随着径向系数逐渐变大.

图4说明数值孔径对各辐射力作用明显. 图4(a)中散射力随着数值孔径的增大而增大,是因为较大的数值孔径聚焦后形成较小的光斑,具有较集中的光强分布,图4(b)、(c)中都有类似的影响. 数值模拟选取径向系数 $n=3$ 不能实现对作用粒子稳定的三维捕获,这是因为图4(c)中每一数值孔径下的径向梯度力与图4(a)中相应数值孔径下的散射力相差不大,达不到稳定捕获的条件^[28].

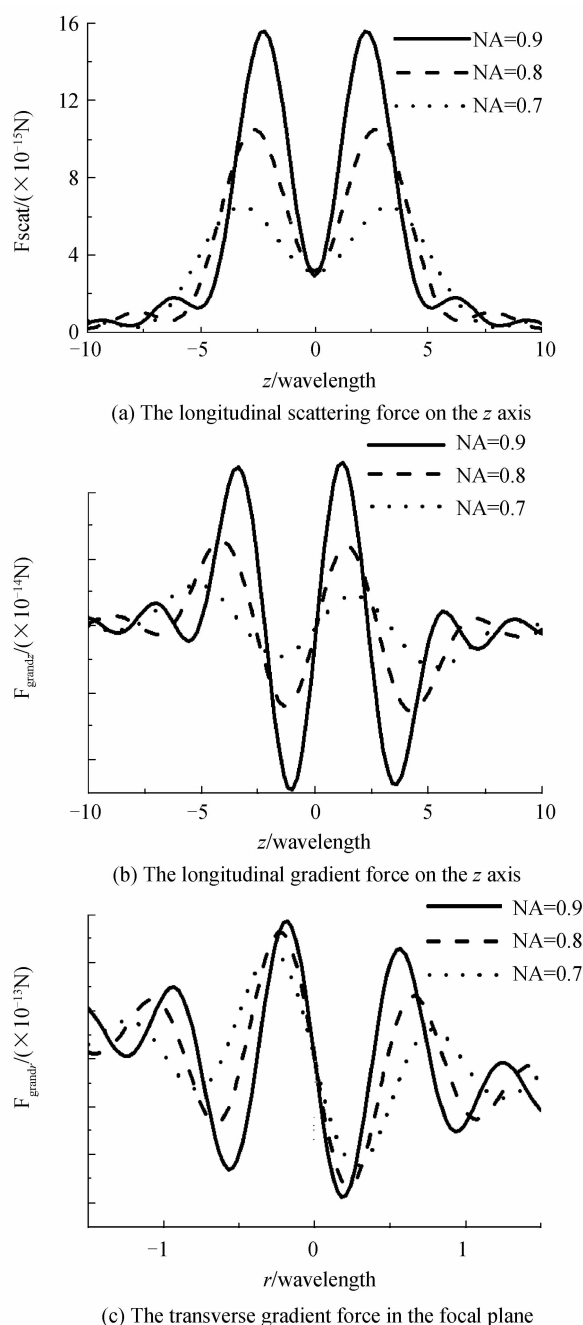


图4 $n=3$ 时,强聚焦混合偏振矢量光束在瑞利粒子上的辐射力

Fig. 4 The radiation forces produced by highly focused hybridly polarized vector beams, $n=3$

图5说明各辐射力受径向系数作用明显,各辐射力最大值均随着径向系数的变大而变小,这是因为随着径向系数的变大,焦斑的形状会从一个椭圆变成一个圆环,且焦环的半径逐渐变大(如图3). $n=1$ 时,焦斑为一椭圆,此时在焦点处容易成功捕获粒子; $n=2$ 时,焦斑变为一圆环,焦点处光强减弱,将在焦点附近实现对粒子的三维捕获.当 n 较大时,如 $n=3$ 或4时,图5(c)中所对应的径向梯度力与图5(a)中散射力相差不大(至少两个数量级),故不能实现三维光矢阱^[29]的稳定捕获.从图中还可以看出(a)、(b)中辐射力的最

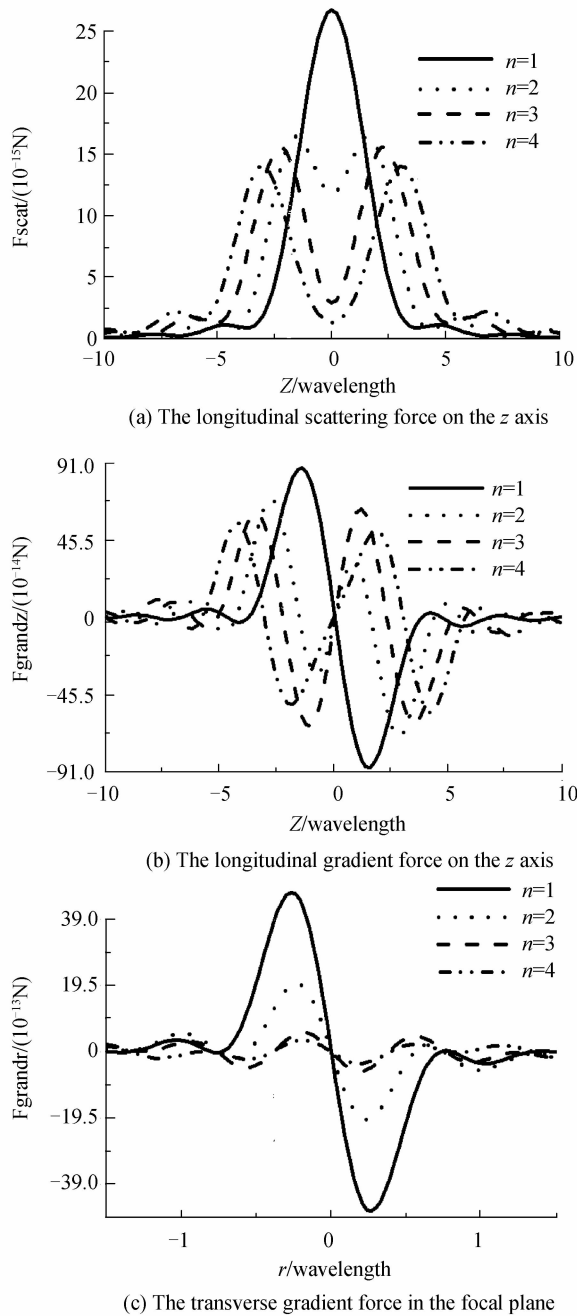


图5 NA=0.9时,强聚焦混合偏振矢量光束在瑞利粒子上的辐射力

Fig. 5 The radiation forces produced by highly focused hybridly polarized vector beams, NA=0.9

大值均随数值孔径的变大逐渐靠近焦平面,而(c)中径向梯度力的最大值随着径向系数的变大逐渐远离 z 轴,为三维稳定捕获创造了条件.

由图4、5均可以看出,在焦点附近,当径向系数达到一定值时,同一位置处的轴向梯度力要大于散射力,径向梯度力要比轴向辐射力大,当达到至少两个数量级时^[30],就达到三维光学稳定捕获.考虑到研究瑞利粒子的散射力,当捕获粒子很小时,其在介质中受到的布朗力将不可忽略,选取粒子半径 $a=26.6$ nm,布朗力量级为 $|F_B|=(12\pi\kappa a k_B T)^{1/2}$,其中 κ 为介质的粘滞系数,本文中为水 $\kappa=7.977\times 10^{-4}$,温度 $T=300$ K, k_B 为波尔兹曼常量,计算其数量级为 1.933×10^{-3} pN,与图4中模拟出的梯度力相比,此情况下的布朗力可以忽略不计,故讨论仍然成立.

3 结论

本文数值模拟了强聚焦混合偏振矢量光束作用在瑞利粒子上的辐射力.研究发现数值孔径与径向系数对其辐射力影响明显,大数值孔径会使聚焦光斑半径变小,具有很强的强度分布,而径向系数的增大会使聚焦焦斑从一个圆变成一个圆环.这种混合偏振矢量光束能够在焦平面附近产生很强的纵向电场,有利于更好地捕获粒子.另外,不同于简单的线偏振,这种矢量光束具有更为复杂的偏振分布,可以通过控制入射光束的偏振态来控制对焦平面粒子的捕获情况,这是其他光束没有的特性.

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