

高转换效率下具有高斯及类高斯光束的内腔倍频*

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提 要

本文在考虑了振幅的横向分布和基波的衰减时,给出了一些关于倍频的有价值的结果。借助于求解三维耦合波方程,导出了二次谐波功率的最一般的表达式,讨论了基波功率和晶体长度的影响。作为一个特例,也给出了低转换效率下二次谐波功率的表达式。讨论了类高斯光束倍频的平面波近似处理方法,这里借助于类高斯光束的光线方程。作为小结,我们列出了八种不同情况下二次谐波功率的表达式,其中后五种来自本文的推导。

最后,阐明了一种处理内腔倍频激光器的新方法。在我们的模型中,对于在腔内循环的基波功率而言,由于倍频的功率损耗,可视为一种可变的损耗。借助于速率方程的数值解,我们求得了激光腔参数和倍频晶体的最佳值。

到目前为止,所有对于内腔倍频激光器的分析处理,都局限于平面波和小信号近似,有些作者^[1]也涉及到高转换效率的情况,只得到平面波近似的结果。随着如 KTiOPO_4 一类高质量的非线性晶体的研究成熟,以及相位匹配技术的完善^[2,3],倍频效率可达 50~60% 以上。另外,低阶混合模光束(即类高斯光束)^[4]的实际应用,使声光 Q 开关的内腔倍频 YAG 激光器的平均输出功率超过 10 瓦^[4],这就有必要研究高斯及类高斯光束在高转换效率下的倍频问题,而且应该考虑振幅的横向分布。我们在类高斯光束理论^[5]的基础上,考虑了基波的衰减,振幅的横向分布,并导出了二次谐波功率的表达式,进而讨论了高转换效率下的内腔倍频。

一、高转换效率下高斯光束的倍频

为了考虑振幅的横向分布,我们采用柱坐标系 (r, φ, z) (见图 1),假设基波具有圆对称性质,倍频晶体也是圆对称的,所以认为二次谐波也是圆对称的,其基波场和谐波场可写为:

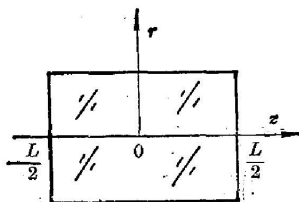


图 1

$$E_1 = \frac{1}{2} \varepsilon_1(r, z) \exp[i(k_1 z + \varphi_1 - \omega_1 t)],$$

$$E_2 = \frac{1}{2} \varepsilon_2(r, z) \exp[i(k_2 z + \varphi_2 - \omega_2 t)].$$

有理由假设基波和谐波的振幅部分能分离为只含 r 和 z 的两部

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分, 即认为场振幅由径向分量和轴向分量两部分组成, 而且各自是独立的, 又假设相位因子 φ 只随 z 而变。这样我们有

$$E_1 = \frac{1}{2} \varepsilon_{1r} \varepsilon_{1z} \exp [i(k_1 z + \varphi_1(z) - \omega_1 t)], \quad (1)$$

$$E_2 = \frac{1}{2} \varepsilon_{2r} \varepsilon_{2z} \exp [i(k_2 z + \varphi_2(z) - \omega_2 t)]. \quad (2)$$

二阶极化为

$$P_1 = d \varepsilon_{1r} \varepsilon_{1z} \varepsilon_{2r} \varepsilon_{2z} \exp i[(k_2 - k_1)z + \varphi_2(z) - \varphi_1(z) - (\omega_2 - \omega_1)t], \quad (3)$$

$$P_2 = d \varepsilon_{1r}^2 \varepsilon_{1z}^2 \exp [i(2k_1 z + 2\varphi_1(z) - 2\omega_1 t)]. \quad (4)$$

在柱坐标下的耦合波方程为

$$\frac{\varepsilon}{c^2} \frac{\partial^2 E_1}{\partial t^2} - \frac{4\pi}{c^2} \frac{\partial^2 P_1}{\partial t^2} = \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial E_1}{\partial r} \right) + \frac{\partial^2 E_1}{\partial z^2}, \quad (5)$$

$$\frac{\varepsilon}{c^2} \frac{\partial^2 E_2}{\partial t^2} - \frac{4\pi}{c^2} \frac{\partial^2 P_2}{\partial t^2} = \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial E_2}{\partial r} \right) + \frac{\partial^2 E_2}{\partial z^2}. \quad (6)$$

当略去二阶小量, 并令 $\theta = z \Delta k + \Delta \varphi = (2k_1 - k_2)z + (2\varphi_1 - \varphi_2)$, 则有

$$\frac{4\pi d \omega_1^2}{c^2} \varepsilon_{1r} \varepsilon_{1z} \varepsilon_{2r} \varepsilon_{2z} e^{-i\theta} = \frac{1}{2r} \frac{d\varepsilon_{1r}}{dr} \varepsilon_{1z} + ik_1 \frac{d\varepsilon_{1z}}{dz} \varepsilon_{1r} - k_1 \frac{d\varphi_1}{dz} \varepsilon_{1z} \varepsilon_{1r}, \quad (7)$$

$$\frac{4 \times 4\pi d \omega_1^2}{c^2} \varepsilon_{1r}^2 \varepsilon_{1z}^2 e^{i\theta} = \frac{1}{2r} \frac{d\varepsilon_{2r}}{dr} \varepsilon_{2z} + ik_2 \frac{d\varepsilon_{2z}}{dz} \varepsilon_{2r} - k_2 \frac{d\varphi_2}{dz} \varepsilon_{2r} \varepsilon_{2z}. \quad (8)$$

比较方程(7), (8)中的虚部和实部, 并令 $A = \frac{4\pi d \omega_1^2}{k_1 c^2}$, 则得

$$\frac{d\varepsilon_{1z}}{dz} = -A \varepsilon_{1z} \varepsilon_{2r} \varepsilon_{2z} \sin \theta, \quad (9)$$

$$\frac{d\varepsilon_{2z}}{dz} = 2A \frac{\varepsilon_{1r}^2 \varepsilon_{1z}^2}{\varepsilon_{2r}} \sin \theta, \quad (10)$$

$$\frac{d\theta}{dz} - \frac{\cos \theta}{\sin \theta} \left[\frac{d}{dz} (\ln(\varepsilon_{1z}^2 \varepsilon_{2z})) \right] = \Delta k + \frac{1}{4k_1 r} \frac{d}{dr} \left(\ln \frac{\varepsilon_{1r}^4}{\varepsilon_{2r}} \right). \quad (11)$$

显然, 方程(11)的左边只与 z 有关, 而右边只与 r 有关, 而 z 与 r 是独立的坐标变量, 所以必须等于同一常数, 即

$$\frac{d\theta}{dz} - \frac{\cos \theta}{\sin \theta} \frac{d}{dz} [\ln(\varepsilon_{1z}^2 \varepsilon_{2z})] = \Delta k + \frac{1}{4k_1 r} \frac{d}{dr} \left(\ln \frac{\varepsilon_{1r}^4}{\varepsilon_{2r}} \right) = \Gamma. \quad (12)$$

由(12)式可得

$$\varepsilon_{1r}^4 = c_1 \varepsilon_{2r} e^{2k_1(\Gamma - \Delta k)r^2}.$$

考虑到在腔内基波的自洽情况, 有理由认为 ε_{1r} 具有 $e^{-\frac{r^2}{W_0^2}}$ 的形式, 由此可得

$$\Gamma = \Delta k - \frac{2}{k_1 W_0^2}. \quad (13)$$

再由(12)式可得

$$\frac{d}{dz} [\ln(\varepsilon_{1z}^2 \varepsilon_{2z} \cos \theta)] = -\frac{\sin \theta}{\cos \theta} \cdot \Gamma. \quad (14)$$

解方程(14), 并注意到, 当 $z = \frac{L}{2}$ 时, $\varepsilon_{1z} = \varepsilon_{10z}$ 及 $\varepsilon_{2z} = 0$, 这样

$$\cos \theta = -\frac{\varepsilon_{2r} \cdot \varepsilon_{2z} \cdot \Gamma}{4A \varepsilon_{1z}^2 \varepsilon_{1r}},$$

$$\sin \theta = \pm \sqrt{1 - \frac{\Gamma^2}{16A^2} \cdot \frac{\varepsilon_{2r}^2 \varepsilon_{2z}^2}{\varepsilon_{1z}^4 \cdot \varepsilon_{1r}^4}} \quad (15)$$

将(15)式代入(10)式可得

$$\frac{d\varepsilon_{2z}}{dz} = \pm 2A \frac{\varepsilon_{1r}^2 \varepsilon_{1z}^2}{\varepsilon_{2r}} \sqrt{1 - \frac{\Gamma^2}{16A^2} \cdot \frac{\varepsilon_{2r}^2 \cdot \varepsilon_{2z}^2}{\varepsilon_{1z}^4 \cdot \varepsilon_{1r}^4}} \quad (16)$$

由 Manley-Rowe 关系, 可得

$$\varepsilon_{1z}^2 = \frac{-\varepsilon_{2r}^2 \varepsilon_{2z}^2}{2\varepsilon_{1r}^2} + \varepsilon_{10z}^2$$

代入(16)式得

$$2A dz = \frac{d\varepsilon_{2z}}{\sqrt{\varepsilon_{2z}^4 - b\varepsilon_{2z}^2 + c}} = \frac{d\varepsilon_{2z}}{\sqrt{(\varepsilon_{2z}^2 - p^2)(\varepsilon_{2z}^2 - q^2)}} \quad (17)$$

式中

$$b = \varepsilon_{1r}^2 \varepsilon_{10z}^2 + \Gamma/16A^2,$$

$$c = \varepsilon_{1r}^4 \varepsilon_{10z}^4 / \varepsilon_{2r}^2,$$

$$p = \frac{1}{2}(-b + \sqrt{b^2 - 4c}),$$

$$q = \frac{1}{2}(-b - \sqrt{b^2 - 4c}).$$

对方程(17)两边积分

$$2Az = \int_0^{\varepsilon_{2z}} \frac{d\varepsilon_{2z}}{\sqrt{(\varepsilon_{2z}^2 - p^2)(\varepsilon_{2z}^2 - q^2)}},$$

所以

$$2Az = \frac{1}{p} F\left(\frac{q}{p} \arcsin \frac{\varepsilon_{2z}}{q}\right). \quad (18)$$

二次谐波振幅 ε_{2z} 是双周期的亚纯函数,

$$\varepsilon_{2z} = \text{sn}(2Az, p, q). \quad (19)$$

由于 ε_{2z} 是 ε_{1r} 及 ε_{2r} 的函数, 以(19)式表示的 ε_{2z} 实际上表示的只是坐标 z 处, 径向坐标 r 处的值, 为了得到总的二次谐波功率, 必须对 r 从 0 到 ∞ 积分, 即

$$P_2(z) = \frac{cn}{2\pi} \int_0^\infty \varepsilon_{2z}^2 2\pi r dr = cn \int_0^\infty \text{sn}^2[2Az, p, q] r dr, \quad (20)$$

已知 ε_{1r} 及 ε_{2r} , 一般可用数值解求得 $P_2(z)$ 。

如果 $\Gamma=0$, 即 $\Delta k = \frac{2}{k_1 W_0^2}$, 可得

$$2Az = \frac{\frac{2}{\varepsilon_{2r}} d\varepsilon_{2z}}{\frac{2\varepsilon_{1r}^2 \cdot \varepsilon_{10z}^2}{\varepsilon_{2r}^2} - \varepsilon_{2z}^2},$$

$$\varepsilon_2(r, z) = \varepsilon_{2r} \varepsilon_{2z} = \sqrt{2} \cdot e^{-\frac{r^2}{W_0^2}} \varepsilon_{10z} \cdot \text{th}\left(\sqrt{2} AL \varepsilon_{10z} e^{-\frac{r^2}{W_0^2}}\right). \quad (21)$$

则二次谐波的功率为

$$P_2(z) = \frac{cn}{2\pi} \int_0^\infty 2\pi r |\varepsilon_2(r, z)|^2 dr = \frac{cnW_0^2}{2} \varepsilon_{10z}^2 - \frac{cnk_1 c^2 W_0^2 \varepsilon_{10z}}{4\sqrt{2} d\pi \omega_1^2 L} \text{th}\left(\frac{4\sqrt{2} d\pi \omega_1^2 L \varepsilon_{10z}}{k_1 c^2}\right) + \frac{cnk_1^3 c^4 W_0^2}{32d^3 \pi^3 \omega_1^4 L^3} \ln \text{ch}\left(\frac{4\sqrt{2} d\pi \omega_1^2 L \varepsilon_{10z}}{k_1 c^2}\right). \quad (22)$$

二、低转换效率近似

当转换效率不高时,可以认为基波在晶体内部没有衰减,即 $\varepsilon_1(z) = \varepsilon_{10z}$, 并假设基波和谐波的横向分布具有相同的高斯形式,并且可略去附加相移,这时基波和谐波可表示为

$$E_1 = \frac{1}{2} \varepsilon_{1z} e^{-\frac{r^2}{W_0^2}} \exp[i(k_1 z - \omega_1(t))],$$

$$E_2 = \frac{1}{2} \varepsilon_{2z} e^{-\frac{r^2}{W_0^2}} \exp[i(k_2 z - \omega_2(t))].$$

则耦合波方程为

$$\frac{d\varepsilon_2}{dz} = i \frac{2\varepsilon_2}{k_2} \left[\frac{r^2}{W_0^4} - \frac{1}{W_0^2} \right] - i \frac{16\pi d\omega_1^2}{c^3 k_2} \varepsilon_1^2 e^{-\frac{r^2}{W_0^2}} e^{i(\Delta k z)}, \quad (23)$$

令

$$N = \frac{2}{k_2} \left[\frac{r^2}{W_0^4} - \frac{1}{W_0^2} \right],$$

$$Q = -\frac{16\pi d\omega_1^2}{c^3 k_2} \varepsilon_1^2 e^{-\frac{r^2}{W_0^2}},$$

则(23)式可简化为

$$\frac{d\varepsilon_2}{dz} - iN\varepsilon_2 = iQe^{i(\Delta k z)}. \quad (24)$$

方程(24)的解为

$$\varepsilon_2(z) = \frac{Q}{\Delta k - N} \left[e^{i\Delta k z} - e^{i(N - \Delta k)\frac{L}{2} + 4Nz} \right],$$

所以

$$\varepsilon_2\left(\frac{L}{2}\right) = \frac{i16\pi d\omega_1^2 L}{c^3 k_2^2} \varepsilon_1^2 e^{-\frac{r^2}{W_0^2}} e^{4N\frac{L}{2}} \cdot \frac{\sin\left[(\Delta k - N)\frac{L}{2}\right]}{(\Delta k - N) \cdot \frac{L}{2}}. \quad (25)$$

当略去 $\frac{d^2\varepsilon_2}{dz^2}$ 的影响时,则

$$\Gamma' = \Delta k + \frac{2}{k_2} \cdot \frac{1}{W_0^2}, \quad (26)$$

所以

$$P_2 \Big|_{z=\frac{L}{2}} = \frac{cn}{2\pi} \int_0^\infty \left| E_2\left(r, \frac{L}{2}\right) \right|^2 2\pi r dr = \frac{64\pi^2 d^2 \omega_1^4 L^2 W_0^2 n}{c^3 k_2^2} \varepsilon_{10z}^4 \left[\frac{\sin\left(\Gamma' \frac{L}{2}\right)}{\Gamma' \frac{L}{2}} \right]^2. \quad (27)$$

如果 $\Gamma' = 0$, 我们则有 P_2 更简单的形式

$$P_2 \Big|_{z=\frac{L}{2}} = \frac{64\pi^2 d^2 \omega_1^4 L^2 W_0^2 n}{c^3 k_2^2} \varepsilon_{10z}^4. \quad (28)$$

公式(13)和(26)表示高斯光束由于倍频而引入的附加相位失配因子,在高及低转换效率下,它们具有相同的形式。当 $\Gamma = 0$, 存在这样一个光斑尺寸,即 $W_0 = \sqrt{\frac{2}{k_1 \Delta k}}$, 此时在倍频过程中,由于高斯光束的发散而引入的失配,可以由晶体取向的失配 Δk 来补偿。所以选择合适的光斑尺寸 W_0 是重要的。

三、类高斯光束的倍频

当一个激光器运转在混合模情况下, 它的光斑半径 $W_M(z)$ 可由基模高斯光束的光斑半径 $W(z)$ 和混合模系数 M 来表示^[5], $W_M(z) = MW(z)$, 这里 M 是仅取决于在激光器中运转的模序数的常数。

对于方镜腔

$$M^2 = \frac{\sum_m (2m+1) 2^m \cdot m!}{\sum_m 2^m \cdot m!} \quad \text{或} \quad M^2 = \frac{\sum_n (2n+1) 2^n \cdot n!}{\sum_n 2^n \cdot n!}, \quad (29)$$

对于圆镜腔

$$M^2 = \frac{\sum_m \sum_n (m+2n+1) \frac{(m+n)!}{n!}}{\sum_m \sum_n \frac{(m+n)!}{n!}}. \quad (30)$$

对于类高斯光束的倍频, 只需把上述公式中的 W_0 改变为 $MW(0)$ 即可, 这样就可以分别讨论 M 和 $W(0)$ 的影响。

四、考虑类高斯光束失配时的倍频处理方法

类高斯光束的基波场可写成

$$e_1 = e_0 \frac{W_0}{W(z)} e^{-\frac{r^2}{M^2 W^2(0)}} e^{-i\phi(r, z)}, \quad (31)$$

在平面波近似下, $W(0) \approx W(z)$, $\phi(r, z) \approx kr$ 所以

$$e_1 = e_0 e^{-\frac{r^2}{M^2 W^2(0)}} e^{-ik_1 r}. \quad (32)$$

耦合方程为

$$\frac{d e_2(r, z)}{dz} = -i \frac{8\pi\omega_2^2 d}{k_2 c^2} e_1^2(r) e^{-i\Delta k z}, \quad (33)$$

这里 Δk 是失配因子, 由文献[6]可得

$$\left. \begin{aligned} \Delta k &= A(\delta\zeta) \text{ (对于非 } 90^\circ \text{ 匹配),} \\ \Delta k &= A'(\delta\zeta)^2 \text{ (对于 } 90^\circ \text{ 匹配).} \end{aligned} \right\} \quad (34)$$

这里 $\delta\zeta$ 是失配角。光束光轴方向是精确的相位匹配方向, 光束的能流方向与光轴的夹角即为失配角, 当在非线性晶体内的双折射效应可以忽略时, 可近似地用波法线方向作为 $\delta\theta$, 由[5]可得

$$\delta\zeta = \frac{\lambda_1^2 r \beta}{\pi W^4(0) \beta} \left\{ 1 + \left[\frac{\lambda_1 z}{\pi W^2(0)} \right]^2 \right\}^{\left(\frac{1}{2\theta} - 1\right)}, \quad (35)$$

式中

$$\beta = \left| 1 - \frac{M^2 \lambda^2}{2\pi^2 W^2(0)} \right|. \quad (36)$$

在倍频晶体内部, $\left(\frac{\pi W^2(0)}{\lambda z}\right) \gg 1$, (35)式可简化为

$$\delta\theta = \frac{\lambda_1^2 r z}{n^2 \pi W^4(0) \beta}. \quad (37)$$

这样可以分别求解对于非 90° 匹配和 90° 匹配时的二次谐波振幅 $\varepsilon_2(r)$, 然后由 $P_2 = \frac{cn}{2\pi} \int_0^{M W(0)} |\varepsilon_2(r)|^2 2\pi r dr$ 求解二次谐波的功率 P_2 ,

对于非 90° 匹配:

$$P_2 = \frac{256\pi^2 \omega_0^4 d^2 \varepsilon_{10}^4 n}{k_2^2 c^3} \left[3.1 \times 10^{-2} M^2 W^2(0) L^2 - 3.7 \times 10^{-5} \frac{A^2 \lambda_1^4 L^6 M^4}{n^4 \pi^2 W^4(0) \beta^2} \right], \quad (38)$$

表 1

SHG				
	转换效率		失配因子	ε_2, P_2
平面波	低	①	$\Delta k = 0$	$\varepsilon_2 \propto \varepsilon_{10}^2, P_2 \propto \varepsilon_{10}^4$
		②	$\Delta k \neq 0$	$\varepsilon_2 \propto \varepsilon_{10}^2 \left(\frac{\sin \Delta k \cdot L/2}{\Delta k \cdot L/2} \right)^2, P_2 \propto \varepsilon_{10}^4 \left(\frac{\sin(\Delta k \cdot L/2)}{\Delta k \cdot L/2} \right)^2$
	高	③	$\Delta k = 0$	$\varepsilon_2 = \varepsilon_{10} \operatorname{th} \left(\frac{4\pi\omega_0^2 d \cdot L}{k_1 c^2} \varepsilon_{10} \right),$ $P_2 = \frac{cn}{2\pi} A' \varepsilon_{10}^2 = \frac{cn W_0^2}{2} \varepsilon_{10}^2 \operatorname{th}^2 \left(\frac{4\pi\omega_0^2 d \cdot L}{k_1 c^2} \varepsilon_{10} \right)$
类高斯的平面波近似	低	④	$\Delta k \neq 0$ $\Delta k = A\delta\theta$ $\Delta k = A'(\delta\theta)^2$	对于非 90° 匹配: $P_2 = \frac{256\pi^2 \omega_0^4 d^2 \varepsilon_{10}^4 n}{k_2^2 c^3} \left[3.1 \times 10^{-2} M^2 W^2(0) L^2 - 3.7 \times 10^{-5} \frac{A^2 \lambda_1^4 L^6 M^4}{n^4 \pi^2 W^4(0) \beta^2} \right] (W(z) = W(0), \phi(r, z) = kz)$ 对于 90° 匹配 $P_2 = 7.85 \frac{\pi^2 \omega_0^4 d^2 \varepsilon_{10}^4 n L^2 M^2 W^2(0)}{k_2^2 c^3}$
高斯和类高斯光束	低	⑤	$L'' = \Delta k - \frac{2}{k_2}$ $\left[\frac{r^2}{W_0^2} - \frac{1}{W_0^2} \right] = 0$	$P_2 = \frac{64\pi^2 d^2 \omega_0^4 L^2 W_0^2 n}{c^3 k_2^2} \varepsilon_{10}^4$
		⑥	$L'' \neq 0$	(1) $\left E_2 \left(r, \frac{L}{2} \right) \right ^2 = \frac{16\pi^2 d^2 \omega_0^4 L^2}{c^4 k_2^2} \varepsilon_{10}^4 e^{-\frac{r^2}{W_0^2}} \times \left[\frac{\sin[(\Delta k - N) \cdot L/2]}{(\Delta k - N) \cdot L/2} \right]^2$ $P_2 = \frac{cn}{2\pi} \int_0^\infty \left E_2 \left(r, \frac{L}{2} \right) \right ^2 2\pi r \cdot dr$ (2) 如果 $\frac{\partial^2 B}{\partial r^2} = 0, P_2 = \frac{64\pi^2 d^2 \omega_0^4 L^2 W_0^2 n}{c^3 k_2^2} \varepsilon_{10}^4 \times \left[\frac{\sin L'' \cdot L/2}{L'' \cdot L/2} \right]^2, (L'' = \Delta k - 2/k_2 \cdot W_0^2)$
	高	⑦	$L' = \Delta k - \frac{2}{k_1 W_0^2} = 0$	$\varepsilon_2(r, z) = \sqrt{\frac{2}{z}} e^{-\frac{r^2}{W_0^2}} \varepsilon_{10} \operatorname{th} \left(\sqrt{\frac{2}{z}} A L \varepsilon_{10} e^{-\frac{r^2}{W_0^2}} \right)$ $P_2(z) = \frac{cn W_0^2}{2} \varepsilon_{10}^2 - \frac{cn k_1 c^2 W_0^2 \varepsilon_{10}}{4\sqrt{2} d \pi \omega_0^2 L} \operatorname{th} \left[\frac{4\sqrt{2} d \pi \omega_0^2 L \varepsilon_{10}}{k_1 c^2} \right] + \frac{cn k_1^2 c^4 W_0^2}{32\pi^2 d^2 \omega_0^4 L^2} \ln \left[\frac{4\sqrt{2} d \omega_0^2 L \varepsilon_{10}}{k_1 c^2} \right]$
		⑧	$L' \neq 0$	$\varepsilon_2(z) = sn(2Az, p, q)$ $P_2(z) = cn \int_0^\infty sn^2(2Az, p, q) r dr \quad \left(\begin{matrix} \varepsilon_1, \varepsilon_2 = f(r) \cdot g(z) \\ \varepsilon_{1r} = \varepsilon_{1r_0} e^{-\frac{r^2}{W_0^2}} \end{matrix} \right)$

对于 90° 匹配:

$$P_2 = \frac{7.85\pi^2 \omega_2^4 d^2 \epsilon_0^4 n L^2 M^2 W^2(0)}{k_2^2 c^3} \quad (39)$$

表 1 列出了在各种条件下经过倍频晶体后二次谐波的功率 P_2 的表达式, 其中前三种情况取自文献, 后五种情况见本文推导。图 2, 图 3 示出了基波场振幅和晶体长度对 P_2 的影响, 所有曲线已由最大值归一化了。

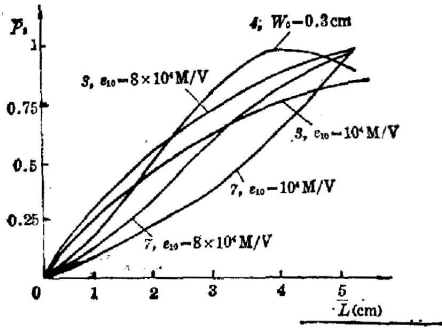


图 2

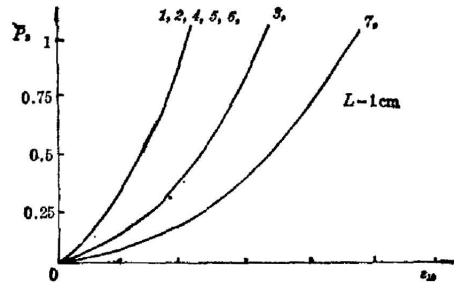


图 3

五、高转换效率下的内腔倍频

在我们的模型中 (见图 4), 视由于倍频过程对腔内循环的基波功率为一种随基波功率变化的可变损耗, 这样, Q 开关激光器中对基波而言的速率方程可表示为

$$\frac{dn_1}{dt} = -Bnq_1, \quad (40)$$

$$\frac{dq_1}{dt} = Bnq_1 - \alpha(t)q_1 - \Delta q(\epsilon_{10}, L). \quad (41)$$

方程(41)中 $\alpha(t)q_1$ 为损耗项, $\alpha(t)$ 为 Q 开关的开关函数。 $\Delta q(\epsilon_{10}, L)$ 项即为由于倍频过程的基波损耗项, 它应该是腔内循环的基波功率 ϵ_{10} , 腔参数及倍频晶体参数 (如长度 L , 失配 Δk , Γ 或 Γ' , 有效非线性系数等) 的函数。表 1 中前 7 种情况, P_2 都有解析表示式, 由此很容易导出 Δq 。如情况 ③, 可导出:

$$\Delta q = \frac{cq_1}{4L_0} \text{th}^2(2HL\sqrt{q_1}), \quad (42)$$

式中 L_c ——腔长, $H = 4\pi\omega d \sqrt{8\pi\hbar\omega}/cn_0$

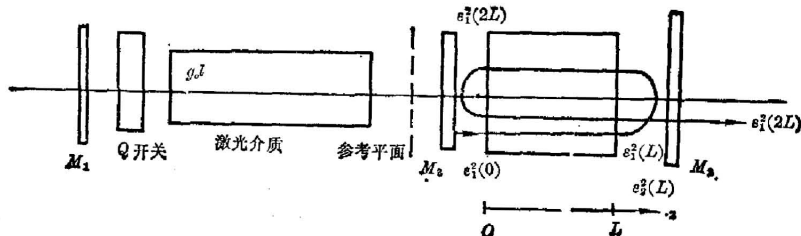


图 4

有了 Δq 的表示式,可求速率方程的数值解。作为一个例子,我们对表 1 中第 ③ 种情况求数值解,对象为一个声光 Q 开关的 YAG 激光器。设开关函数 $\alpha(t) = \alpha_0 + \alpha_1 e^{-t/\tau_s}$, $\sigma = 8.8 \times 10^{-19} \text{ cm}^2$, $\beta = \sigma \frac{c}{\gamma \tau} = 1.5 \times 10^{-5}$, $H = 3.8 \times 10^{-8}$, $L_0 = 60 \text{ cm}$, $\frac{c}{4L_0} = 1.25 \times 10^8$, 激光器速率方程简化为

$$\frac{dn_1}{dt} = 1.5 \times 10^{-8} n_1 q_1, \tag{43}$$

$$\frac{dq_1}{dt} = 1.5 \times 10^{-8} n_1 q_1 - \alpha(t) q_1 - 1.25 \times 10^{-8} q \text{th}^2(3.8 \times 10^{-8} L \sqrt{q_1}). \tag{44}$$

然后 n_1 和 q_1 分别用 N_0 和 q_m 归一化

$$N_0 = 0.01 \gamma n_0, \quad \text{取 } n_0 = 1.386 \times 10^{20} / \text{cm}^3,$$

这样归一化速率方程为

$$\frac{d\bar{n}}{dt} = -0.21 \bar{n} \bar{q}, \tag{45}$$

$$\frac{d\bar{q}}{dt} = 21 \gamma \bar{n} \bar{q} - \alpha(t) 10^{-9} \bar{q} - 0.125 \bar{q} \text{th}^2(9L \sqrt{\bar{q}}). \tag{46}$$

数值解的主要结果示于图 5~图 8。图 5 为不同晶体长度时光子数密度随时间的变化。图 6, 图 7 分别为不同损耗系数时,二次谐波脉冲和能量随晶体长度的变化。由此可见在一定晶体长度下,有最大输出能量,此时具有较小的脉宽,由此可选出最佳晶体长度。图 8 表示脉宽 τ_2 随腔长 L_0 的变化,内腔倍频的规律与常规 Q 开关不同。由图可见,在结构允许情况下,应适当增加腔长。

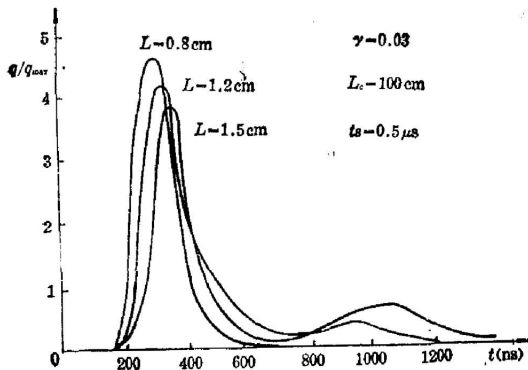


图 5

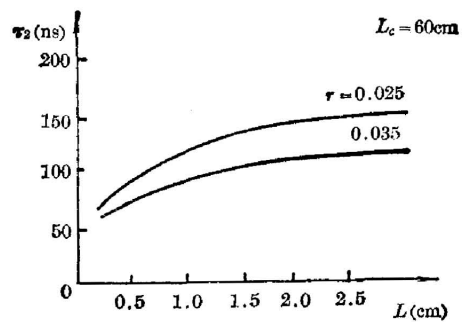


图 6

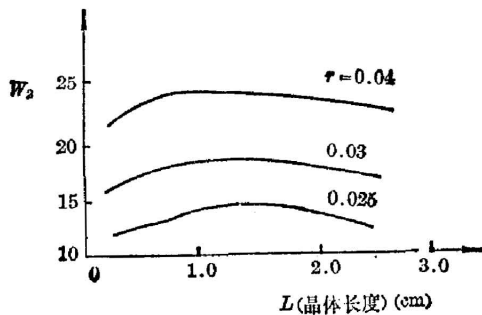


图 7

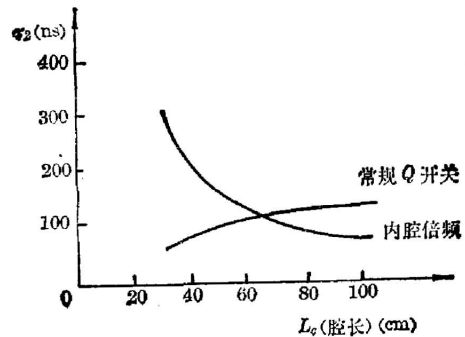


图 8

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Intracavity frequency doubling with Gaussian and Gaussian-Like beam at high conversion efficiency*

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Abstract

This paper presents some valuable results of frequency doubling, considering the transversal variation of the amplitude and the depletion of the fundamental wave power. By solving three dimension-coupling wave equation, the most common expressions of second harmonic wave power are driven. The influences of the fundamental wave power and the crystal length are discussed. As a special example the expressions of second harmonic wave power at low conversion efficiency are given.

As a summary, eight expressions of the second harmonic wave power at different cases are listed, in which five cases come from this paper.

Finally, a new way of dealing with the intracavity frequency doubled laser is given. In our model the power loss due to SHG is considered as a viriable loss for the fundamental wave power which is circulating in the cavity. By solving the rate equations numerically, the optimum parameters of the cavity and of the frequency doubling crystal are found.

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