

超冷原子冷却用集成全光纤1064 nm 激光系统的 研制

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摘要 深度冷却是超冷原子制备过程的关键步骤,是探寻极低温度的关键技术。详细阐述了一种用于^{sr}Rb原子深度冷却的集成化全光纤1064 nm激光系统的研制方案。激光器采用两级主振荡功率放大的方案,将单一种子源信号进行放大、分束和调控,输出4路具备独立控制的激光,作为制备超冷量子气体的交叉光阱的光源。经测试,激光器在功率、稳定性、噪声等各方面满足原子深度冷却的实验需求。在地面条件下进行的两级深度冷却预实验中,获得了10 nK以下的初步实验结果,这验证了激光器具备实现超冷原子深度冷却所需的全部功能。激光器集成了种子源、放大器和全功能光学平台的功能,其内部模块采用全光纤器件研制,具有集成化、数字化、高稳定、免调试、易维护等优点,经过简易改造能够应用于远程遥控和遥测的超冷原子项目中。

关键词 激光光学;激光囚禁;玻色-爱因斯坦凝聚体;光纤激光器;激光冷却 中图分类号 O515 **文献标志码** A

1引言

超低温一直是物理研究与技术发展的关键目标与 驱动力。1985年激光冷却技术的发明将稀薄原子气体 的温度极限推进到了μK量级^[1-5],为人类带来了冷原子 干涉仪^[6-8]等精密测量仪器。1995年的蒸发冷却实验成 功实现了nK量级的冷却温度,更是开拓了对玻色-爱因 斯坦凝聚体(BEC)^[9-12]和简并费米气体(DFG)^[13-14]的实 验研究,进一步实现了用于研究复杂量子多体问题的 光晶格量子模拟^[15-20]。

为了排除重力的影响、更进一步获得低于1nK的 超低温,科学家们相继提出了Quantus落塔^[21]、抛物线 飞机^[22]、MAIUS声速火箭^[23-24]和冷原子实验室(CAL) 国际空间站载荷^[25]等微重力实验方案,并利用小型化原 子芯片等装置实现了动能等效温度小于1nK的超冷原 子气体。2021年,Rasel小组^[26]利用BEC四极振荡模将 一维动量转移至其他两个维度上,并利用脉冲冲击冷 却(DKC)的方法冷却剩下两个维度,创造了等效温度 低于38pK的超低温极限。2022年,Gaaloul等^[27]同样 利用DKC的方法在轨获得了50pK的超低温样本。

为了与微重力设备兼容,上述实验方案大部分采 用小型化的原子芯片,利用磁透镜DKC进行深度冷 却。2013年陈徐宗小组^[28]提出了一个应用于微重力 条件下基于全光方法进行深度冷却的实验方案。该方 案采用两对1064 nm 远失谐光阱(FORT),相继进行 蒸发冷却和绝热膨胀冷却,通过直接蒙特卡罗模拟算 法计算得出在微重力环境中可以获得低于100 pK 的 超冷原子气体的结论。相比于 DKC,这种两级冷却 (TSC)方法能够避免阱频率各向异性导致的冷却效 率的降低,从而实现更低的冷却温度,因此更具有应用 潜力^[29-30]。通过磁托举方法,2018年 Luan 等^[30]对⁸⁷Rb 原子进行了地面模拟微重力实验,获得了温度低达 3 nK 的⁸⁷Rb BEC。

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空间超冷原子物理实验采用上述 TSC 实验方案 作为超低温冷原子制备的关键技术路线,并基于此进 行了如下改进:增大光阱光功率动态范围和关断比,进 一步降低冷却温度;采用4路独立控制的光阱激光,避 免单路激光复用导致的光功率不平衡等问题;系统具 备集成化、小型化、高可靠性特性,满足实验设备工程 化需求。

为了实现在轨全光深度冷却,在前期工作^[31-34]的基础上,开发了一套集成化全光纤1064 nm光阱激光系统。激光器内部集成了种子源、光功率开关以及放大、调控、闭环反馈等功能,激光器与物理系统通过光纤进行连接,提供满足TSC冷却实验需要的4路交叉光阱激光。相比于常规地面实验室常见的FORT光路设

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计^[35-36], 全光纤链路具有高稳定、免调试、易维护等优 点, 充分满足空间站等远程遥控项目的应用需求。本 文描述了激光器的光学设计, 通过指标分解及实验验 证, 提供了一套标准的设计实施流程, 以为后续工作提 供借鉴和参考。

2 理论分析

TSC方案采用不同功率的两对1064 nm 连续光构 成阱深和阱体积各不相同的FORT,按照光腰大小可 将光阱分为细腰光阱和粗腰光阱。对于束腰 w 相同、 传播方向垂直的一对高斯光束构成的光阱,其势阱空 间分布为

$$U(x, y, z) = -U_z \exp\left[-\frac{2(x^2 + y^2)}{w^2}\right] - U_x \exp\left[-\frac{2(y^2 + z^2)}{w^2}\right], \qquad (1)$$

式中: U_z 和 U_x 分别是沿z和x方向传播的光阱深度; $U_{z(x)} = \frac{3\pi c^2 P_{z(x)}}{2\omega_0^3 w^2} \left(\frac{\Gamma_{\text{nature}}}{\omega_0 - \omega_{\text{laser}}} \right), P_{z(x)}$ 为沿z(x)方向传播 的光阱的光功率, c为真空光速, Γ_{nature} 为原子上能级自 然线宽, ω_0 为共振跃迁频率, ω_{laser} 为光阱工作频率。

根据目前的实验参数,细腰光阱阱深需要在 500 μK~100 nK范围内连续可调,而粗腰光阱阱深要 求覆盖1 nK~100 nK范围,对应的两类光阱的功率不 小于5 W和100 mW,要求关断比不小于60 dB和 40 dB。

两级冷却期间,光阱的功率波动会导致加热,基于 参量激发理论对激光器相对功率稳定度ε₀进行 估计^[37]:

$$\boldsymbol{\varepsilon}_{0} = \sqrt{\int_{0}^{\infty} \mathrm{d}\boldsymbol{v}_{\mathrm{trap}} S_{\epsilon}(2\boldsymbol{v}_{\mathrm{trap}})} = \sqrt{\int_{v_{\mathrm{trap}}}^{v_{\mathrm{upper}}} \mathrm{d}\boldsymbol{v}_{\mathrm{trap}} \frac{1}{T_{1} \pi^{2} \boldsymbol{v}_{\mathrm{trap}}^{2}}, (2)$$

式中: $S_{\epsilon}(2v_{trap})$ 为阱频率 v_{trap} 的2倍处的噪声功率谱密度; T_1 是预期的原子寿命(加热率的倒数); v_{lower} 和 v_{upper} 分别为二倍阱频率的上下限,由相应的实验光阱阱频率范围决定。假设原子寿命 $T_1 \ge 100$ s,相应的满功率下细腰、粗腰光阱光功率稳定度静态指标分别为 $\epsilon_{0, trin} \le 2.5 \times 10^{-3}$ 和 $\epsilon_{0, wide} \le 2.13 \times 10^{-2}$ 。当光阱光功率反馈带宽大于冷却阶段的功率扫描采样频率时,可以将每个采样点视为一段静态过程,由此可以将满功率下光阱光的静态光功率稳定性指标视为两级冷却期间的动态指标。

此外,航天工程对集成化、小型化、数字化具有较高要求,商用激光器难以满足。结合上述实验要求,研制了一套用于超冷原子深度冷却的集成化全光纤1064 nm激光器。

3 激光系统光学设计

3.1 激光系统模块设计

总体上,激光器采用分束放大的方案,即采用"前 级放大器+分束+功率控制+后级放大器"对单一种 子源进行多路高功率放大与大动态范围控制,使其满 足原子冷却实验的需求。种子源选用具有连续输出能 力的单模窄线宽1064 nm激光管。光功率放大器采用 光纤主振荡功率放大(MOPA)方案。光功率控制采 用光纤耦合声光调制器(AOM)。

激光系统由全保偏光纤器件组成,光纤链路如图 1所示,依照功能可分为高质量种子源(图1左侧部分) 和高功率放大(图1右侧部分)等两大模块。单一光源



图 1 1064 nm 激光器光学原理设计图 Fig. 1 Optical principle design of 1064 nm laser

小信号种子光经MOPA器件、光纤分束器、光纤AOM 等产生CH1~CH4这4路功率可调谐的1064 nm 远失 谐光阱激光。其中CH1、CH2作为高功率细腰光阱 光,CH3、CH4作为低功率粗腰光阱光。

高质量种子源模块用于产生后续光学系统所需的 稳定可靠的光源,包含种子源、高增益预放大器(PA) 和光纤分束器三个部分。其中,种子源(PL-DFB-1064-A1,LD-PD公司)输出中心波长为1064 nm、功 率为50 mW的种子光。PA对小信号种子光进行高增 益光功率放大,实现大于2 W的高稳定闭环反馈输出。 PA输出信号经过两级分束,产生功率比满足3:3:2:2 的4路支路信号,其中前两路作为细腰光阱光源,后两 路作为粗腰光阱光源。

高功率放大模块起到放大、功率控制和监测的作用,使得输出信号在功率、动态范围和稳定性等方面均能满足实验需求。高功率放大模块包含功率控制级和 功率监测级两个组成部分。根据输出需求的不同,每 一路的功率控制级设计方案也略有差异。4路光阱光 均采用光纤 AOM 进行功率控制,同时对成对信号引 入了160 MHz的频率差,以避免光阱交叠处产生的干 涉条纹对原子的加热(光阱的阱频率一般在kHz量级, 远低于160 MHz)。特别地,在CH1、CH2支路 AOM 后再插入一级高功率主放大器(BO),以实现细腰光阱 光大于5W的输出需求。为了满足输出功率的稳定性 要求,在各路激光输出前,利用高分束比的分光器对输 出功率进行采样,采用 PD 进行功率监测,并将功率采

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样信号通过伺服系统反馈至AOM射频源或BO泵浦 电流驱动上,实现输出光功率的闭环反馈控制。

3.2 光纤放大器设计

MOPA 器件选用发射波段为 1000~1100 nm 的掺 镱光纤(YDF)作为增益介质,同时选用 976 nm 光栅锁 波长 LD 对 YDF 进行包层正向泵浦。如此选择的原 因是:1)增益光纤对 976 nm 光波具有最大的吸收系 数,能减短 YDF,抑制受激布里渊散射(SBS)阈值,提 高输出功率;2)泵浦光波长锁定能够有效避免敏感波 段波长抖动,导致泵浦效率的降低,提高输出稳定性; 3)正向泵浦具有较小的噪声系数,能够有效提高输出 光束的信噪比。

对于高功率光路 CH1、CH2,采用两级 MOPA 方 案,通过 PA 与 BO 的配合,缩短单级增益光纤长度,提 高 SBS 阈值,抑制其对输出线宽的影响,通过中间级 滤波等处理,减少自发辐射放大(ASE)噪声在链路中 传播,提高输出信号的信噪比和光谱纯度。

PA与BO两类放大器结构如图2所示,均采用了 单级MOPA方案。信号通过分束器后,进行功率监 测,将其反馈到泵浦LD供电控制上,避免放大器空载 导致损坏。随后,利用功率耦合器(PC)将信号光与泵 浦光进行合束,一同输入YDF进行饱和增益放大。放 大后,利用包层泵浦除去器(CPS)上涂敷的高折射率 包层材料,除去残余在包层中的高功率泵浦信号,进而 提高输出光谱纯度。最后通过光纤光隔离器(ISO)隔 离回波,避免自激振荡对光纤器件的损坏。为了进一



图2 光功率光纤放大级 MOPA 结构

Fig. 2 MOPA structure of optical power fiber amplification stage

步提高输出稳定性,采用分束器和光电探测器(PD)对输出信号进行采样,通过伺服系统反馈至泵浦LD,对输出功率进行反馈控制。

根据应用场景的不同,两者设计也略有不同。PA 输入级采用了具备隔离功能的隔离分束器(tap-ISO) 以有效隔离放大器的后向回波,防止损坏种子源。由 于前级PA输出具备了隔离功能,所以BO输入级仅使 用高分束比的分束器即可防止放大器空载,能够降低 ISO带来的插入损耗。另一处不同在于,在CPS后级 PA添加了一段滤波带宽为±2 nm的保偏带通滤波片 (PMBP)作为中间级滤波,提高PA输出的信噪比,抑 制ASE等噪声在光纤链路中的传播。

4 结果与讨论

4.1 部组件测试

MOPA器件是实现光功率放大的唯一器件,同时 也是细腰光阱高功率控制的重要组成部分,通过对三 路放大器进行逐级测量,确定了放大器工作点和驱动 电流控制曲线。

测得不同泵浦功率下 MOPA 器件的开环功率曲 线[图3(a)]和各级LD的泵浦功率随电流的变化曲线 [图3(b)]。图中方点线、圆点线和三角点线分别是 PA、BO-CH1和BO-CH2的测试数据。放大器的泵浦 阈值功率较低,增益曲线线性光滑,未出现明显损伤及 饱和现象,最大输出功率均能满足激光器设计需求。



图 3 MOPA 输出功率随 PA和 BO的泵浦功率的变化,以及放大器泵浦功率随泵浦电流的变化。(a) MOPA 输出功率随 PA和 BO 的泵浦功率的变化;(b) 放大器泵浦功率随泵浦电流的变化

Fig. 3 Pump power of PA and BO varying with MOPA output power, and pump power of amplifier varying with pump current. (a) Pump power of PA and BO varying with MOPA output power; (b) pump power of amplifier varying with pump current

对放大器输出信号进行光谱采集,得到图4所示的谱线数据。比较图中两类放大器的输出光谱特征可





以发现,相比于种子源,经过PA(实线)和BO(短点线)放大后的信号没有产生明显的加宽和噪声,边模抑制比均达到了-56 dB的水平。特别地,中间级滤波器的加入有效抑制了-10 dB带外噪声,提高了PA预放大光的信噪比,提高了后级放大效率。

测量了不同调制电压下 AOM 的输出光功率,得 到了如图 5 所示的关系曲线,利用曲线对光阱光输出 功率进行标定,以实现深度冷却末期对光阱阱深的精 确控制。选用 0~500 mV 的调制电压的单调增区间 (图中高亮区域)作为光阱光功率的有效控制区间。此 外,还可以通过匹配不同的控制电压来平衡成对光阱 光的输出光功率,防止超冷原子在冷却过程中功率不 平衡导致的加热。由图 5 可知,控制区间内最大关断 比分别为 48.55 dB 和 52.7 dB,满足粗腰光阱光对光





功率关断比的实验要求。

4.2 集成测试

组装完成的激光器可分为两个标准机柜抽屉,其 中光学&电控系统整机高度为178 mm,供电模块高度 为44.5 mm,较常规1.2 m×1.5 m的小型光学实验平 台尺寸更便于集成,可以满足各类可搬运需求。完成 系统集成后,对激光器输出性能和稳定性进行了测试。

对光阱输出光功率和关断比进行的测量与统计结果如表1所示,RSD为相对标准差,Pon为最高出光功率,Poff为最低出光功率。其中,细腰、粗腰光阱光的标准输出功率分别达到5.4W和0.16W,光功率开关比(Ron/off)分别达到了60dB和45dB以上,光功率长期漂移低于6×10⁻³,短期稳定性优于7.2×10⁻⁵@1s。

	Channel	$P_{\rm on}/{ m W}$	$P_{_{\rm off}}/\mu W$	$R_{ m on/off}$ / dB	RSD at 1 h /10 ⁻³	RSD at 1 s /10 ⁻⁵
	CH1	5.41	5.2	60.1	6	7.2
	CH2	5.40	2.2	63.9	5	8.3
	CH3	0.161	4.7	45.4	2	5.5
	CH4	0.167	4.6	45.6	3	6.3

表1 激光器输出光功率与闭环稳定性 Table 1 Output power of laser and closed-loop stability

经过进一步的测量,得到了满负荷输出时光阱光 功率相对强度噪声(RIN)谱线,如图6所示。图中虚线 为由式(2)推导出的原子寿命*T*₁>100 s所对应的 RIN 值曲线,短点线为细腰光阱光的 RIN 谱线,而实线为粗 腰光阱光的 RIN 谱线。可以发现由于末级采用了带宽 为 10 kHz 的光功率反馈控制,粗细腰光阱光的 RIN 曲 线不存在明显的差异,且全频域均优于需求曲线。

特别地,在如图 6 插图所示的高亮区域 ($v_{lower} \sim 10 \text{ kHz}$),激光器 RIN 值显著低于需求曲线,从 而避免了参量激发导致的严重加热和原子数损失现 象。利用式(2)定量计算两束光阱光的功率抖动,其中 细腰光阱光的功率稳定度静态指标为 $\varepsilon_{thin} = 5.1 \times 10^{-4}$ ($v_{lower} = 160 \text{ Hz}$),而粗腰光阱光的功率稳定度静

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图 6 两类光阱满功率输出时的 RIN 谱线(插图为 DC 到 10 kHz 阴影区域的噪声谱)

Fig. 6 RIN spectral lines of two optical dipole traps with full output power (inset is detail of shadow area from DC to 10 kHz)

态指标为 ε_{wide} =7.9×10⁻³(v_{lower} =1Hz)。

以上测试结果完全满足 TSC 深度冷却实验对光 功率、关断比和噪声抑制的各项需求。

4.3 实验验证

将上述激光系统集成至超冷原子物理实验柜地面 样机的物理系统上,并进行了初步的⁸⁷Rb的地面模拟 TSC 深度冷却实验。实验包括了预冷却阶段 (MOT & molasses)、光阱装载阶段(FORT loading)、 蒸发冷却阶段(1st eva. cooling)和绝热膨胀阶段(2nd adia. cooling)等,流程如图7所示。实验周期内,光阱 光功率依照图中短点线和实线的方式进行扫描,采样 频率为1kHz。



- 图 7 细腰光阱(1st FORT)与粗腰光阱(2nd FORT)的光功率 曲线(右上角插图为二级绝热膨胀冷却阶段细节展开图, 图 I 为细腰光阱蒸发冷却结束时的原子光学密度,图 Ⅱ 是粗腰光阱保持结束时的原子光学密度,图 Ⅲ是绝热膨 胀冷却结束时的原子光学密度)
- Fig. 7 Optical power curves of 1st FORT and 2nd FORT (inset is details of 2nd adia. cooling stage, subfigures I, II, and III are atom optical density of end of 1st eva. cooling for 1st FORT, end of holding for 2nd FORT, and end of 2nd adia. cooling)

在粗腰光阱绝热膨胀冷却各阶段采用20ms的飞 行时间的吸收成像对深度冷却效果进行分析,得到如 图 7中插图 I、Ⅱ、Ⅲ所示的光学厚度(OD)分布。插 图 I 中原子处于蒸发冷却结束阶段,此时 BEC等效温 度降低至 33 nK;插图 Ⅱ 对应粗腰光阱保持阶段结束, 此时系统温度进一步降低至 14 nK;插图 Ⅲ 是进行绝 热膨胀冷却后的结果,温度进一步降低至 10 nK。以 上实验结果说明本文所设计的光阱激光器具备进行实 验的条件,满足实验要求。

5 结 论

详细阐述了一种用于⁸⁷Rb原子冷却的集成式全光 纤1064 nm激光系统的研制和测试。该系统利用全光 纤器件实现了种子源、光功率放大、光功率调控和输出 反馈等功能,具备小型化、集成化的特点,适合各类具 有搬运需求的超冷原子应用中。激光器采用了两级分 离式的MOPA方案,利用后置的高功率放大器实现了 两路5W和两路160mW的大跨度的光功率独立输 出。配合严格的时序控制,联合了BO与光纤AOM的 功率控制能力,实现了60dB的大动态范围功率扫描。 通过有效的反馈控制措施,将相对强度噪声降低到 5×10⁻⁴的水平。后续的地面模拟微重力TSC实验中 得到了低于一般全光蒸发冷却能够达到的10 nK量级 的超低温,结果证明该激光系统充分满足TSC深度冷 却实验对4束冷却光在功率、控制以及稳定性上的要 求,在后续空间超冷原子物理实验柜在轨实验中起到 了工程验证的作用。

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Development of Integrated All-Fiber 1064 nm Laser System for Ultracold Atomic Cooling

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Abstract

Objective Deep cooling is a key step in the preparation of ultracold atoms and a key technology for exploring extremely low temperatures. To rule out the effect of gravity, scientists combined microgravity experiments with atomic cooling experiments to get even colder temperatures below 1 nK. The Cold Atom Physics Research rack in the Chinese space station will adopt the deep cooling scheme of all-optical two-stage cooling (TSC) proposed by Chen Xuzong's research group at Peking University. In this scheme, two pairs of 1064 nm Far-Off Resonant optical-dipole Traps (FORTs) are used to successively cool ⁸⁷Rb atomic cloud by evaporative cooling and adiabatic expansion cooling. According to a direct Monte Carlo simulation, it is concluded that ultracold atomic gas below 100 pK can be obtained in microgravity environments by TSC process. In order to cover the experimental requirements in orbit, we develop a set of integrated optical-fiber 1064-nm laser system. This system provides four high power, high dynamic range, and low relative intensity noise (RIN) 1064-nm infrared channels, with full digitalization, high integration, high stability, and easy maintenance, which fully meets the application requirements of the space station and other remote-control projects.

Methods The system adopts beam splitting amplification scheme, namely, "pre-amplifiers+beam splitters +power controlling+post-amplifiers", to carry out multi-channel, high-power amplified, and high-dynamic range-controlled laser sources which is generated from a single seed light.

This laser system composed of polarization-maintaining fiber devices, as shown in Fig. 1, can be divided into two stages. The first stage, "high-quality seed source", as shown in left purpure shadow of Fig. 1, consists of three parts: a seed source, a high-gaining pre-amplifier (PA), and cascade fiber beam splitters, and it is used to provide stable and narrow-linewidth seed light required by the subsequent optical operations. The other stage, "high-power amplification", as shown in right shadow of Fig. 1, consists of two components: a power control level, consisting of boost amplifiers (BO) and fiber-coupled acousto-optic modulator (AOM), and a power monitoring level, consisting of terminal photodiodes, and it plays the role of amplifying, output controlling, and power feedback, so that the output signals meet the experimental requirements in terms of high power, high dynamic range, high stability, and low RIN. From the left to right in Fig. 1, the continuous-wave seed signal, coming from a single-mode narrow 1064-nm laser tube, is sequentially amplified, filtered, split, and controlled within this full-functional optical platform to generate four 1064-nm FORTs, CH1-CH4, where CH1 and CH2 are called as high-power thin-waisted FORTs, and CH3 and CH4 are named after low-power wide-waisted FORTs.

As for the design of amplifiers, our laser adopts the full-fiber Master Oscillation Power Amplifier (MOPA) scheme to enlarge the optical power, where ytterbium-doped fibers (YDFs) with emission band from 1000 nm to 1100 nm are selected as the gain medium in the application of ⁸⁷Rb TSC and a 976-nm wavelength-locked laser diode is used for cladding forward pumping of these YDF. Both of PA and BOs are adopted a one-level MOPA scheme, as present in Fig. 2, to amplify and control the gained beams. With these amplifiers and power feedback mechanism, the laser system has capability of producing multi-channel laser with high power and low noisy, which satisfies the TSC experimental requirements.

Results and Discussions We run a series of tests to evaluate the performance of the laser system in terms of output power, spectrum, stability, RIN, etc. and conduct ground-based TSC pre-experiments to verify the overall system design in real experimental environments. The results show that this system has realized two 5-W and two 160-mW optical power independent output channels, has performed its capability of 60-dB high power-scanning dynamic range, as shown in Table 1, and has reduced the RIN as low as 5×10^{-4} , as demonstrated in Fig. 6. In the subsequent ground TSC experiments, we have obtained an ultra-cold ⁸⁷Rb atomic cluster with an extreme-low temperature of 10 nK, which is much lower than the cooling temperature in general all-optical evaporative cooling, and the experimental results are presented in Fig. 7 in details. All the tests and experiments indicate that our laser system reaches the overall performance requirements and is competent in future in-orbit TSC experiments.

Conclusions In this paper, we describe in detail the development and testing of an integrated all fiber 1064-nm laser system for ⁸⁷Rb atomic deep cooling. The system uses all optical fiber devices to realize the functions of seed source, optical power amplification, and optical power feedback controlling. It has the characteristics of digitalization and integration, and it is suitable for various applications of ultracold atoms with mobile requirements. The performance evaluation and experimental results prove that the laser system fully meets the power, control, and stability requirements of the TSC deep cooling experiments on four beams of optical dipole traps. This laser system has been installed in the Cold Atom Physics Research rack in Chinese Space Station, has been launched in October 2022, and plays an important role in ultracold physics researches in orbit.

Key words laser optics; laser trapping; Bose-Einstein condensate; optical fiber laser; laser cooling