## Broadband and polarization-insensitive subwavelength grating reflector for the near-infrared region

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We propose a polarization-insensitive and broadband subwavelength grating reflector based on a multilayer structure. The reflector has an overlapped high reflectivity (>99.5%) bandwidth of 248 nm between the TE and the TM polarizations, which is much higher than the previously reported results. We believe this subwavelength grating reflector can be applied to unpolarized devices.

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Subwavelength gratings have attracted enormous attention theoretically and experimentally in the past few years [1-5]. Due to the elimination of non-zero order diffraction according to the grating equation, subwavelength gratings are promising for many integrated optoelectronic applications such as polarizers<sup>[1]</sup>, couplers<sup>[2]</sup>, filters<sup>[1,3]</sup>, absorbers<sup>[4]</sup>, and reflectors<sup>[5]</sup>. Besides, when surrounded by low-index material, they will demonstrate a high reflectivity over a broad wavelength range, which are so-called high-index-contrast subwavelength grating (HCG) reflectors<sup>[5-8]</sup>. They can be applied to the vertical-cavity surface-emitting lasers (VCSELs) to replace the traditional distributed Bragg reflectors (DBRs) which are bulky and difficult to fabricate<sup>[6-8]</sup></sup>. Moreover, with a shortened cavity, HCG-VCSELs have many new properties, such as the single-mode operation and hightuning speed<sup>[8]</sup>. Additionally, with the progress of tunable VCSEL<sup>[9]</sup>, broadband property becomes more desirable. However, subwavelength gratings are polarizationselective inherently, thus they cannot be applied to light demultiplexing<sup>[10]</sup>, unpolarized lasers, or detectors.

Recently, Wu et al. reported a high performance polarization independent reflector based on a multilayered configuration grating structure<sup>[11]</sup>. The reflector demonstrated a high reflection (R > 99%) from 1.57 to 1.8  $\mu$ m. However, the multi-subpart profile will bring considerable difficulties to the practical fabrication. We also demonstrated a polarization insensitive subwavelength grating reflector based on a semiconductor-insulatormetal structure. The reflector demonstrated an 89-nm overlapped high reflectivity (> 99.5%) bandwidth<sup>[5]</sup>. The mechanism of polarization-insensitivity was mainly attributed to the combined effect of HCG and metallic subwavelength grating with the insertion of insulator layer. However, the bandwidth can be further broadened by the redshift of the TM polarization reflectance spectra while increasing the reflectivity of both polarizations. In this letter, we propose a broadband and polarization-insensitive subwavelength grating reflector for the near-infrared region.

As shown in Fig. 1, the structure has a multilayered configuration, which is consisted of an  $Al_{0.6}Ga_{0.4}As$  layer, a silica layer, an Au layer, a silica layer, and an Au layer from bottom to top, respectively. The refractive indexes for Al<sub>0.6</sub>Ga<sub>0.4</sub>As and silica are 3.2 and 1.47, respectively. The Drude model<sup>[12]</sup> is taken to depict the dispersion information of Au. The device is normally illuminated by a plane wave with both TE and TM polarized components, and is highly reflective in the zeroth order. The key parameters to be optimized are marked in Fig. 1, where the thicknesses of the layers from bottom to up, the period of subwavelength grating and the width of un-etched part are denoted as  $T_1$ ,  $T_2$ ,  $T_3$ ,  $T_4$ ,  $T_5$ ,  $\Lambda$ , and d, respectively. The rigorous coupled-wave analysis (RCWA)<sup>[13,14]</sup> method is used to calculate the reflectance spectra.

Compared with the structure in Ref. [5], we insert a layer of silica grating and a layer of Au grating between the Al<sub>0.6</sub>Ga<sub>0.4</sub>As grating layer and silica grating layer with the other parameters unchanged. By increasing the thickness of the silica grating layer, the wavelength of constructive interference<sup>[15]</sup> for TM polarization light will become longer. The shifts of wavelength are represented by the shift of point 'A' in Fig. 2(a), which is at the bottom of TM polarization reflectance spectra. As to the TE polarization light, its wavelength shift will be represented by the shift of point 'B' in Fig. 2(a), which is at the bottom of the TE polarization reflectance spectra. The shifts of point 'A' and point 'B' with the increase of  $T_2$  are demonstrated in Figs. 2(b) and (c), respectively. It can be seen that point 'B' moves slower than point 'A'. This can be explained by the relatively low reflectivity of



Fig. 1. Schematic configuration of our proposed structure.



Fig. 2 (a) Reflectance spectra after inserting two layers. Positions of points (b) 'A' and (c) 'B' with the increase of  $T_2$ .



Fig. 3 Variation of overlapped bandwidth versus (a) the thickness of the first silica grating layer  $T_2$  when  $T_1=235$  nm,  $T_3=100$  nm,  $T_4=400$  nm,  $T_5=100$  nm, FF=0.7; (b) the thickness of the first Au grating layer  $T_3$  with  $T_2$  already optimized; (c) the thickness of the second silica grating layer with  $T_2$  and  $T_3$  already optimized; (d) the thickness of second Au grating layer with  $T_2$ ,  $T_3$ , and  $T_4$  already optimized; (e) the thickness of Al<sub>0.6</sub>Ga<sub>0.4</sub>As grating layer with  $T_2$ ,  $T_3$ ,  $T_4$ ,  $T_5$  already optimized; (f) FF.

one-dimensional semiconductor material grating for TE polarization light<sup>[16]</sup>. Besides, from the equation

$$2 \times n_{\text{eff}} \times \Delta T_2 = N \times \Delta \lambda,\tag{1}$$

where the refractive index of silica  $n_{\rm eff}=1.47$ ;  $\Delta\lambda$  and  $\Delta T_2$  are the differences of  $\lambda$  and  $T_2$ , respectively; N is an integer. The calculated slope  $(\Delta\lambda/\Delta T_2)$  is 0.98 when N is equal to 3. This value is very close to the result given by RCWA method, which is 0.89 after curve fitting. The

little difference between them can be explained that only part of the TM polarization light is involved in the interference.

We further scan and optimize the key parameters including  $T_1$ ,  $T_2$ ,  $T_3$ ,  $T_4$ ,  $T_5$ , and FF defined by  $d/\Lambda$ . The period is kept unchanged. Additionally, the bandwidth presented in Fig. 3 is the result after multiplied by a proper constant to maximize the bandwidth within the range of  $0.7-1 \,\mu\text{m}$  according to the scale effect of photonic crystals<sup>[17]</sup>. For example, if the overlapped bandwidth is  $0.8-1.1 \,\mu\text{m}$ , then the dimensions of the reflector will be multiplied by 1/1.1 with the other paramets unchanged. As a result, the overlapped bandwidth will shift to  $0.727-1 \,\mu\text{m}$ , within the range of  $0.7-1 \,\mu\text{m}$ .

The scanned results for  $T_1$ ,  $T_2$ ,  $T_3$ ,  $T_4$ ,  $T_5$ , and FF are demonstrated in Fig. 3. When the biggest overlapped bandwidth is achieved, the optimal values for these parameters are 0.235 µm, 0.170 µm, 0.130 µm, 0.170 µm,  $0.120 \ \mu m$ , and 0.8, respectively. And the overlapped bandwidth is 0.800-0.884 and  $0.902-1.081 \ \mu m$ . After multiplying the dimensions of the reflector by 1/1.081, the period,  $T_1$ ,  $T_2$ ,  $T_3$ ,  $T_4$ ,  $T_5$ , and FF now are 0.352  $\mu$ m,  $0.217 \ \mu m$ ,  $0.157 \ \mu m$ ,  $0.120 \ \mu m$ ,  $0.157 \ \mu m$ ,  $0.130 \ \mu m$ , and 0.8, respectively. The overlapped bandwidth are 248 nm, ranging from 0.740 to 0.818  $\mu$ m and 0.834 to 1  $\mu$ m, as shown in Fig. 4. The absorptance spectra and transmittance spectra are also demonstrated in Fig. 4. It can be seen that although some absorption loss exists in the range of  $0.7-1 \,\mu\text{m}$ , the transmission loss is almost negligible. Besides, the absorption loss is below 0.5% in most wavelength region from 0.7 to 1  $\mu$ m.

In conclusion, we demonstrate a subwavelength grating reflector based on a multilayer configuration. Compared to the previous works, layers of silica grating and Au grating are inserted between the original  $Al_{0.6}Ga_{0.4}As$  grating layer and silica grating layer. As a result, the overlapped bandwidth between the TE and TM polarization lights reaches 248 nm, which means the reflector is polarization-insensitive for the wavelength from 0.74 to 0.818  $\mu$ m and from 0.834 to 1  $\mu$ m. We believe that this subwavelength grating reflector can replace the top DBR of single-mode unpolarized VCSEL, and can also be applied to other unpolarized devices.

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Fig. 4. Simulation results of our structure.

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