

## 方形孔径的宏观傅里叶叠层超分辨成像研究

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**摘要** 随着成像系统小型化发展, 透镜和光阑不再必须是圆形的, 方形孔径更有利于收集微成像器件完整孔径的光场。研究了基于方形孔径的宏观傅里叶叠层成像技术, 利用成像传感器及其傅里叶域自然的矩形结构, 更有效利用方形孔径的合成来提高成像分辨率。数值模拟和实验验证表明: 边长和直径相等的方形孔径与圆形孔径相比, 方形孔径具有高通量和宽传递函数的优势, 可实现更高的成像分辨率、速度和信噪比。

**关键词** 显微; 傅里叶叠层; 合成孔径; 成像系统

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## 1 引言

远场光学超分辨成像在生物医学、化学、国防和航天航空领域有着广泛的应用需求。各种新颖的成像技术和方法已经在显微<sup>[1-8]</sup>/显纳等微观领域取得了丰硕的成果。然而, 针对宏观目标的光学超分辨成像的研究报道相对较少。傅里叶叠层衍射<sup>[9-10]</sup>(FP)是少有的微观(FPM)和宏观方面都实现了超分辨成像的技术之一。显微方面, 加州理工学院的 Zheng Guoan 和国内左超团队<sup>[11]</sup>、姚保利团队<sup>[12]</sup>、张福才团队<sup>[13]</sup>等在 FPM 方面取得了重要的研究成果, 并实现了商业化<sup>[14]</sup>。宏观方面, 美国西北大学 Holloway 等<sup>[15-16]</sup>提出了宏观傅里叶叠层成像方法, 并实现了 1.5 m 外反射式物体的长距离超分辨成像。国内汶德胜/宋宗玺团队<sup>[17-18]</sup>和赵明等<sup>[19]</sup>开发和改进该方法并将其用于宏观目标的超分辨成像。傅里叶叠层算法一个显著的缺点就是需要在傅里叶域完成  $N \times N$  的孔径扫描, 这一过程需要耗费大量时间, 并且随着数据量的增加, 对计算机性能的要求不断提升。为此, 清华大学曹良才团队<sup>[20]</sup>提出了一种基于稀疏孔径的长距离超分辨成像方法, 该方法只需在傅里叶域采集  $N$  个孔径就可以实现相当于  $N \times N$  的孔径扫描效果, 大大缩短了数据采集所耗费的时间, 降低了对计算机性能的要求。哈尔滨工业大学张永兵团队<sup>[21]</sup>将深度学习和超分辨成像方法相结合, 在改善成像分辨率的同时提高了复杂光学像差与相干噪声的鲁棒性。

FP 成像技术属于计算成像<sup>[22]</sup>的范畴, 虽然它在有限光学孔径下可以同时实现大视野和高(超)分辨, 但

是它和常规数字显微或望远系统一样, 存在一个基本矛盾——镜头和传感器在形状以及尺寸上不匹配。一般镜片为圆形结构, 而图像传感器如 CCD、CMOS 等为面阵结构, 两者在匹配时牺牲了镜头的视场。传统的光学透镜通过铣磨、精磨、抛光和研磨等机械加工工艺来生产, 这就决定了圆形孔径的透镜制备成本低且均匀性好。随着摄像头模组和光学镜头模组的小型化发展, 圆形透镜的必要性需要被重新考量, 比如手机摄像头(镜头)模组的基本构造包括镜头、镜座、传感芯片、电路板和连接器, 除了镜头外, 其余器件都是方形结构(镜座是方形底座连接圆形接口, 用于连接镜头)。艾迈斯半导体的集成式微型摄像头模块型号为 MCM-NanEyeM, 整个图像传感器的封装尺寸非常小, 仅  $1 \text{ mm} \times 1 \text{ mm} \times 2 \text{ mm}$ , 所有部件中, 也仅有镜片是圆形的, 其他均是方形结构。超透镜采用半导体行业的可扩展制造工艺制造, 其中电子束光刻为最核心的数字化制备步骤, 无论是电子束偏移系统还是工作台(一般是压电平移台)的扫描, 电子束刻蚀系统均是依赖于  $o-xy$  直角坐标系下的物理系统和驱动电路。显然, 随着微纳制备技术的发展, 光学成像系统的圆形孔径光阑和透镜不再是必要的, 相反, 它已经成为成像质量的限制之一。针对此限制, 席鹏团队<sup>[23]</sup>考虑了具有更大有效孔径的传感器对角化方法, 从而提高了显微成像系统的分辨率。本文通过分析方形孔径相干传递函数以及圆形孔径相干传递函数, 比较了恢复结果的图像强度、对比度和分辨率, 以此说明方形孔径在 FPM 中比圆形孔径更具有优势, 同时表明方形孔径在未来微型化摄像(镜头)的制备中有非常大的潜在应用价值。

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## 2 傅里叶叠层成像模型

与显微傅里叶叠层成像不同的是,宏观傅里叶叠层成像需要移动图像传感器或者使用阵列图像传感器来

获取物体的频域信息。在远场条件下,利用透镜对物体进行傅里叶变换,再使用图像传感器收集频域信息。

在满足夫琅禾费衍射的远场条件,透镜平面的光场是物光场的空间频谱分布  $U(x', y')$ , 其表达式为

$$U(x', y') = \frac{\exp(j\lambda d_0) \exp\left[j\frac{2\pi(x'^2 + y'^2)}{2\lambda d_0}\right]}{j\lambda d_0} \iint_{\infty} U_0(x_0, y_0) \exp\left[-j\frac{2\pi}{\lambda d_0}(x'x_0 + y'y_0)\right] dx_0 dy_0 = \frac{\exp(j\lambda d_0) \exp\left[j\frac{2\pi(x'^2 + y'^2)}{2\lambda d_0}\right]}{j\lambda d_0} \mathcal{F}_{\frac{1}{\lambda d_0}}[U_0(x_0, y_0)], \quad (1)$$

式中:  $\lambda$  表示为波长;  $U_0$  表示物光场;  $d_0$  为物距;  $(x_0, y_0)$  和  $(x', y')$  分别为物体平面和透镜平面的坐标;  $\mathcal{F}$  为傅里叶变换函数。

首先,在频谱面上使用孔径光阑进行频域扫描,图像传感器孔径光阑为  $B[x' - m'_x(i), y' - m'_y(i)]$ ,  $[m'_x(i), m'_y(i)]$  为当前光阑位置。因为孔径光阑的尺寸小于物体的频谱尺寸,所以孔径光阑对频域信息进行了截取。图像传感器在当前位置所获得的二维频域信息为  $U(x', y')B[x' - m'_x(i), y' - m'_y(i)]$ 。然后,利用成像镜头对频域信息进行傅里叶变换,由于图像传感器只能记录光场的强度信息,因此图像传感器所记录的强度信息为

$$I = \left| \mathcal{F}^{-1}\{U(x', y')B[x' - m'_x(i), y' - m'_y(i)]\} \right|^2, \quad (2)$$

式中:  $\mathcal{F}^{-1}$  表示傅里叶逆变换函数。式(2)为傅里叶叠层成像的数学形式,可以看出随着光阑孔径位置  $[m'_x(i), m'_y(i)]$  的变换,图像传感器将获取不同位置的频域信息,所记录的对应位置频域信息形成的图像为  $I$ 。

## 3 傅里叶合成孔径超分辨算法

合成孔径就是将不同位置孔径截取的频域信息通过算法合成来恢复完整的物体频域信息。图 1 为宏观傅里叶叠层光路示意图。

在恢复过程中,使用空域约束和频域约束两个条件来保证相位恢复的可解性。采用 PIE 算法进行更新

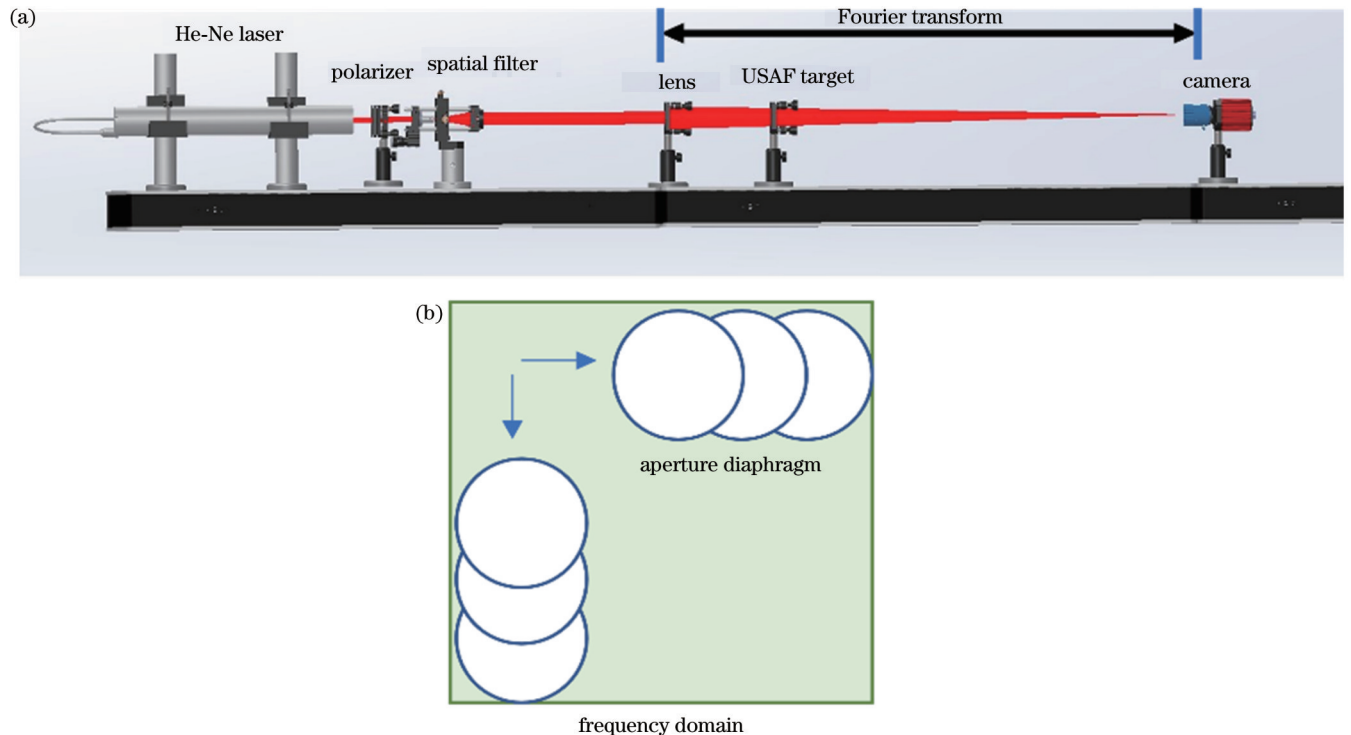


图 1 宏观傅里叶叠层成像示意图。(a)光路装置;(b)孔径光阑扫描

Fig. 1 Schematic for macroscopic Fourier ptychography imaging. (a) Lightpath and device; (b) aperture scanning

迭代恢复相位,获得由孔径合成的频谱,再将合成频谱进行傅里叶逆变换获得高分辨率图像。图 2 给出了算

法恢复的过程,恢复步骤如下。

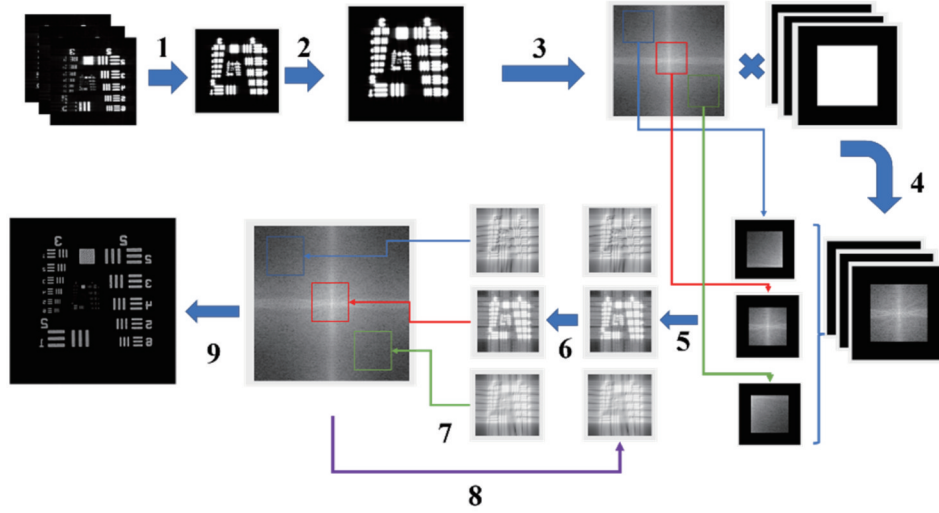


图 2 宏观傅里叶叠层成像重建流程图

Fig. 2 Flowchart of reconstruction process of Fourier ptychography imaging

1) 由图像阵列进行均值处理获得空域的初始猜想;

2) 根据孔径重叠率,使用双线性插值法进行分辨率拉伸;

3) 将分辨率拉伸后的图像进行傅里叶变换,成为初始猜想  $U_0'(x', y')$ ;

4) 将当前位置的光阑函数与物体的频谱相乘,光阑函数所截断的频域信息为  $\varphi_i'(x', y') = U_0'(x', y')B[x' - m_x'(i), y' - m_y'(i)]$ ;

5) 将截断的频域信息进行傅里叶逆变换到空域  $\phi_i^k = \mathcal{F}^{-1}\varphi_i'(x', y')$ ;

6) 将变换到空域的图像信息进行迭代运算  $\phi_i^k = \sqrt{\frac{I_i}{|\phi_i^k|^2}} \phi_i^k$ ;

7) 根据第  $i$  个扫描位置更新的低分辨率频谱更新高分辨率中对应位置的频谱信息;

8) 返回步骤 6) 进行迭代运算,通过最小二乘法进行约束,即

$$\hat{\phi}^{k+1} \leftarrow \min_{\phi} \sum_{i=0}^n \|\phi_i^k - \mathcal{F}^{-1}\varphi_i'(x', y')\|_2^2 + \tau \|\hat{\phi}\|_2^2; \quad (3)$$

9) 将迭代运算完成的合成频谱信息进行傅里叶逆变换,获得高分辨率图像。

## 4 宏观傅里叶叠层实验

### 4.1 实验设计

搭建了宏观傅里叶叠层成像系统(图 3),对所提理论的可行性进行验证。首先,由激光器产生相干光,通过空间滤波器进行滤波;然后,通过透镜的相位变换

因子来抵消菲涅耳衍射传播中的二次相位因子,以保证物体的光场到相机镜头之间满足傅里叶变换关系;最后,使用放置在高精度位移台上的孔径光阑以及图像传感器在二维傅里叶平面进行采样,获得目标物体的低分辨率图像信息。

实验仪器如图 4 所示。将波长  $\lambda = 632.8 \text{ nm}$  的激光器作为光源,在光源前方放置偏光片,以降低光源强度。使用空间滤波器对相干光滤波。分辨率靶到可调光阑的距离为  $0.5 \text{ m}$ ,透镜的焦距为  $200 \text{ m}$ ,聚焦透镜为  $80 \text{ mm}$  的长步道镜头,镜头前为可调光阑,将光阑孔径大小设置为  $5 \text{ mm}$ ,采集相机为巴斯勒 CCD 相机(acA2040-90  $\mu\text{m}$ ),像元大小为  $3.75 \mu\text{m}$ ,放置在高精度三维位移台上,使用的目标为美国空军分辨率板(USAF),直径为  $21 \text{ mm}$ 。

### 4.2 实验过程与实验数据

将圆形光阑直径调制为  $5 \text{ mm}$ ,根据  $80\%$  的重叠率,将移动步长设置为  $1 \text{ mm}$ 。在二维空间中,在水平和垂直两个方向一共设置了  $49$  个位置进行采样。在当前位置采集完毕获得低分辨率图像之后,根据步长需求移至下一位置采集图像,直至图像采集完毕。再将方形光阑边长调制为  $5 \text{ mm}$  并将其替换圆形光阑重复上述过程,采集的数据如图 4 所示。由于实验是基于宏观光路进行的,因此采用圆形透镜加方形光阑来模拟方形透镜会更加方便。

在传统显微领域的 FPM 系统中,只是通过点亮不同位置的 LED 来改变入射角度,实现频谱的搬移。在这种方法下,目标物体与图像传感器没有发生位置的相对变化。而对于宏观傅里叶叠层扫描来说,因为光源无法大幅度调节入射角度,若要实现频域扫描就得改变图像传感器的位置。随着相机位置的变化,每次

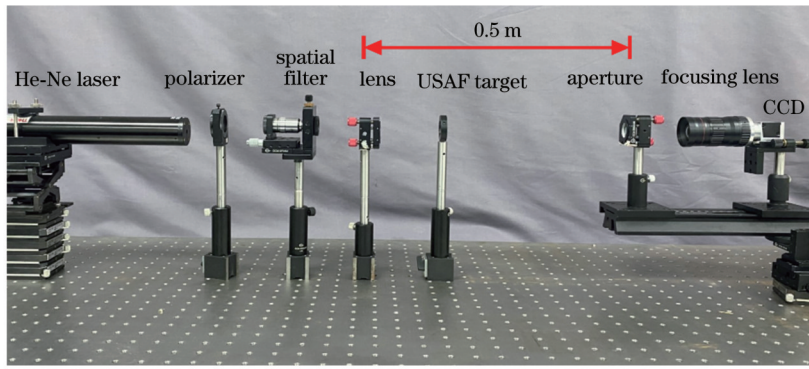


图3 宏观傅里叶叠层成像实验装置

Fig. 3 Experimental setup for Fourier ptychography imaging

采集频域信息时视场都会随之改变。

关的模板匹配法进行图像配准。互相关系数的计算公

为了克服视场变化所带来的影响,使用基于互相

式为

$$\gamma(\mu, \nu) = \frac{\sum_{x,y} [f(x,y) - \bar{f}_{\mu,\nu}] [t(x-\mu, y-\nu) - \bar{t}]}{\left\{ \sum_{x,y} [f(x,y) - \bar{f}_{\mu,\nu}]^2 \sum_{x,y} [t(x-\mu, y-\nu) - \bar{t}]^2 \right\}^{0.5}}, \quad (4)$$

式中:  $f$  为图像;  $\bar{t}$  为模板的平均值;  $\bar{f}_{\mu,\nu}$  为模板下区域的平均值。图像配准后, 将目标所成的像从原始图像中

剪裁出来, 再根据扫描顺序进行排列形成原始图像阵列。

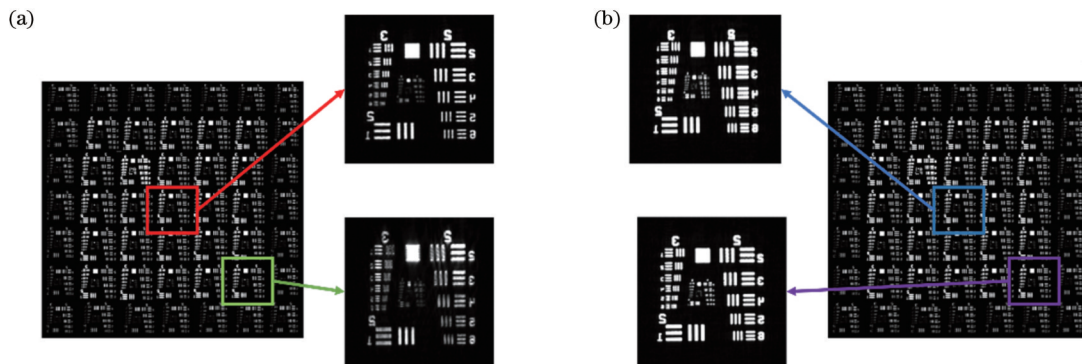


图4 USAF 分辨率靶对应的傅里叶叠层数据集。(a)利用圆形孔径采集;(b)利用方形孔径采集

Fig. 4 Fourier ptychography datasets for USAF target collected by different apertures. (a) Collected by circular aperture; (b) collected by square aperture

为了比较方形孔径采集与圆形孔径采集的区别, 挑选出同一位置采集的图像进行局部分析。图5中给出了相同频域位置下, 使用圆形孔径截取的信息和使用方形孔径截取的信息。

从图5(d)、(e)可以看出, 在(2,5)组与(2,6)组中, 由方形孔径采集的图像中依旧有灰度值为255的像素点, 而由圆形孔径采集的图像中, 因光通量不足, 没有灰度值为255的像素点。由此可见, 在提升图像强度这一方面, 方形孔径有显著的优势。

### 4.3 重建结果与分析

利用傅里叶叠层迭代算法对圆形孔径数据集和方形孔径数据集进行重建, 重建结果如图6所示。

将重建结果分辨率靶的(2,4)组(线宽为

88.39  $\mu\text{m}$ , 线对密度为 5.66  $\text{lp}\cdot\text{mm}^{-1}$ )、(3,5)组(线宽为 39.37  $\mu\text{m}$ , 线对密度为 12.7  $\text{lp}\cdot\text{mm}^{-1}$ )、(4,1)组(线宽为 31.25  $\mu\text{m}$ , 线对密度为 16  $\text{lp}\cdot\text{mm}^{-1}$ )进行对比。为了方便比较, 将基准线灰度图像绘出如图7所示。从宏观角度进行分析, 方形孔径恢复出的图像强度强于圆形孔径的图像强度。根据对比度公式, 有

$$C = \frac{\bar{w} - \bar{b}}{\bar{w} + \bar{b}}, \quad (5)$$

式中:  $C$  为对比度;  $\bar{w}$  为亮区像素点的平均灰度值;  $\bar{b}$  为暗区像素点的平均灰度值。在(4,1)组的情况下, 方形孔径依旧有0.4的良好对比度, 而圆形孔径的对比度几乎为零。

关于不同几何形状的孔径对于叠层成像恢复质量

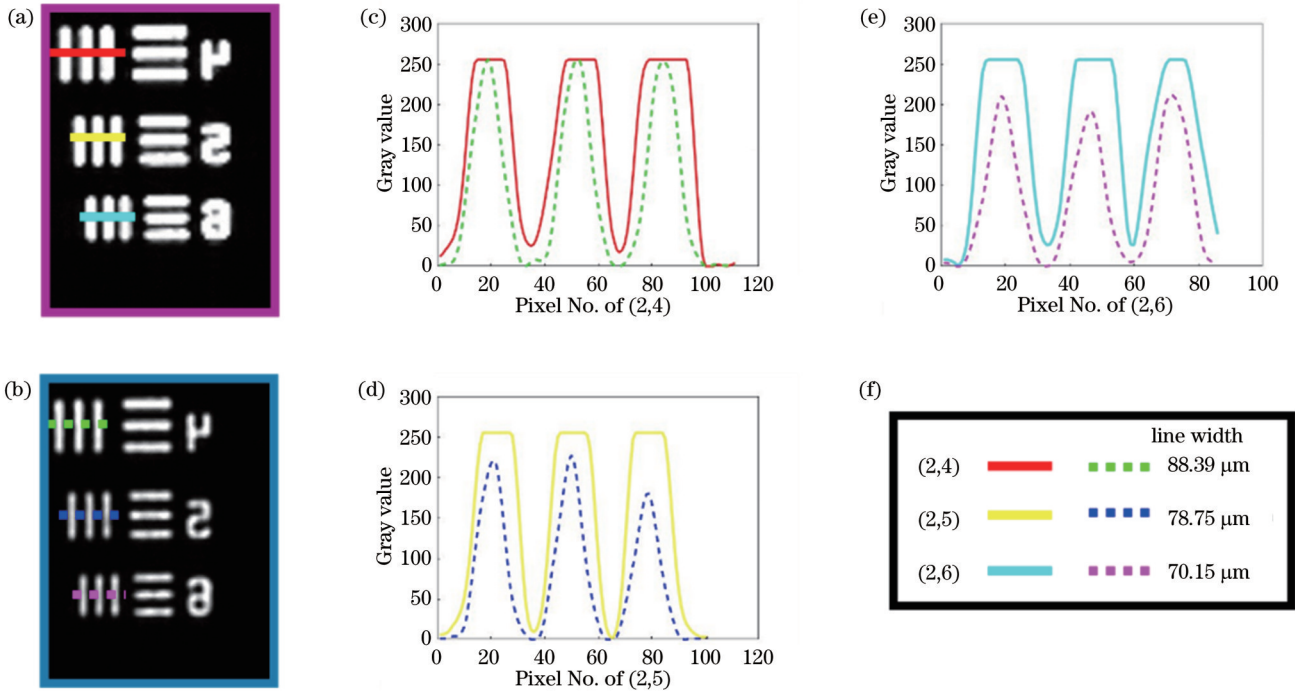


图 5 USAF 分辨率板细节图。(a)使用方形孔径截取图像信息的局部图像;(b)使用圆形孔径截取图像信息的局部图像;(c)线宽为 88.39  $\mu\text{m}$  的灰度图像;(d)线宽为 78.75  $\mu\text{m}$  的灰度图像;(e)线宽为 70.15  $\mu\text{m}$  的灰度图像;(f)线宽示意图  
 Fig. 5 USAF resolution board details. (a) Fourier Ptychography details collected by circular aperture; (b) Fourier Ptychography details collected by square aperture; (c) gray image with line width of 88.39  $\mu\text{m}$ ; (d) gray image with line width of 78.75  $\mu\text{m}$ ; (e) gray image with line width of 70.15  $\mu\text{m}$ ; (f) schematic of line width

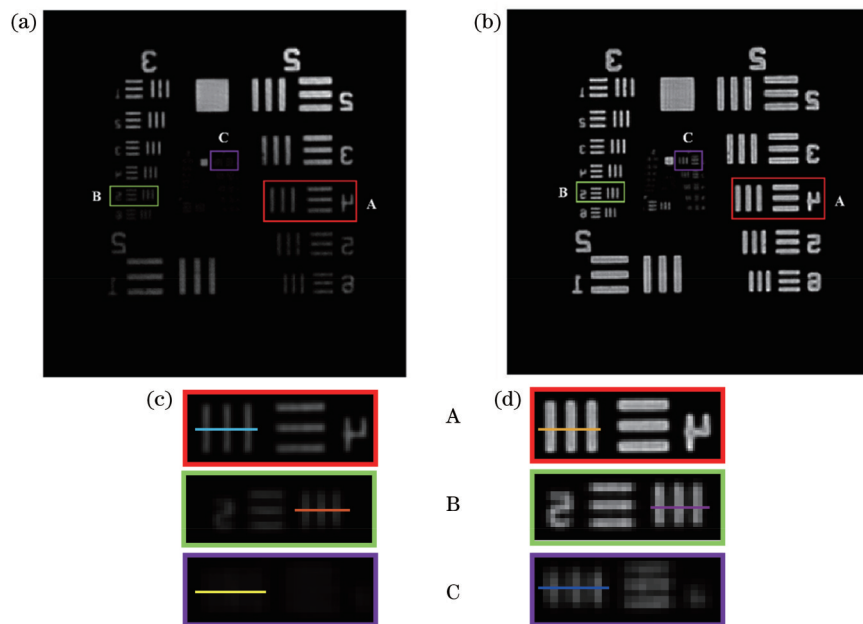


图 6 USAF 分辨率重建结果。(a)基于圆形孔径的重建结果;(b)基于方形孔径的重建结果;(c)图 6(a)的局部放大图;(d)图 6(b)的局部放大图  
 Fig. 6 Reconstruction results for USAF target. (a) Reconstruction results based on circular aperture; (b) reconstruction results based on square aperture; (c) partial enlargement of Fig. 6(a); (d) partial enlargement of Fig. 6(b)

的影响,史伟诗教授团队<sup>[24]</sup>比较了圆形孔径、六边形孔径和方形孔径的夫琅禾费衍射图样,发现信息度由低频到高频时,方形孔径保留的远场衍射信息度低于圆

形孔径和六边形孔径,因此在算法中影响了最优解收敛的速度,由此得出方形孔径在空域的控制波前的效果不如圆形孔径的结论。而本文的孔径限制是在傅里

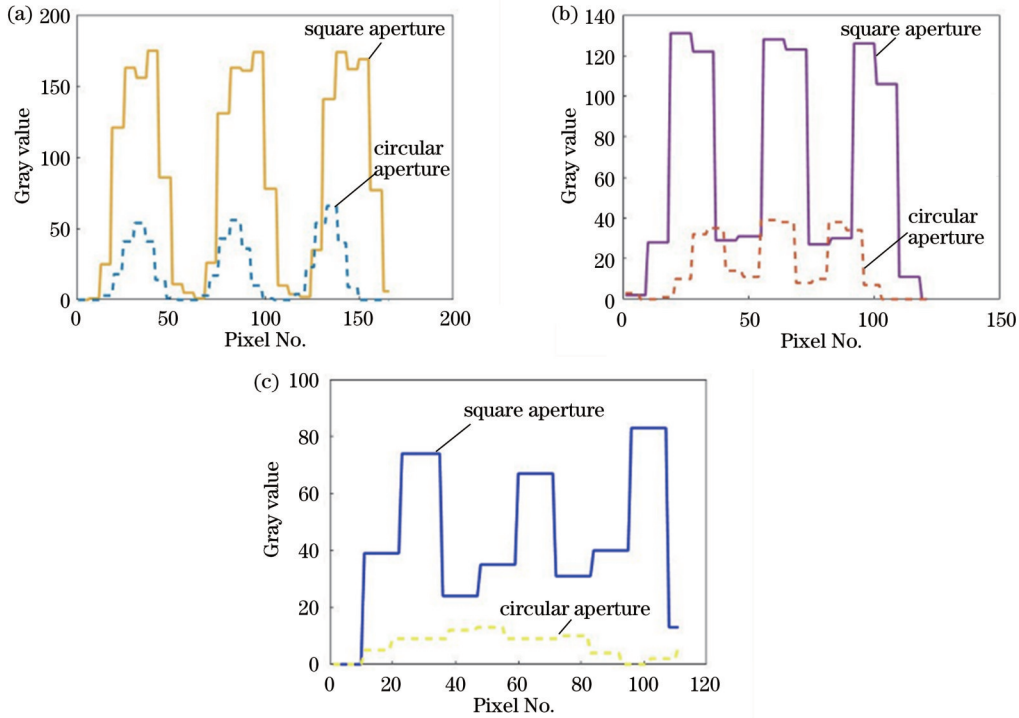


图 7 基准线上的灰度图像对比。(a)线宽为 88.39 μm 的灰度图像对比; (b)线宽为 39.37 μm 的灰度图像对比; (c)线宽为 31.25 μm 的灰度图像对比

Fig. 7 Comparison of gray images on baseline. (a) Comparison of gray images with 88.39 μm line width; (b) comparison of gray images with 39.37 μm line width; (c) comparison of gray images with 31.25 μm line width

叶频域面,由于方形孔径面积大于圆形孔径,所以在傅里叶频域信息截取时,方形孔径能够保留更多的频域信息且在采样时光通量也有所提升。

一个直径为  $D$  的圆形光瞳,其孔径函数  $P(x, y)$  可表示为

$$P(x, y) = \text{circ}\left(\frac{\sqrt{x^2 + y^2}}{D/2}\right), \quad (6)$$

其相干传递函数为

$$H(\xi, \eta) = P(\lambda d_i \xi, \lambda d_i \eta) = \text{circ}\left[\frac{\sqrt{\xi^2 + \eta^2}}{D/(2\lambda d_i)}\right]. \quad (7)$$

由圆柱函数的定义可知:在小于  $\frac{D}{2\lambda d_i}$  频率范围内

$H(\xi, \eta) = 1$ ; 在大于  $\frac{D}{2\lambda d_i}$  频率范围,  $H(\xi, \eta) = 0$ 。故

截止频率为  $\rho_c = \frac{D}{2\lambda d_i}$ 。

对于边长为  $a$  的正方形,其光瞳函数为

$$P(x, y) = \text{rect}\left(\frac{x}{a}\right)\text{rect}\left(\frac{y}{a}\right), \quad (8)$$

相干传递函数为

$$H(\xi, \eta) = P(\lambda d_i \xi, \lambda d_i \eta) = \text{rect}\left(\frac{\lambda d_i \xi}{a}\right)\text{rect}\left(\frac{\lambda d_i \eta}{a}\right). \quad (9)$$

由式(9)可知,不同方位上的截止频率不相同,当

等相位线与  $x$  轴成  $45^\circ$  角时,系统的截止频率最大,此时  $\xi = \eta$ , 此方向的截止频率  $\rho_c = \frac{\sqrt{2} a}{2\lambda d_i}$ 。此时与  $x$  轴成  $45^\circ$  角的方形孔径的截止频率大于圆形孔径。同时由于方形孔径的光通量提升,进一步提高了参与傅里叶叠层超分辨算法的低分辨率图像阵列的图像强度,最终使恢复结果图像强度得到了提升。可以利用方形孔径的优势来减少数据集的动态范围,从而缩短图像采集的时间。原数据采用了 300、500、700、900、1500 μs 曝光时间,减少 500 μs 和 700 μs 两组曝光时间后恢复结果如图 8 所示。

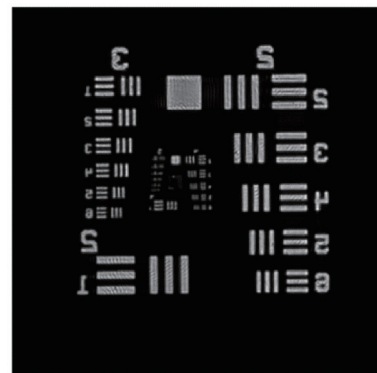


图 8 小动态范围下的方形孔径恢复图像  
Fig. 8 Square aperture restoration image in small dynamic range

使用方形孔径来代替圆形孔径进行数据采集不仅减少了数据采集的工作量,且恢复结果依旧拥有良好的分辨率。当孔径光阑从圆形换成方形,由于光阑所在平面(理想情况下与透镜同一平面)为物场的空间频谱面,方形光阑相比于圆形光阑具有更大的孔径面积,因此能收集更高频谱的光场。当采用圆形孔径时,CCD 对角线方向可以获取最高的频域信息。席鹏团队<sup>[23]</sup>便是利用这一原理,旋转传感器进行多次采样和对角拼合,从而获得约 1.4 倍的分辨率提升。当孔径光阑从圆形换成方形时,无需旋转采样和拼合,方形 CCD 能自然获取方形孔径的最高频谱信息。

## 5 结 论

随着微小成像系统的迅速发展,依靠牺牲镜头的视场来完成与图像传感器匹配的方法已经不能满足既要集成设备,又要保证良好的成像质量的密集式微型成像系统的要求。在透镜的微纳制备技术中,透镜和孔径光阑的制备不仅局限于圆形,方形孔径光阑和透镜可以更好地解决其与图像传感器匹配方面存在的问题,且具有更大的有效孔径来确保成像质量。

傅里叶叠层技术在显微成像领域发展成熟之后,被推广到远场光学超分辨成像领域,但在傅里叶频域面采集数据时依旧是使用圆形孔径。为了提高信息的采集程度和提升图像分辨率,利用方形孔径的更大有效孔径优势在傅里叶频域截取信息。以此为出发点,本文开展了基于不同孔径扫描的宏观傅里叶叠层实验,搭建了光学系统,对比了基于方形孔径扫描的宏观傅里叶叠层结果和基于圆形孔径扫描的宏观傅里叶叠层结果,发现基于方形孔径扫描的宏观傅里叶叠层结果具有更好的对比度,且因为方形孔径在傅里叶域能够截取更多的信息,最后恢复出的图像分辨率略大于圆形孔径扫描的图像。同时利用光通量的增加,可以减少采集图像的动态范围,进而减少图像采集时间。上述实验说明了方形孔径在宏观傅里叶叠层实验中比圆形孔径更具优势。

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## Fourier Ptychography Super-Resolution Imaging Based on Square Aperture

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### Abstract

**Objective** Fourier ptychography (FP) is a recently developed phase retrieval approach, which simultaneously realizes image restoration with super-resolution and a large field of view. This approach is also a novel super-resolution optical imaging technique that can be efficiently applied to microscopy and macroscopy respectively. However, one limitation of FP is the long acquisition and reconstruction time due to the numerous low-resolution (LR) images that are needed. Especially when the LR image is acquired under large angle illumination (dark field imaging), the low illumination intensity leads to the long exposure time of the imaging sensors. The situation becomes more time-consuming when a new sample is imaged, and thus a larger number of images with different exposure time for each LR image should be tested to obtain the corresponding best exposure time. Losing low gray value pixels exists in the FP algorithm preprocessing, which ultimately leads to the loss of image information due to the weak local image intensity in the recovery result. With the development of optical integration and micro/nano fabrication technology, the circular lens is no longer necessary. On the contrary, the square lens can fill the entire aperture of the miniaturized imaging system (cuboid) and collect more light fields. This paper introduces the square aperture lens into the FP approach which is conducive to collecting the complete aperture light field for further miniaturized imaging devices. The introduced square lens is expected to improve the image intensity and resolution of the FP approach, reduce the data acquisition time, and be more in line with the optical integration development.

**Methods** According to the Rayleigh criterion, the low resolution of the optical imaging system is caused by the lens aperture. The FP approach achieves super-resolution and large-field imaging by combining multiple LR images. Different from the FP microscopy, the macroscopic FP technique requires moving the imaging camera or using array imaging cameras to obtain a series of LR images of the object. Each LR image is obtained by locating the aperture on the spatial spectrum plane with different positions set in horizontal and vertical directions. After the LR image is acquired at the current position, the aperture is moved to the next position according to the required step size until the spatial spectrum is fully collected. To overcome the position offset of each LR image, the template matching method based on cross-correlation is applied for image registration. This paper studies the macroscopic FP imaging technology based on square aperture. Using the imaging sensor and its natural rectangular structure in the spatial Fourier domain is more effective to use the synthesis of square aperture to improve the imaging resolution and reduce the time consumption. The macroscopic FP technology based on circular aperture is also tested to make a better comparison. In the simulation, the ptychographical iterative engine (PIE) algorithm on the MATLAB platform is adopted to iteratively recover the phase to obtain a high-resolution image. In the experiment, a macroscopic FP optical setup is built. A square aperture, a lens, and a CCD are mounted on an optical bench as a comment imaging system. The system translated in the  $x$ - $y$  direction to collect different spatial spectra and obtain a series of LR images. The PIE algorithm used in the simulation can recover the super-resolution image from the LR images.

**Results and Discussions** When the circular aperture is used in the FP method, the image intensity is too weak as luminous flux lacks. The low gray value pixels would be missed during the FP algorithm preprocessing, which ultimately leads to image information loss due to the weak local image intensity in the recovery result. Compared to the circular



aperture, the square aperture has a greater luminous flux and can obtain higher image intensity when collecting image information in the spatial spectrum plane. In theory, it is well known that when the side length of the square aperture is the same as the diameter of the circular aperture, the coherence transfer function of the former is greater than that of the circular aperture. This means that the square aperture can collect more spatial frequency information in the spatial spectrum domain for each LR image. The experimental results show that the square aperture still has a good contrast of 0.4 in the case of groups (4, 1) in the USAF target (Fig. 6). The high luminous flux of the square aperture is utilized to reduce the dynamic range of the data set, therefore reducing the image acquisition time. The small dynamic range recovery results are shown in Fig. 8, and the image still has good contrast.

**Conclusions** This study demonstrates the macroscopic FP technique based on square aperture. The macroscopic FP technique has a better performance by replacing the conventional circular aperture scanning on the spatial spectrum plane with a square aperture. The numerical simulation and experimental verification show that when the square side length and circular diameter are the same, the square aperture has the advantages of high luminous flux and wide optical transfer function compared with the circular aperture. The wider spectrum of each LR image can increase the overlapping information between two adjacent images. The increase in luminous flux can reduce the dynamic range of image acquisition, thereby reducing the image acquisition time. As a result, the FP technique with the square aperture can achieve higher imaging resolution, speed, and signal-to-noise ratio. With the development of optical integration and micro/nano optical fabrication, the fabrication and integration of square aperture lens will be more convenient and can make full use of the aperture of the optical integrated devices. Considering the imaging sensor and its natural rectangular structure both in spatial and Fourier domains, the square aperture is more matched than the circular aperture. Square aperture lenses are promising to be integrated into various imaging systems and will appear in future miniaturized optical devices.

**Key words** microscopy; Fourier ptychography; synthetic aperture; imaging system