

湍流大气脉冲波束经漫射目标散射的统计特性

向宁静¹ 吴振森² 郭秋芬¹

¹咸阳师范学院物理与电子工程学院, 陕西 咸阳 712000

²西安电子科技大学物理与光电工程学院, 陕西 西安 710071

摘要 基于广义惠更斯-菲涅耳原理和粗糙面散射理论, 考虑发射机到目标和目标到接收机双程路径中大气湍流对光束传输的影响, 研究了脉冲波束经漫射目标散射后的二阶统计特性。推导了接收机处双点双频互相干函数(MCF)的表达式, 计算得到平均强度以及复相干度因子, 并对此进行数值模拟。结果表明, 相位结构函数占优情况下, 接收面的脉冲平均强度与大气湍流水平无关; 但脉冲相干带宽与湍流强度、中心频率、湍流外尺度、观察处两点间距离、频差有关。

关键词 物理光学; 大气湍流; 双频互相干函数; 脉冲波束; 漫射目标

中图分类号 O564 **文献标识码** A

doi: 10.3788/AOS201636.1026016

Statistical Properties of Pulse Beams from Diffuse Targets in Atmospheric Turbulence

Xiang Ningjing¹ Wu Zhensen² Guo Qiufen¹

¹*School of Physics and Electronic Engineering, Xianyang Normal University, Xianyang, Shaanxi 712000, China*

²*School of Physics and Optoelectronic Engineering, Xidian University, Xi'an, Shaanxi 710071, China*

Abstract Based on the generalized Huygens-Fresnel principle and the rough surface scattering theory, the effect of atmospheric turbulence on both pulse beam propagating to the target and scattering field propagating back to the receiver is studied, and the second-order statistical properties of pulses scattered by diffuse targets are investigated. An expression is deduced for the multiple-frequency mutual coherence function (MCF) of a reflected pulse beam from the rough target in atmospheric turbulence. According to MCF an expression of the mean intensity and the degree of complex coherence at the receiver is derived. The numerical simulation results indicate that the mean intensity is independent on the atmospheric turbulence, and the coherence bandwidth depends on the turbulence strength, the central angular frequency, the outer scale of turbulence, the position separation and the angular frequency difference when the phase structure function is dominant.

Key words physical optics; atmospheric turbulence; multiple-frequency mutual coherence function; pulse beam; diffuse target

OCIS codes 260.2110; 010.1330; 010.3310

1 引 言

近年来, 高频带宽在卫星通信中对数据的传输使得超短脉冲波束在遥感、雷达工作、高速自由空间光通信、高空防御技术等许多领域有广泛的应用。Gardner 等^[1]利用 Rytov 理论分析激光脉冲波束在弱起伏湍流大气中的传输理论。20 世纪 70 年代, 研究人员主要研究湍流大气中球面波的双频互相干函数(MCF)^[2-4]。1981 年, Fante^[5]利用广义惠更斯-菲涅耳原理计算窄带平面源辐射非均匀湍流中的双频互相干函数。20 世纪 90 年代, Young 等^[6]利用 ABCD 矩阵推导了弱湍流高斯脉冲的双频互相干函数。在以上

收稿日期: 2016-03-30; **收到修改稿日期:** 2016-05-09

基金项目: 国家自然科学基金(61271110, 11504286)、陕西省教育厅基金(14JK1798)、咸阳师范校级项目(14XSYK1010, 15XSYK035)

作者简介: 向宁静(1979—), 女, 博士, 主要从事光(电磁)波在大气湍流中的散射特性方面的研究。

E-mail: xiangningjing@sohu.com

研究的基础上,许多学者讨论了脉冲波束在随机介质中的光场特征以及平均强度和交叉谱密度函数^[7-12]。

目前工作集中考虑脉冲波束在湍流中传输时的脉冲展宽、脉冲畸变、时间相干度等特性,没有涉及湍流中含有目标的情况。许多文献不考虑湍流的影响^[13-14],讨论了脉冲波束经粗糙面散射后的双频 MCF,继而分析粗糙面特性。Lee 等^[15-17]研究了湍流大气中漫射目标和含多个镜反射点漫射目标的散斑统计特性。西安电子科技大学吴振森课题组讨论了湍流大气中斜程传输漫射目标、角反射器散射特性以及高斯分布粗糙面的散射特性^[18-22]。本文在已完成的连续波束工作的基础上,研究了双程湍流脉冲波束经漫射目标散射后通过湍流大气传输的二阶统计特性。

2 分析模型

考虑窄带源光束在湍流中辐射,光场的时延特性写为

$$U(L, \boldsymbol{\rho}, t) = \exp(i\omega_0 t) \int u(L, \boldsymbol{\rho}, \omega) \exp(i\omega t) d\omega, \quad (1)$$

式中 $u(L, \boldsymbol{\rho}, \omega)$ 为时频谱的正频部分, ω_0 为辐射中心频率, $\boldsymbol{\rho}$ 为垂直传输距离的横向坐标矢量, L 为脉冲的传输距离, ω 为脉冲频率, t 为时间。如果 $\langle u(L, \boldsymbol{\rho}_1, \omega) u^*(L, \boldsymbol{\rho}_2, \omega') \rangle$ 值已知, 根据(1)式可以计算 $\langle U(L, \boldsymbol{\rho}_1, t) U^*(L, \boldsymbol{\rho}_2, t') \rangle$ 测量值。

假定源场 $u(0, \mathbf{r}_1, k_1)$ 在 $L=0$ 处以频率 $\omega_1 = ck_1$ 向外辐射, c 为光速, k_1 为波数, $\mathbf{r}_1 = (x_1, y_1)$ 。根据广义惠更斯-菲涅耳原理可以得到 L 处的场为

$$u_i(L, \boldsymbol{\rho}_1, k_1) = \frac{k_1 \exp(ik_1 L)}{2\pi i L} \int d\mathbf{r}_1 u(0, \mathbf{r}_1, k_1) \exp\left[i \frac{k_1}{2L} (\boldsymbol{\rho}_1 - \mathbf{r}_1)^2 + \psi(\boldsymbol{\rho}_1, \mathbf{r}_1, k_1)\right], \quad (2)$$

式中 $\psi(\boldsymbol{\rho}_1, \mathbf{r}_1, k_1)$ 是球面波通过湍流从 $(0, \mathbf{r}_1)$ 到 $(L, \boldsymbol{\rho}_1)$ 引起的复相位扰动。如果湍流边界与波长满足 $k_1 L \gg 1$, $|\boldsymbol{\rho}_1 - \boldsymbol{\rho}_2| \ll L$ 且 $k_1 |\boldsymbol{\rho}_1 - \boldsymbol{\rho}_2|^3 z^{-4} \ll 1$ 时(2)式成立。假定源场起伏与湍流介质的起伏相互独立, 从(2)式可得

$$\begin{aligned} \Gamma_{12}(L, \boldsymbol{\rho}_1, \boldsymbol{\rho}_2) &= \langle u_i(L, \boldsymbol{\rho}_1, k_1) u_i^*(L, \boldsymbol{\rho}_2, k_2) \rangle = \\ &= \frac{k_1 k_2 \exp[i(k_1 - k_2)L]}{(2\pi L)^2} \iint d\mathbf{r}_1 d\mathbf{r}_2 \Gamma_{12}(0, \mathbf{r}_1, \mathbf{r}_2) \exp\left[\frac{ik_1}{2L} (\boldsymbol{\rho}_1 - \mathbf{r}_1)^2 - \frac{ik_2}{2L} (\boldsymbol{\rho}_2 - \mathbf{r}_1)^2\right] \cdot \\ &\quad \langle \exp[\psi(\boldsymbol{\rho}_1, \mathbf{r}_1, k_1) + \psi^*(\boldsymbol{\rho}_2, \mathbf{r}_2, k_2)] \rangle, \end{aligned} \quad (3)$$

$$\Gamma_{12}(0, \mathbf{r}_1, \mathbf{r}_2) = u(0, \mathbf{r}_1, k_1) u^*(0, \mathbf{r}_2, k_2). \quad (4)$$

考虑准直光束

$$u(0, \mathbf{r}_1, k_1) = \exp\left(-\frac{r_1^2}{2\omega_0^2}\right), \quad (5)$$

式中 ω_0 为波源有效半径, 利用 Rytov 二次结构近似方法^[3]可得

$$\begin{aligned} &\langle \exp[\psi(\boldsymbol{\rho}_1, \mathbf{r}_1, k_1) + \psi^*(\boldsymbol{\rho}_2, \mathbf{r}_2, k_2)] \rangle \approx \\ &\Gamma_2 \exp\left[-\frac{(\mathbf{r}_1 - \mathbf{r}_2)^2 + (\boldsymbol{\rho}_1 - \boldsymbol{\rho}_2) \cdot (\mathbf{r}_1 - \mathbf{r}_2) + (\boldsymbol{\rho}_1 - \boldsymbol{\rho}_2)^2}{\rho_0^2}\right], \end{aligned} \quad (6)$$

式中 $\Gamma_2 = \exp(-0.391 C_n^2 L k_d^2 L_0^2)$, L_0 为湍流的外尺度, C_n^2 为大气折射率结构常数, $k_d = k_1 - k_2$; $\rho_0 = (0.54 C_n^2 k_c^2 l_0^{-1/3} L)^{-1/2}$ 为球面波通过大气湍流的空间相干长度, l_0 为湍流内尺度, $2k_c = k_1 + k_2$ 。采用 von-Karman 谱求解湍流的复相位扰动, 当 $(k_1 - k_2)/(k_1 + k_2) \ll 1$ 时适合任何湍流强度。

将波束照射的目标等效为一个源, 将经过目标散射后的场 $u_s(\boldsymbol{\rho})$ 看作初始场, 则接收机 \mathbf{p} 处的场表达式为

$$u_r(\mathbf{p}) = \frac{k \exp(ikL)}{2\pi i L} \int d\boldsymbol{\rho} u_s(\boldsymbol{\rho}) \exp\left[\frac{ik}{2L} |\mathbf{p} - \boldsymbol{\rho}|^2 + \psi_2(\mathbf{p}, \boldsymbol{\rho})\right]. \quad (7)$$

根据粗糙面理论, 类比连续波束粗糙面散射, 得到脉冲波束经粗糙面散射后的场为

$$\langle u_s(\boldsymbol{\rho}_1, k_1) u_s^*(\boldsymbol{\rho}_2, k_2) \rangle = \frac{4\pi^2}{k_1 k_2} \langle u_i(\boldsymbol{\rho}_1, k_1) u_i^*(\boldsymbol{\rho}_2, k_2) \rangle \delta(\boldsymbol{\rho}_1 - \boldsymbol{\rho}_2), \quad (8)$$

式中 δ 表示散射场满足 δ 分布。

考虑脉冲经历的湍流前向路径与后向路径互不相关, 散射场经湍流传输后在接收面的场为

$$\langle u_r(L, \mathbf{p}_1, k_1) u_r^*(L, \mathbf{p}_2, k_2) \rangle = \frac{k_1 k_2 \exp[i(k_1 - k_2)L]}{(2\pi L)^2} \iint d\boldsymbol{\rho}_1 d\boldsymbol{\rho}_2 \langle u_s(\boldsymbol{\rho}_1, k_1) u_s^*(\boldsymbol{\rho}_2, k_2) \rangle \times \exp\left[\frac{ik_1}{2L} (\mathbf{p}_1 - \boldsymbol{\rho}_1)^2 - \frac{ik_2}{2L} (\mathbf{p}_2 - \boldsymbol{\rho}_2)^2\right] \langle \exp[\psi(\mathbf{p}_1, \boldsymbol{\rho}_1, k_1) + \psi^*(\mathbf{p}_2, \boldsymbol{\rho}_2, k_2)] \rangle. \quad (9)$$

将(8)式代入(9)式得到散射场的互相干函数为

$$\langle u_r(L, \mathbf{p}_1, k_1) u_r^*(L, \mathbf{p}_2, k_2) \rangle = \frac{\exp[i(k_1 - k_2)L]}{\pi L^2} \int d\boldsymbol{\rho} \langle u_i(\boldsymbol{\rho}, k_1) u_i^*(\boldsymbol{\rho}, k_2) \rangle \times \exp\left[\frac{ik_1}{2L} (\mathbf{p}_1 - \boldsymbol{\rho})^2 - \frac{ik_2}{2L} (\mathbf{p}_2 - \boldsymbol{\rho})^2\right] \langle \exp[\psi(\mathbf{p}_1, \boldsymbol{\rho}, k_1) + \psi^*(\mathbf{p}_2, \boldsymbol{\rho}, k_2)] \rangle. \quad (10)$$

根据(3)式可以计算得到双频单点的互相干函数为

$$\langle u_i(L, \boldsymbol{\rho}, k_1) u_i^*(L, \boldsymbol{\rho}, k_2) \rangle = \frac{k_1 k_2 \exp[i(k_1 - k_2)L]}{(2\pi L)^2} \iint d\mathbf{r}_1 d\mathbf{r}_2 \exp\left(-\frac{r_1^2 + r_2^2}{2\omega_0^2}\right) \times \exp\left[\frac{ik_1}{2L} (\boldsymbol{\rho} - \mathbf{r}_1)^2 - \frac{ik_2}{2L} (\boldsymbol{\rho} - \mathbf{r}_2)^2\right] \langle \exp[\psi(\boldsymbol{\rho}, \mathbf{r}_1, k_1) + \psi^*(\boldsymbol{\rho}, \mathbf{r}_2, k_2)] \rangle. \quad (11)$$

采用坐标变化 $2\mathbf{R} = \mathbf{r}_1 + \mathbf{r}_2, \mathbf{r} = \mathbf{r}_1 - \mathbf{r}_2$, 则

$$\langle u_i(L, \boldsymbol{\rho}, k_1) u_i^*(L, \boldsymbol{\rho}, k_2) \rangle = \frac{k_1 k_2 \exp[i(k_1 - k_2)L]}{(2\pi L)^2} \iint d\mathbf{r} d\mathbf{R} \exp\left(-\frac{2R^2 + r^2/2}{2\omega_0^2}\right) \times \exp\left[\frac{ik_1}{2L} \left(\boldsymbol{\rho} - \frac{2\mathbf{R} + \mathbf{r}}{2}\right)^2 - \frac{ik_2}{2L} \left(\boldsymbol{\rho} - \frac{2\mathbf{R} - \mathbf{r}}{2}\right)^2\right] \Gamma_2 \exp\left(-\frac{r^2}{\rho_0^2}\right). \quad (12)$$

对(12)式进行积分,

$$\langle u_i(L, \boldsymbol{\rho}, k_1) u_i^*(L, \boldsymbol{\rho}, k_2) \rangle = \frac{k_1 k_2 \exp(ik_d L)}{(2\pi L)^2} \frac{4\pi^2}{4ab + k_c^2/L^2} \Gamma_2 \exp\left\{-\frac{[ak_d^2 L + k_c^2(ik_d + bL)]\rho^2}{L(k_c^2 + 4abL^2)}\right\}, \quad (13)$$

式中 $a = \frac{1}{4\omega_0^2} + \frac{1}{\rho_0^2} + \frac{ik_d}{2L}$, $b = \frac{1}{\omega_0^2} + \frac{ik_d}{2L}$ 。将(13)式代入(9)式得

$$\langle u_r(L, \mathbf{p}_1, k_1) u_r^*(L, \mathbf{p}_2, k_2) \rangle = \frac{k_1 k_2 \exp[2i(k_1 - k_2)L]}{\pi (2\pi L)^2 L^2} \frac{4\pi^2}{4ab + k_c^2/L^2} \int d\boldsymbol{\rho}_2 \Gamma_2 \times \exp\left\{-\frac{[ak_d^2 L + k_c^2(ik_d + bL)]\rho^2}{L(k_c^2 + 4abL^2)}\right\} \Gamma_2 \exp\left(-\frac{p^2}{\rho_0^2}\right) \times \exp\left[\frac{ik_1}{2L} (\mathbf{p}_1 - \boldsymbol{\rho})^2 - \frac{ik_2}{2L} (\mathbf{p}_2 - \boldsymbol{\rho})^2\right], \quad (14)$$

式中 $p = |\mathbf{p}_1 - \mathbf{p}_2|$ 。(14)式进行积分可得

$$\langle u_r(L, \mathbf{p}_1, k_1) u_r^*(L, \mathbf{p}_2, k_2) \rangle = \frac{k_1 k_2 \exp[2i(k_1 - k_2)L]}{(2\pi L)^2 L^2} \frac{4\pi^2}{4ab + k_c^2/L^2} \cdot \Gamma_2^2 \exp\left(\frac{ik_1}{2L} p_1^2 - \frac{ik_2}{2L} p_2^2\right) \frac{1}{d} \exp\left(\frac{e^2}{4d}\right) \exp\left(-\frac{p^2}{\rho_0^2}\right), \quad (15)$$

式中 $c = \frac{ak_d^2 L + k_c^2(ik_d + bL)}{L(k_c^2 + 4abL^2)}$, $d = -\frac{ik_d}{2L} + c$, $e = \frac{ik_2 p_2}{2L} - \frac{ik_1 p_1}{2L}$ 。

考虑单点双频互相干函数即 $k_1 \neq k_2, \mathbf{p}_1 = \mathbf{p}_2 = \mathbf{p}$, (15)式变为

$$\langle u_r(L, \mathbf{p}, k_1) u_r^*(L, \mathbf{p}, k_2) \rangle = \frac{k_1 k_2 \exp(2ik_d L)}{d (2\pi L)^2 L^2} \frac{4\pi^2}{4ab + k_c^2/L^2} \Gamma_2^2 \exp\left(\frac{ik_d}{2L} p^2\right) \exp\left(\frac{e^2}{4d}\right), \quad (16)$$

式中 $e = -ik_d p/L$ 。

考虑单点单频互相干函数(平均强度), 即 $k_1 = k_2, \mathbf{p}_1 = \mathbf{p}_2$, 则(15)式化简为

$$\langle u_r(L, \mathbf{p}, k) u_r^*(L, \mathbf{p}, k) \rangle = \frac{\omega_0^2}{L^2}. \quad (17)$$

可以看出接收面的平均强度与大气湍流水平无关, 只与波源的有效半径和传播距离有关, 此结果与文献[14]

结论一致。

考虑双点单频即 $k_1 = k_2, \mathbf{p}_1 \neq \mathbf{p}_2$, 则(15)式变为

$$\langle u_r(L, \mathbf{p}_1, k) u_r^*(L, \mathbf{p}_2, k) \rangle = \frac{\omega_0^2}{L^2} \exp \left[-\frac{p^2}{4\omega_0^2} - \frac{k^2 \omega_0^2 p^2}{4L^2} - \frac{2p^2}{\rho_0^2} + \frac{ik}{2L}(p_1^2 - p_2^2) \right]. \quad (18)$$

(18)式结果与文献[14]中 高斯波束经粗糙面散射后在接收面的强度分布和互相干函数结果一致, 取振幅为 1。频差为零时, 互相干函数表示散射场自身的相干性, 是双频互相干函数的特例。

3 复相干度

复相干度用来量化一对任意频率散射场的相关强度, 其表达式为

$$\mu(\mathbf{p}_1, \mathbf{p}_2, L, k_1, k_2) = \frac{\Gamma(\mathbf{p}_1, \mathbf{p}_2, L, k_1, k_2)}{\sqrt{\Gamma(\mathbf{p}_1, L, k_1) \Gamma(\mathbf{p}_2, L, k_2)}} = \frac{L^2 k_1 k_2 \exp(2ik_d L)}{\omega_0^2 (2\pi L)^2 L^2} \frac{4\pi^2}{4ab + k_c^2/L^2} \Gamma_2^2 \exp\left(\frac{ik_1}{2L} p_1^2 - \frac{ik_2}{2L} p_2^2\right) \frac{1}{d} \exp\left(\frac{e^2}{4d}\right) \exp\left(-\frac{p^2}{\rho_0^2}\right). \quad (19)$$

从(19)式可以看出复相干度与湍流强度、频率、波源的有效半径等参数有关。 Γ_2 和 $\exp(-p^2/\rho_0^2)$ 是与角频率和两点位置有关的湍流引起的衰减因子, 影响复相干度的调制。

考虑窄带脉冲散射, 定义新的变量 $\omega_d = \omega_1 - \omega_2, 2\omega_c = \omega_1 + \omega_2$ 代换 $\omega = kc = 2\pi c/\lambda$ 。窄带脉冲入射波时间信号的中心角频率 ω_0 远大于信号带宽, 复相干度函数为 ω_c 的缓变函数。 $|\mu(\mathbf{p}_1, \mathbf{p}_2, L, k, k)|$ 或 $|\mu(\mathbf{p}_1, \mathbf{p}_2, L, \omega, \omega)|$ 描述了光束横向相干长度的相关性, 实际上与初始脉宽和时域相关带宽没有关系。图 1 中 $|\mu(\mathbf{p}, \mathbf{p}, L, \omega_0, \omega_d)|$ 作为频差 ω_d 的函数, 其中心频率 $\omega_0 = 2\pi c/\lambda_0$ 固定, 角频率 $\omega_1 = \omega_0 + \omega_d$ 随着 ω_d 变化。 $|\mu(\mathbf{p}, \mathbf{p}, L, \omega_0, \omega_d)|$ 用来测量 \mathbf{p} 点在不同频率 ω_0, ω_1 的空间谱相干性。考虑在轴 $\mathbf{p} = (0, 0)$ 复相干因子, 从图 1、2 看出复相干因子关于 $\delta_\lambda = 0$ 不完全对称, 与中心频率 ω_0 、频差 ω_d 、表征湍流强度的参数 C_n^2 等有关。散射波的双频互相干函数在中心频率处最大, 随着频差 $\omega_d = 2\pi c/\lambda_0 - 2\pi c/(\lambda_0 + \delta_\lambda)$ 的增大, 互相干函数迅速减小到零。从物理意义上讲, 当双频互相干函数下降到 $1/e$ 时对应的频率间隔定义为相干带宽。散射波的脉冲宽度 T_d 与双频互相干函数之间的相干带宽满足 $T_d = 2\pi/\omega_d$, 频差越小, 散射波的脉冲宽度越大。

从图 1 得出湍流强度越大, 相干带宽越小, 相应脉冲宽度越大, 这与理论相符; 湍流强度影响波束横向空间相干度, 随着湍流增强, 谱相干度逐渐减小, 这与文献[23]结果一致。由图 2 可知中心波长影响相干带宽, 波长越大, 相干带宽越大, 反之脉冲宽度越小, 这是因为湍流对长波长的影响较小。从图 3 可以看出湍流的外尺度对相干带宽影响较大, 最新实验证明湍流的外尺度大约在 5 m 之内。湍流外尺度变大时, 相干带宽相应减小, 而脉冲宽度变大。由于湍流内尺度使波束发生衍射作用, 谱表达式中的内尺度大小对互相干函数几乎没有影响。从图 4 可以看出, 不同的内尺度产生的相干带宽相同。图 5 考虑了不同点的互相干函数, 随

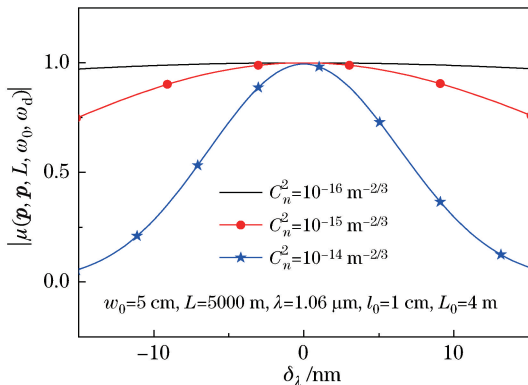


图 1 不同湍流强度下复相干函数因子随波长差的变化
Fig. 1 Dependence of degree of complex coherence on wavelength difference under different turbulence intensity

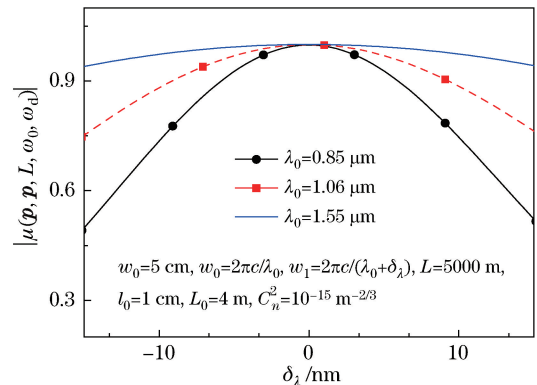


图 2 不同中心波长下复相干函数因子随波长差的变化
Fig. 2 Dependence of degree of complex coherence on wavelength difference at different central wavelengths

着两点距离的增加,互相干函数减小,逐渐降到零,即空间相干长度减小;初始频差越小,互相干函数衰减越慢,随着两点距离增加,频差影响不明显,互相干函数趋于一致,说明此时起主导作用的是两点间距离,湍流等其他因素影响较小。

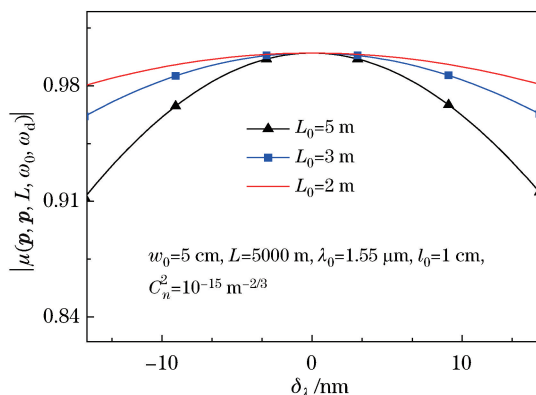


图 3 不同外尺度下复相干函数因子随波长差的变化
Fig. 3 Dependence of degree of complex coherence on wavelength difference at different outer scales

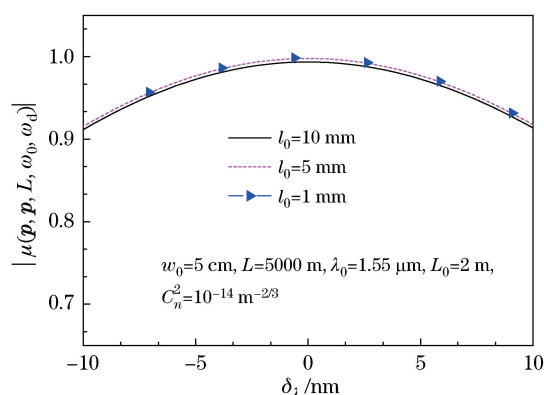


图 4 不同内尺度下复相干函数因子随波长差的变化
Fig. 4 Dependence of degree of complex coherence on wavelength difference at different inner scales

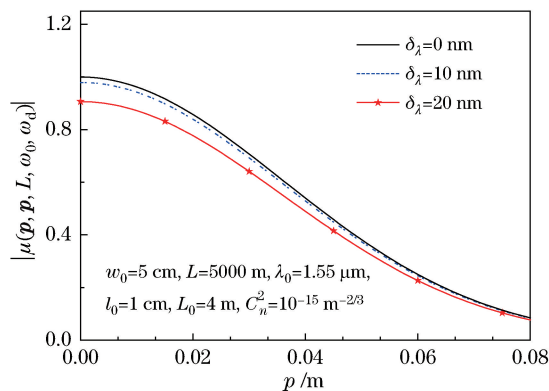


图 5 不同波长差条件下复相干函数因子随两点之间距离的变化

Fig. 5 Dependence of degree of complex coherence on position separation under different wavelength difference

4 结 论

基于广义惠更斯-菲涅耳原理和粗糙面理论知识,利用相位结构函数的二次近似,研究双程湍流大气中漫射目标对脉冲光束散射的二阶统计特性。考虑脉冲波束和完全漫反射目标,推导了接收面处的双频双点互相干函数表达式,双频双点互相干函数可以退化为双频单点、单点双频互相干函数。在此基础上计算了复相干度因子并进行数值模拟,结果表明,大气湍流越强,复相干因子下降越迅速;中心波长 λ_0 越大,即中心频率 ω_0 越小,复相干因子下降越慢;其他条件一定时,湍流的外尺度 L_0 对复相干因子有影响,外尺度 L_0 越大,复相干因子衰减越快;湍流内尺度 l_0 对复相干因子几乎没有影响,说明湍流的折射效应起主导作用。当观察处两点间距离增加时,复相干因子下降迅速,波长差越大,下降越快,复相干因子逐渐趋于一致。由于有关湍流大气中漫射目标光散射特性的实验结果目前报道较少,因此数值模拟结果可为下一步研究任意粗糙目标提供参考。

参 考 文 献

- Gardner C S, Plonus M A. The effect of atmospheric turbulence on the propagation of pulsed laser beams [J]. Radio Science, 1975, 10(1): 129-137.
- Sreenivasiah I, Ishimaru A, Shin T H. Two-frequency mutual coherence function and pulse propagation in random medium: An analytic solution to the plane wave case [J]. Radio Science, 1976, 11(10): 775-778.

- 3 Fante R. Multiple-frequency mutual coherence functions for a beam in a random medium [J]. IEEE Transactions on Antennas and Propagation, 1978, 26(4): 621-623.
- 4 Sreenivasiah I, Ishimaru A. Beam wave two-frequency mutual-coherence function and pulse propagation in random media: Analytic solution [J]. Applied Optics, 1979, 18(10): 1613-1618.
- 5 Fante R L. Two-position, two-frequency mutual-coherence function in turbulence [J]. Journal of the Optical Society of America, 1981, 71(12): 1446-1451.
- 6 Young C Y, Ishimaru A, Andrews L C. Two-frequency mutual coherence function of a Gaussian beam pulse in weak optical turbulence: An analytic solution [J]. Applied Optics, 1996, 35(33): 6522-6526.
- 7 Gozani J. Pulsed beam propagation through random media [J]. Optics Letters, 1996, 21(21): 1712-1714.
- 8 Young C Y, Andrews L C, Ishimaru A. Time-of-arrival fluctuations of a space-time Gaussian pulse in weak optical turbulence: An analytic solution [J]. Applied Optics, 1998, 37(33): 7655-7660.
- 9 Navas A J, Balsells J M G, Vázquez M C, *et al.* Numerical model for the temporal broadening of optical pulses propagating through weak atmospheric turbulence [J]. Optics Letters, 2009, 34(23): 3662-3664.
- 10 Chen C, Yang H, Lou Y, *et al.* Second-order statistics of Gaussian Schell-model pulsed beams propagating through atmospheric turbulence [J]. Optics Express, 2011, 19(16): 15196-15204.
- 11 Xu Zhengwen, Wu Jian, Huo Wenping, *et al.* Temporal broadening of pulse in turbulence medium [J]. Science in China (Series G), 2003, 33(2): 139-147.
许正文, 吴 健, 霍文平, 等. 湍流介质中传播的脉冲时间展宽特性[J]. 中国科学(G辑), 2003, 33(2): 139-147.
- 12 Li Xiaoqing, Ji Xiaoling, Zhu Jianhua. Higher-order intensity moments of optical beams in atmospheric turbulence [J]. Acta Physica Sinica, 2013, 62(4): 044217.
李晓庆, 季小玲, 朱建华. 大气湍流中光束的高阶强度矩[J]. 物理学报, 2013, 62(4): 044217.
- 13 Greenwood D, Powers E. The scattering from curved rough surfaces of an EM wave transmitted through a turbulent medium [J]. IEEE Transactions on Antennas and Propagation, 1972, 20(1): 19-30.
- 14 Sprague R A. Surface roughness measurement using white light speckle [J]. Applied Optics, 1972, 11(12): 2811-2816.
- 15 Lee M H, Holmes J F, Kerr J R. Statistics of speckle propagation through the turbulent atmosphere [J]. Journal of the Optical Society of America, 1976, 66(11): 1164-1172.
- 16 Holmes J F, Lee M H, Kerr J R. Effect of the log-amplitude covariance function on the statistics of speckle propagation through the turbulent atmosphere [J]. Journal of the Optical Society of America, 1980, 70(4): 355-360.
- 17 Wei Hongyan, Wu Zhensen, Peng Hui. Scattering from a diffuse target in the slant atmospheric turbulence [J]. Acta Physica Sinica, 2008, 57(10): 6666-6672.
韦宏艳, 吴振森, 彭 辉. 斜程大气湍流中漫射目标的散射特性[J]. 物理学报, 2008, 57(10): 6666-6672.
- 18 Wu Z S, Li Y Q. Scattering of a partially coherent Gaussian-Schell beam from a diffuse target in slant atmospheric turbulence [J]. Journal of the Optical Society of America A, 2011, 28(7): 1531-1539.
- 19 Xiang Ningjing, Wu Zhensen, Hua Xuexia, *et al.* Statistical properties of a Gaussian-Schell beam from a semi-rough target in the atmospheric turbulence [J]. Scientia Sinica Physica, Mechanica & Astronomica, 2014, 44(5): 457-464.
向宁静, 吴振森, 华雪侠, 等. 高斯-谢尔光束通过湍流大气任意粗糙目标的散射统计特性[J]. 中国科学: 物理学 力学 天文学, 2014, 44(5): 457-464.
- 20 Xiang N J, Wu Z S, Wang M J. Statistic of a Gaussian beam from an arbitrary rough target in the single passage atmospheric turbulence[J]. Science China: Physics, Mechanics & Astronomy, 2014, 57(10): 1854-1859.
- 21 Ke Xizheng, Wang Jiao. Intensity of reflected wave from corner reflector illuminated by partially coherent beam in the atmospheric turbulence[J]. Acta Optica Sinica, 2015, 35(10): 1001001.
柯熙政, 王 姣. 大气湍流中部分相干光束角反射器的回波光强特性[J]. 光学学报, 2015, 35(10): 1001001.
- 22 Wang Liguang, Wu Zhensen, Wang Mingjun. Second-order statistics for wave reflected by a plane mirror with a finite aperture[J]. Acta Optica Sinica, 2013, 33(11): 1101002.
王利国, 吴振森, 王明军. 湍流大气中的有限孔径平面镜反射波的二阶统计特性[J]. 光学学报, 2013, 33(11): 1101002.
- 23 Chen C Y, Yang H M, Lou Y, *et al.* Second-order statistics of Gaussian Schell-model pulsed beams propagating through atmospheric turbulence [J]. Optics Express, 2011, 19(16): 15196-15205.