# 单模锥形光纤锥区光场及超短脉冲的传输特性\*

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摘 要:根据光波导理论,采用数值方法分析了单模锥形光纤维区传输常数和光场分布的变化情况.采用分步傅里叶法数值求解广义的非线性薛定谔方程,对超短脉冲在锥区的传输演化进行了研究.结果表明:传输常数沿拉锥方向缓慢减小,在拉锥末端迅速减小;在拉锥初始阶段,能量主要集中在纤芯中,"转换点"之后能量在纤芯和包层中重新分布,光强在拉锥末端变强;脉宽小于80 fs 的超短脉冲沿锥区传输时,沿拉锥方向,脉冲不断展宽,而当脉宽大于80 fs 时,脉冲展宽不明显.

关键词:导波与光纤光学;传播常数;光场传输;超短脉冲

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# 0 引言

近年来,随着锥形光纤在医学<sup>[1]</sup>、近场光学显微镜<sup>[2]</sup>、光纤传感与检测、超连续谱产生和光纤色散补偿等各领域应用的迅速开展,锥形光纤的理论和实验研究已引起科技工作者的广泛关注.目前,有关锥形光纤的研究主要集中在腰区<sup>[3-5]</sup>,此时光纤直径不变,将光纤视为二层(空气层与纤芯层).文献[6-7]分析了锥形光纤中模式的传输特性以及拉锥光纤的锥度对光波模场分布的影响;文献[8]采用高斯模场近似和模场匹配方法,仿真计算了超辐射 LD 与带类球透镜保偏光纤的耦合技术;文献[9-10]研究了熔锥光纤锥区传输、耦合、偏振和调制特性.

但是,在锥形光纤的锥区,光纤的直径随着拉锥的进行不断发生变化.锥区的光场分布、非线性系数及色散参量的分析计算对于理解整段光纤的光传输和非线过程(自相位调制、四波混频、孤子分裂等)有重要作用.脉冲在锥区的演化特性对于研究超连续谱在锥形光纤中的产生有重要意义.本文的研究集中在锥形光纤的锥区,应用光波导理论,将锥形光纤视为三层光纤(纤芯层、包层和空气层),通过求解特征方程,用数值方法计算了850 nm 和500 nm 的光波的传输常数以及光场的分布.从广义非线性薛定谔方程出发,数值模拟了脉宽为20 fs、30 fs、40 fs、50 fs 的超短脉冲在锥区的传输演化情况.

# 1 基本理论

#### 1.1 光波导理论

本文所研究的单模锥形光纤包层半径表达式

Tel: 13430345080 Email: yuzhiqiang612@163.com 收稿日期:2008-09-17 修回日期:2008-11-27 为[11]

 $r_{\text{clading}}(\mu \text{m}) = -1.9 + 67.8 \exp(-z/4.7)$  (1)

式中  $r_{\text{clading}}$  为包层半径; z 为光传输方向,即光纤拉锥方向. 在拉锥过程中包层与纤芯半径比保持不变. 图 1 和图 2 分别为锥形光纤锥区结构图和折射率分布图. 图中 a、b 分别为纤芯和包层的半径, r 为沿径向的距离. 对于绝热近似过程[12],由光纤半径变化引起的能量从基模向高阶模的转化可以忽略[13]. 在这种光纤中传输的模式为基模(HE<sub>11</sub> 或LP<sub>01</sub>).

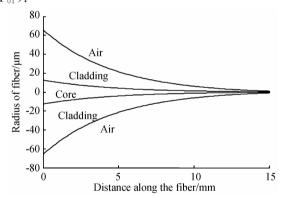


图 1 锥形光纤锥区结构

Fig. 1 Radial profile along the tapered fiber

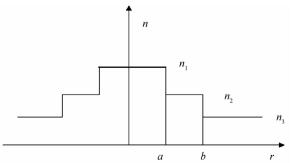


图 2 锥区横截面折射率分布

Fig. 2 Index profile of the tapered fiber

考虑空气层,将锥形光纤视为三层:纤芯、包层和空气,其折射率分别为 $n_1, n_2, n_3$ . 在计算时,取空

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气折射率为 1,纤芯和包层的折射率满足塞尔迈耶尔(Sellmeier)方程[14]

$$n^{2}(\lambda_{0}) = 1 + \frac{b_{1}\lambda_{0}^{2}}{\lambda_{0}^{2} - a_{1}} + \frac{b_{2}\lambda_{0}^{2}}{\lambda_{0}^{2} - a_{2}} + \frac{b_{3}\lambda_{0}^{2}}{\lambda_{0}^{2} - a_{3}} + \cdots$$
 (2)

式中  $\lambda_0$  为光场中心波长(以  $\mu$ m 为量纲),相应的其他参量可分别表示为:

纤芯时, $a_1 = 0.007290464$ , $a_2 = 0.01050294$ ,

 $a_3 = 97.93428$ ,  $b_1 = 0.7083952$ ,  $b_2 = 0.4203993$ ,  $b_3 = 0.8663412$ ; 包层时,  $a_1 = 0.004679148$ ,  $a_2 = 0.01351206$ ,  $a_3 = 97.93400$ ,  $b_1 = 0.6961663$ ,  $b_2 = 0.4079426$ ,  $b_3 = 0.8974794$ .

根据光波导理论<sup>[15]</sup>,可得径向场在各个区域的分量为

$$R(r) = \begin{cases} A_{0}J_{m}\left(U_{1}\frac{r}{a}\right) & 0 \leqslant r \leqslant a \\ A_{1}J_{m}\left(U_{2}\frac{r}{b}\right) + A_{2}Y_{m}\left(U_{2}\frac{r}{b}\right) & a \leqslant r \leqslant b \\ A_{3}J_{m}\left(W_{1}\frac{r}{b}\right) & r \geqslant b \end{cases}$$

$$R(r) = \begin{cases} A'_{0}J_{m}\left(U_{1}\frac{r}{a}\right) & 0 \leqslant r \leqslant a \\ A'_{1}I_{m}\left(W_{2}\frac{r}{b}\right) + A_{2}K_{m}\left(W_{2}\frac{r}{b}\right) & a \leqslant r \leqslant b \\ A'_{3}K_{m}\left(W_{1}\frac{r}{b}\right) & r \geqslant b \end{cases}$$

$$(\beta > k_{0}n_{2})$$

$$(4)$$

式中,R(r)为径向场分量;a、b 分别为纤芯和包层半径; $\beta$  为传输常量; $k_0$  为真空中的波矢; $J_m$ 、 $Y_m$  分别为第一类、第二类贝塞尔函数; $K_m$ 、 $I_m$  分别为第一类、第二类变形的贝塞尔函数; $A_0$ 、 $A_1$ 、 $A_2$ 、 $A_3$  及 $A_0$ 0、 $A_1$ 1、 $A_2$ 1、 $A_3$ 2 从为常量; $U_1 = a$ 2  $\sqrt{k_0^2 n_1^2 - \beta^2}$ , $U_2 = a$ 3 以为常量; $U_1 = a$ 4  $\sqrt{k_0^2 n_1^2 - \beta^2}$ , $U_2 = a$ 5 以为常量; $U_1 = a$ 5  $\sqrt{k_0^2 n_1^2 - \beta^2}$ , $U_2 = a$ 6  $\sqrt{k_0^2 n_1^2 - \beta^2}$ , $U_2 = a$ 6  $\sqrt{k_0^2 n_1^2 - \beta^2}$ , $U_2 = a$ 6  $\sqrt{k_0^2 n_1^2 - \beta^2}$ , $U_2 = a$ 6  $\sqrt{k_0^2 n_1^2 - \beta^2}$  , $U_2 = a$ 6  $\sqrt{k_0^2 n_1^2 - \beta^2}$  , $U_2 = a$ 6  $\sqrt{k_0^2 n_1^2 - \beta^2}$  , $U_2 = a$ 6  $\sqrt{k_0^2 n_1^2 - \beta^2}$  , $U_2 = a$ 6  $\sqrt{k_0^2 n_1^2 - \beta^2}$  , $U_2 = a$ 6  $\sqrt{k_0^2 n_1^2 - \beta^2}$  , $U_2 = a$ 6  $\sqrt{k_0^2 n_1^2 - \beta^2}$  , $U_2 = a$ 6  $\sqrt{k_0^2 n_1^2 - \beta^2}$  , $U_2 = a$ 6  $\sqrt{k_0^2 n_1^2 - \beta^2}$  , $U_2 = a$ 6  $\sqrt{k_0^2 n_1^2 - \beta^2}$  , $U_2 = a$ 6  $\sqrt{k_0^2 n_1^2 - \beta^2}$  , $U_2 = a$ 6  $\sqrt{k_0^2 n_1^2 - \beta^2}$  , $U_2 = a$ 6  $\sqrt{k_0^2 n_1^2 - \beta^2}$  , $U_2 = a$ 6  $\sqrt{k_0^2 n_1^2 - \beta^2}$  , $U_2 = a$ 6  $\sqrt{k_0^2 n_1^2 - \beta^2}$  , $U_2 = a$ 6  $\sqrt{k_0^2 n_1^2 - \beta^2}$  , $U_2 = a$ 6  $\sqrt{k_0^2 n_1^2 - \beta^2}$  , $U_2 = a$ 6  $\sqrt{k_0^2 n_1^2 - \beta^2}$  , $U_2 = a$ 7  $U_2 = a$ 8  $U_2 = a$ 8  $U_3 = a$ 9  $U_3 = a$ 9

 $b\sqrt{k_0^2n_2^2-\beta^2}$ , $W_1=b\sqrt{\beta^2-k_0^2n_2^2}$ , $W_2=b\sqrt{\beta^2-k_0^2n_3^2}$ 为波导的归一化横向波数.

在 r=a 和 r=b 两个边界面上,由于 R(r) 和  $\frac{\partial R(r)}{\partial r}$  连续,可得

当 $\beta < k_0 n_2$ 时,

$$\begin{bmatrix}
J_{m}(U_{1}) & J_{m}(U_{2}Q) & Y_{m}(U_{2}Q) & 0 \\
U_{1}J_{m}^{'}(U_{1}) & U_{2}QJ_{m}^{'}(U_{2}Q) & U_{2}QY_{m}^{'}(U_{2}Q) & 0 \\
0 & J_{m}(U_{2}) & Y_{m}(U_{2}) & K_{m}(W_{1}) \\
0 & U_{2}J_{m}^{'}(U_{2}) & U_{2}Y_{m}^{'}(U_{2}) & W_{1}K_{m}^{'}(W_{1})
\end{bmatrix}
\begin{bmatrix}
A_{0} \\
A_{1} \\
A_{2} \\
A_{3}
\end{bmatrix}$$
(5)

得

$$\frac{\left[\overset{\wedge}{J}_{m}(U_{1})-\overset{\wedge}{Y}_{m}(U_{2}Q)\right]\left[\overset{\wedge}{K}_{m}(W_{1})-\overset{\wedge}{J}_{m}(U_{1})\right]}{\left[\overset{\wedge}{J}_{m}(U_{1})-\overset{\wedge}{J}_{m}(U_{2}Q)\right]\left[\overset{\wedge}{K}_{m}(W_{1})-\overset{\wedge}{Y}_{m}(U_{2})\right]} = \frac{J_{m+1}(U_{2}Q)Y_{m+1}(U_{2})}{J_{m+1}(U_{2})Y_{m+1}(U_{2}Q)}$$

$$\overset{\cong}{\exists} \beta > k_{0} n_{2} \text{ B}, \qquad (6)$$

$$\begin{bmatrix} I_{m}(U_{1}) & I_{m}(W_{1}Q) & K_{m}(W_{2}Q) & 0 \\ U_{1}J'_{m}(U_{1}) & W_{2}QI'_{m}(U_{2}Q) & W_{2}QK'_{m}(U_{2}Q) & 0 \\ 0 & I_{m}(U_{2}) & K_{m}(W_{2}) & -K_{m}(W_{1}) \\ 0 & W_{2}I'_{m}(W_{2}) & W_{2}K'_{m}(W_{2}) & W_{1}K'_{m}(W_{1}) \end{bmatrix} \begin{bmatrix} A'_{0} \\ A'_{1} \\ A'_{2} \\ A'_{3} \end{bmatrix}$$

$$(7)$$

得

$$\frac{\left[\overset{\wedge}{J}_{m}(U_{1})-\overset{\wedge}{K}_{m}(W_{2}Q)\right]\left[\overset{\wedge}{K}_{m}(W_{1})+\overset{\wedge}{I}_{m}(W_{2})\right]}{\left[\overset{\wedge}{J}_{m}(U_{1})+\overset{\wedge}{I}_{m}(W_{2}Q)\right]\left[\overset{\wedge}{K}_{m}(W_{1})-\overset{\wedge}{K}_{m}(W_{2})\right]} = \frac{I_{m+1}(W_{2}Q)K_{m+1}(W_{2})}{I_{m+1}(W_{2})K_{m+1}(W_{2}Q)}$$
(8)

式中, $\overset{\wedge}{Z}_m(x) = \frac{Z_m(x)}{xZ_{m+1}(x)}; Q = \frac{a}{b}.$ 

从式(3)~(8)可以看出,当光波在锥形光纤中传输时,存在一个"转换点"( $\beta=k_0n_2$ ).在此点之前, $\beta>k_0n_2$ ,计算锥形光纤的光场分布和传输常量的方

程分别为式(3)和式(6). 在此点之后, $\beta < k_0 n_2$ ,计算锥形光纤的光场分布和传输常量的方程则分别为式(4)和式(8).

#### 1.2 单模光纤内脉冲的演化方程

超短光脉冲在光纤中满足的广义非线性薛定谔 方程为<sup>[16]</sup>

$$\frac{\partial A}{\partial z} + \frac{\alpha}{2} A - i \sum_{k \ge 2} \frac{\beta_k}{k} \frac{\beta^k A}{\beta T^k} = i \gamma \left[ |A|^2 + i \frac{\lambda_0}{2\pi c} \frac{\partial}{\partial T} (|A|^2 A - T_R A \partial |A|^2 / (\partial T)) \right]$$
(9)

式中左边为线性项:第一项表示脉冲传输(A 为脉冲慢变包络振幅,z 为脉冲在光纤中的传输距离);第二项表示光纤损耗( $\alpha$  为光纤损耗系数);第三项表示色散效应( $\beta_k$  为各阶群速度色散,k 表示色散阶数,T 为以中心波长群速度为移动参考系的时间参量).方程右边为非线性项( $\gamma = n_2 \omega_0 / c A_{\rm eff}$  为非线性系数,对应各阶非线性效应, $n_2$  为非线性折射率系数, $\omega_0$  为脉冲中心频率,c 为真空中的光速, $A_{\rm eff}$  为纤芯有效横截面积):第一项表示自相位调制效应;第二项表示自陡变效应( $\lambda_0$  为脉冲中心波长);第三项表示拉曼散射效应( $T_R$  为内脉冲拉曼散射系数,与拉曼增益的斜率有关,通常为 3 fs).

# 2 计算结果及分析

#### 2.1 传输常量及光场在锥区的分布

图 3 为波长为 850 nm 时,传输常量沿拉锥方向

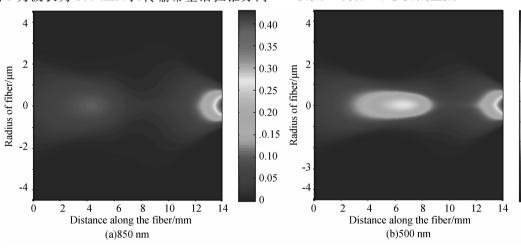


图 4 波长为 850 nm 和 500 nm 时光场分布

Fig. 4 The evolution of the radial distribution of intensity along the tapered fiber at 850 nm and 550 nm

#### 2.2 有效横截面积及色散参量在锥区的变化情况

纤芯有效横截面积  $A_{\text{eff}}$  定义为  $A_{\text{eff}}$  =

$$\frac{(\int_{-\infty}^{\infty} |R(x,y)|^2 dx dy)^2}{\int_{-\infty}^{\infty} |R(x,y)|^4 dx dy}, 式中 R(x,y) 可由式(3)和(4)$$

求出. 这样,即可求出锥形光纤锥区纤芯有效横截面积沿传输方向的变化情况,如图 5. 在拉锥初始阶段,  $A_{\rm eff}$ 从初始值 38  $\mu$ m² 不断减小;在"转换点"附近时,减小到最低值 9  $\mu$ m²,之后迅速增大到最大值 46  $\mu$ m²;而在拉锥末端,又迅速减小至 2  $\mu$ m².

的变化情况. 由图可见,在拉锥前段, $\beta$  缓慢减小;当拉锥接近结束时, $\beta$  迅速减小.

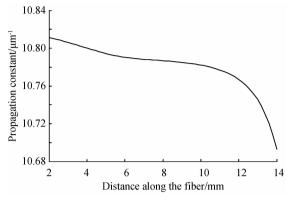


图 3 传输常量沿拉锥方向的变化

Fig. 3 Propagation constant along the tapered fiber

波长为 850 nm 和 500 nm 时光场的分布分别如图 4. 在锥区的前段,光波主要以纤芯模传播,大部分能量都集中在纤芯.由于此时纤芯半径较大,所以光强较弱.随着拉锥的进行,能量开始渗透到包层中,在纤芯和包层中重新分布,纤芯模也开始变成包层模.此时包层半径很大,所以光强很弱.在拉锥的末端,纤芯和包层的半径都很小,所以光强重新变得很大.光波模式从纤芯模变为包层模的点被称为"转换点",或者"纤芯模截止点"[17].

0.45

0.40

0.35

0.30

0.25

0.20

0.15

0.10

0.05

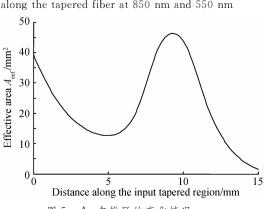


图 5 A<sub>eff</sub> 在锥区的变化情况

Fig. 5  $A_{\rm eff}$  along the tapered fiber

光纤色散参量  $D = \frac{\mathrm{d}\beta_1}{\mathrm{d}\lambda}$ ,又由  $\beta_1 = \frac{\mathrm{d}\beta}{\mathrm{d}w}$ ,得  $D = -\frac{\lambda}{2\pi\epsilon} \left(\frac{2\mathrm{d}\beta}{\mathrm{d}\lambda} + \lambda \frac{\mathrm{d}^2\beta}{\mathrm{d}\lambda^2}\right) \tag{10}$ 

图 6 为波长为 850 nm 的光波在锥形光纤锥区 传输时,色散参量 D 的变化情况. D 在"转换点"之

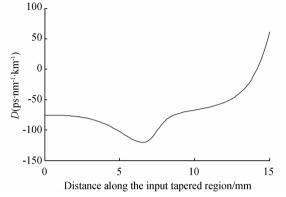


图 6 色散参量在锥区的变化情况 Fig. 6 D along the tapered fiber

前沿拉锥方向从 $-75 \text{ ps} \cdot \text{nm}^{-1} \cdot \text{km}^{-1}$ 逐渐减小至 "转换点"处的最小值 $-120 \text{ ps} \cdot \text{nm}^{-1} \cdot \text{km}^{-1}$ ,而后 迅速增大,在拉锥末端为 60 ps/nm/km.

#### 2.3 超短脉冲在锥区的传输演化

设抽运脉冲为双曲正割形,其中脉冲中心波长  $\lambda_0 = 850$  nm,脉冲峰值功率为  $P_{\text{scale}} = 500$  W,脉冲宽度  $T_{\text{FWHM}}$ 分别为 20 fs、30 fs、50 fs 和 80 fs. 非线性 折射率系数  $n_2 = 3.2 \times 10^{-20}$  m²/W,光纤损耗系数  $\alpha = 0.2$  dB/km. 又由文献[18]可知, $\beta_2 = -\frac{\lambda^2}{2\pi c}D$ ,  $\beta_k = \left(\frac{\mathrm{d}^k \beta}{\mathrm{d}\omega^k}\right)_{\omega = \omega_0}$ ,由此  $\beta_k$  可由算得的色散参量 D 求得. 对方程(9)进行分步傅里叶法[19]数值求解,可得超短脉冲在锥形光纤锥区的演化情况.

图 7 中当脉宽为 20 fs、30 fs、50 fs 时,随着脉冲在锥区的传输,脉宽有一定的展宽,初始脉宽越窄,展宽越明显. 由模拟计算可知,当脉宽大于 80 fs 时,脉冲的脉宽效应不明显.

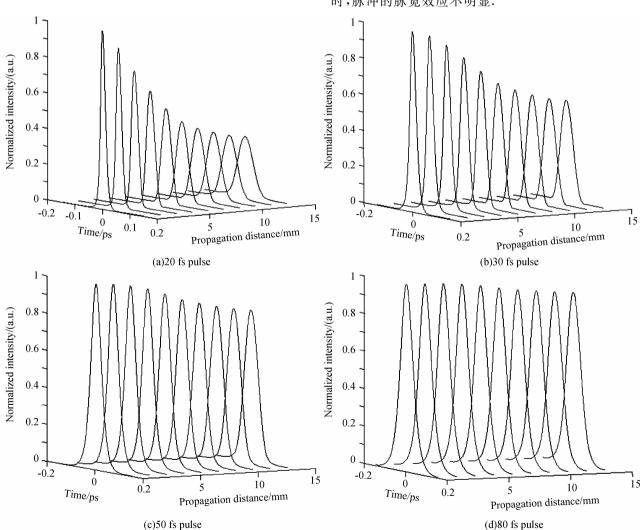


图 7 不同脉宽的脉冲在锥区传输的演化图

Fig. 7 Evolution of pulses with different pulse width in the tapered region

# 3 结论

本文考虑空气层,将锥形光纤锥区视为三层(纤芯、包层和空气层),计算出光波在锥区传输时传输常量和光强的变化情况.研究结果表明,传输常量沿传播方向不断减小,在"转换点"之后迅速减小;光场能量在"转换点"之前主要集中在纤芯中,"转换点"之后,能量在包层和纤芯中重新分布,靠近拉锥末端时,由于光纤半径很小,光强很大.脉宽为 20~50 fs 的脉冲沿锥区传输时,初始脉宽越小,脉冲的展宽越明显.

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# Optical Field Evolution and Transmission Characteristics of Ultra-short Pulse in the Tapered Region of a Single-mode Tapered Fiber

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Abstract: Propagation constant and field evolution in the tapered region are discussed using numerical method based on waveguide theory. GNSE is resolved by the split-step Fourier method to study the transmission characteristics of ultra-short pulse in the tapered region. The calculated results show that at the beginning of the tapered fiber, propagation constant decreases gradually while in the end it drops dramatically. After the "transition point", energy redistributes in the fiber, and it becomes very large in the end. It is found that pulse width is broadened along the tapered region when the pulse width is smaller than 80fs.

**Key words:** Guided wave and fiber optics; Propagation constant; Optical field propagation; Ultra-short pulse



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