

Three-dimensional optical logic devices using spatial multiwaveguide system

Jianxia Pan (潘剑侠)¹ and Yiling Sun (孙一翎)²

¹Electronic Information Institute, Hangzhou Dianzi University, Hangzhou 310018

²College of Optical and Electronic Science, China Jiliang University, Hangzhou 310018

Received October 8, 2007

Based on the weakly coupled-mode theory, the coupled-mode equations of the spatial multiwaveguide system are presented in general. The intensity distribution in each waveguide is determined by numerical method. Optical logic devices based on spatial multiwaveguide system are proposed. The analysis results show that the spatial multiwaveguide system permits different Boolean logic states obtained by phase modulation. Applications of the logic devices include optical calculation, optical interconnection, and spatial optical signal processing.

OCIS codes: 130.3120, 130.3750, 230.7370.

Up to now, most of integrated optical waveguide devices are realized in planar structures^[1,2], which means that these devices can only be applied to process the input/output signal through one-dimensional (1D) interconnect channels. In fact, many applications, such as large data streams, image manipulation, artificial vision, nerve networks and optical calculation, need two-dimensional (2D) spatial optical signal processing. To meet these demands, we should develop integrated optical devices employing three-dimensional (3D) structures^[3,4], which exhibit a higher level of integration. Several 3D integrated optical devices have been successfully implemented, such as vertical waveguide power splitters^[4], 3D optical switches^[5], modulators^[6], spatial logic coders^[7] by using thermo-optic and electro-optic effects.

Waveguides on different planes, which are called spatial multiwaveguide system in this paper, have been incorporated into many 3D integrated optics devices^[5,6]. The coupled-mode theory^[8] presented a general analytical means for traditional planar directional couplers composed of two waveguides in the same plane, and the coupled properties of planar three-waveguide and multiwaveguide systems were also discussed in Refs. [9] and [10], respectively.

In this paper, we apply the weakly coupled-mode theory to analyze the modulation properties of spatial

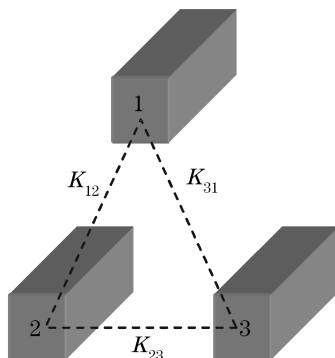


Fig. 1. Schematic diagram of spatial three-waveguide system.

multimode-waveguide system and describe the power transfer among these spatial waveguides by simultaneous differential equations. Optical spatial logic devices are designed based on the analytical results. We consider a spatial 3D system formed by three waveguides, as shown in Fig. 1. The coupled-mode equations for the spatial three-waveguide with propagation along the z -direction can be described as follows^[9]:

$$\frac{\partial A_1}{\partial z} = iK_{12}A_2 \exp(-i\Delta\beta_1 z) + iK_{31}A_3 \exp(i\Delta\beta_3 z - i\Delta\beta_1 z), \quad (1a)$$

$$\frac{\partial A_2}{\partial z} = iK_{12}A_1 \exp(i\Delta\beta_1 z) + iK_{23}A_3 \exp(i\Delta\beta_3 z), \quad (1b)$$

$$\frac{\partial A_3}{\partial z} = iK_{31}A_1 \exp(i\Delta\beta_1 z - i\Delta\beta_3 z) + iK_{23}A_2 \exp(-i\Delta\beta_3 z), \quad (1c)$$

where A_i ($i = 1, 2, 3$) is the amplitude of the field in each waveguide. K_{jl} ($j, l = 1, 2, 3$) is the coupling coefficient between waveguide j and waveguide l , which is a function of the separation distance between the waveguides and the distribution of refractive index distribution. β_i ($i = 1, 2, 3$) is the propagation constant of each waveguide. $\Delta\beta_1$ and $\Delta\beta_3$ are detuning of β_1 and β_3 from β_2 , respectively.

$$\Delta\beta_1 = \beta_1 - \beta_2, \quad (2a)$$

$$\Delta\beta_3 = \beta_3 - \beta_2. \quad (2b)$$

For mathematical simplicity, we use

$$a_1 = A_1 \exp(i\Delta\beta_1 z), \quad (3a)$$

$$a_2 = A_2, \quad (3b)$$

$$a_3 = A_3 \exp(i\Delta\beta_3 z), \quad (3c)$$

which yield

$$\frac{\partial}{\partial z} \begin{bmatrix} a_1 \\ a_2 \\ a_3 \end{bmatrix} = i \begin{bmatrix} \Delta\beta_1 & K_{12} & K_{31} \\ K_{12} & 0 & K_{23} \\ K_{31} & K_{23} & \Delta\beta_3 \end{bmatrix} \begin{bmatrix} a_1 \\ a_2 \\ a_3 \end{bmatrix}. \quad (4)$$

The matrix equation can be used to solve the weakly coupled problem of the spatial three-waveguide system and predict the intensity distribution in each waveguide.

Assuming the eigenvalues of the matrix $\begin{bmatrix} \Delta\beta_1 & K_{12} & K_{31} \\ K_{12} & 0 & K_{23} \\ K_{31} & K_{23} & \Delta\beta_3 \end{bmatrix}$ are β_1 , β_2 , and β_3 , respec-

tively, and the corresponding eigenvectors are $\begin{pmatrix} v_{11} \\ v_{12} \\ v_{13} \end{pmatrix}$,

$\begin{pmatrix} v_{21} \\ v_{22} \\ v_{23} \end{pmatrix}$, $\begin{pmatrix} v_{31} \\ v_{32} \\ v_{33} \end{pmatrix}$, respectively. The solution to Eq. (4) can be written as

$$\begin{bmatrix} a_1(z) \\ a_2(z) \\ a_3(z) \end{bmatrix} = \begin{pmatrix} v_{11} & v_{21} & v_{31} \\ v_{12} & v_{22} & v_{32} \\ v_{13} & v_{23} & v_{33} \end{pmatrix} \times \begin{bmatrix} e^{i\beta_1 z} & 0 & 0 \\ 0 & e^{i\beta_2 z} & 0 \\ 0 & 0 & e^{i\beta_3 z} \end{bmatrix} \begin{bmatrix} B_1 \\ B_2 \\ B_3 \end{bmatrix}, \quad (5)$$

where B_1 , B_2 , and B_3 are the undetermined coefficients, which can be determined by the following equation:

$$\begin{bmatrix} B_1 \\ B_2 \\ B_3 \end{bmatrix} = \begin{pmatrix} v_{11} & v_{21} & v_{31} \\ v_{12} & v_{22} & v_{32} \\ v_{13} & v_{23} & v_{33} \end{pmatrix}^{-1} \cdot \begin{bmatrix} a_1(0) \\ a_2(0) \\ a_3(0) \end{bmatrix}, \quad (6)$$

where $[a_1(0) \ a_2(0) \ a_3(0)]^T$ is the initial condition. The intensity distribution in each waveguide under different initial conditions and detuning parameters can be determined by Eqs. (5) and (6).

If the light power is injected into waveguide 1, the initial conditions will be

$$A_1(0) = 1, \quad A_2(0) = A_3(0) = 0. \quad (7)$$

Assuming $K_{12} = 0.001$, $K_{23} = 0.0015$, $K_{31} = 0.0015$, the length of three identical waveguides z is $\pi/0.003$. Solving the simultaneous differential equations, we can get seven different logic states under different modulation parameters. In the case of $\Delta\beta_1 = -0.018$, $\Delta\beta_3 = 0.03$, the input optical power is completely switched to the waveguide 1. For

$$\begin{bmatrix} |a_1(z)|^2 \\ |a_2(z)|^2 \\ |a_3(z)|^2 \end{bmatrix} = \begin{bmatrix} 0.9999 \\ 0.0000 \\ 0.0001 \end{bmatrix}, \quad (8)$$

this case corresponds to the logic state [100]. We define the extinction ratio ER between the final outputs as

$$\text{ER} = 10 \log \left[\frac{P_{\text{“ON” state}}^{\min}}{P_{\text{“OFF” state}}^{\max}} \right], \quad (9)$$

where $P_{\text{“ON” state}}^{\min}$ is the minimal optical power and $P_{\text{“OFF” state}}^{\max}$ is the maximal optical power. Using the above definition, the extinction ratio ER = 40 dB.

In the case of $\Delta\beta_1 = 0$ and $\Delta\beta_3 = -0.003$, the input optical power is completely switched to the waveguide 2. This case corresponds to the logic state [010], and the

extinction ratio ER = 27 dB. For

$$\begin{bmatrix} |a_1(z)|^2 \\ |a_2(z)|^2 \\ |a_3(z)|^2 \end{bmatrix} = \begin{bmatrix} 0.001 \\ 0.997 \\ 0.002 \end{bmatrix}, \quad (10)$$

in the case of $\Delta\beta_1 = -0.0439$ and $\Delta\beta_3 = -0.0439$, the input optical power is completely switched to the waveguide 3. This case corresponds to the logic state [001], and the extinction ratio ER = 27 dB. For

$$\begin{bmatrix} |a_1(z)|^2 \\ |a_2(z)|^2 \\ |a_3(z)|^2 \end{bmatrix} = \begin{bmatrix} 0.002 \\ 0.000 \\ 0.998 \end{bmatrix}, \quad (11)$$

in the case of $\Delta\beta_1 = 0.008$ and $\Delta\beta_3 = 0.0102$, the input optical power is equally divided between the waveguide 1 and waveguide 3. This case corresponds to the logic state [101], and the extinction ratio ER = 27 dB. For

$$\begin{bmatrix} |a_1(z)|^2 \\ |a_2(z)|^2 \\ |a_3(z)|^2 \end{bmatrix} = \begin{bmatrix} 0.500 \\ 0.001 \\ 0.499 \end{bmatrix}, \quad (12)$$

in the case of $\Delta\beta_1 = 0.0022$ and $\Delta\beta_3 = -0.0215$, the input optical power is equally divided between the waveguide 1 and waveguide 2. This case corresponds to the logic state [110], and the extinction ratio ER = 24 dB. For

$$\begin{bmatrix} |a_1(z)|^2 \\ |a_2(z)|^2 \\ |a_3(z)|^2 \end{bmatrix} = \begin{bmatrix} 0.498 \\ 0.500 \\ 0.002 \end{bmatrix}, \quad (13)$$

in the case of $\Delta\beta_1 = 0.0018$ and $\Delta\beta_3 = 0.0004$, the input optical power is equally divided between the waveguide 2 and waveguide 3. This case corresponds to the logic state [011], and the extinction ratio ER = 7.1 dB. For

$$\begin{bmatrix} |a_1(z)|^2 \\ |a_2(z)|^2 \\ |a_3(z)|^2 \end{bmatrix} = \begin{bmatrix} 0.090 \\ 0.463 \\ 0.447 \end{bmatrix}, \quad (14)$$

in the case of $\Delta\beta_1 = 0.0002$ and $\Delta\beta_3 = 0.0005$, the input optical power is equally distributed among three waveguides. This case corresponds to the logic state [111], and the outputs are all “ON” states. For

$$\begin{bmatrix} |a_1(z)|^2 \\ |a_2(z)|^2 \\ |a_3(z)|^2 \end{bmatrix} = \begin{bmatrix} 0.327 \\ 0.338 \\ 0.335 \end{bmatrix}, \quad (15)$$

the analysis results show that the spatial multiwaveguide system permits different Boolean logic states obtained by phase modulation.

In this paper, optical logic devices based on spatial multiwaveguide system are proposed. The intensity distribution in each waveguide is determined by numerical method. The analysis results show that the optical logic device permits different Boolean logic states obtained by phase modulation. The extinction ratio between the minimum power of “ON” state and the maximum power of “OFF” state can reach 7.1 dB. Applications of the logic devices include optical calculation, optical interconnection, and spatial optical signal processing.

This work was supported by the Key Science and Technology Program of Zhejiang Province under Grant No. 2007C11069. Y. Sun is the author to whom the correspondence should be addressed, his e-mail address is sunyl@cjlu.edu.cn.

References

1. L. Li, Y. Tang, J. Yang, M. Wang, and X. Jiang, *Chin. Opt. Lett.* **4**, 93 (2006).
2. J. Wu, B. Shi, and M. Kong, *Chin. Opt. Lett.* **4**, 167 (2006).
3. C. Wächter, Th. Hennig, Th. Bauer, A. Bräuer, and W. Karthe, *Proc. SPIE* **3278**, 102 (1998).
4. S. M. Garner, S.-S. Lee, V. Chuyanov, A. Chen, A. Yacoubian, W. H. Steier, and L.R. Dalton, *IEEE J. Quantum Electron.* **35**, 1146 (1999).
5. C. Wächter, Th. Bauer, M. Cumme, P. Dannberg, W. Elflein, Th. Henning, U. Streppel, and W. Karthe, *Proc. SPIE* **3936**, 130 (2000).
6. M. Hikita, Y. Shuto, M. Amano, R. Yoshimura, S. Tomaru, and H. Kozawaguchi, *Appl. Phys. Lett.* **63**, 1161 (1993).
7. H.-F. Zhou, J.-Y. Yang, M.-H. Wang, and X.-Q. Jiang, *Chin. Phys.* **16**, 740 (2007).
8. W.-P. Huang, *J. Opt. Soc. Am. A* **11**, 963 (1994).
9. C.-M. Kim and Y.-J. Im, *IEEE J. Sel. Top. Quantum Electron.* **6**, 170 (2000).
10. S. Srivastava and E. K. Sharma, *J. Opt. Soc. Am. A* **13**, 1683 (1996).