

The light waveforms are shown in Fig. 3. Supposing that the light waveform of laser diode (LD) is like “a” and “b” is the modulating signal (RZ) of PM, the output light waveform of PM is like “c”. After transmitting through the long distance fiber, the light is split into two arms. The waveform of arm 1 in Fig. 1 is like “d” if $\Delta\rho$ is 0 and the waveform of arm 2 is like “e” which is delayed from “d” for a half of bit. Two waveforms combine to form waveform “f”. If $\Delta\phi$ is 180 in arm 1, then the waveform of arm 1 is like “g” and “h” is same as “e”. The waveform “g” and “h” will interfere to form waveform “j”. It is clear that waveform “j” is reverse to waveform “f” so that the device “ $\Delta\rho$ ” in Fig.1 can be deleted in practice. After the photodiode transforms the light waveform into electric signal, the signal of high frequency is filtered out and the initial information can be recovered. Because the waveform “j” is same as NRZ form of the signal “b” if the high frequency is filtered.

The simulation setup is shown in Fig. 4. Scopes are used to show waveform of the controlling signal of PM and the output waveform of receiver. PRBS generates 40-GHz random signals which is NRZ form and will be changed into RZ signal to control the PM. The fiber length is 3000 km and delay time τ is 0.125×10^{-10} s. We

can change the value of $\Delta\rho$ to see the difference results.

When the waveform of the “RZ” input signal is like Fig. 5(a), then the waveform of the controlling signal of PM is like Fig. 5(b). When the value of $\Delta\rho$ equals to 180, the output waveform of receiver is shown in Fig. 5(c) and when the value of $\Delta\rho$ equals to 0, the output waveform of receiver is shown in Fig. 5(d). Here, it is clear that the transmitting signal (NRZ form) is 1100 1010 1011 0111 1100 1111 1100 0000 0111. Of course, the waveform of Fig. 5(c) is near as that of (a) and the waveform of Fig. 5(d) is just reversed as that of (a).

Figure 6 shows the eye diagrams of input signal (a) and output signal (b). All above results show us that NMD-PSK format works successfully.

In conclusion, NMD-PSK format, with higher optical noise tolerance and output signal superior nonlinear tolerance, can be one of the optimum modulation format for spectrally efficient ultralong-haul 40-Gb/s DWDM transmission systems. It is also simple and practical. But, At the transition point from 0 to 1 and 1 to 0, the PSK signal phase changes rapidly from 0 to π and π to 0. This rapid phase change can cause the frequency chirping. We can reduce the effects of the frequency chirping

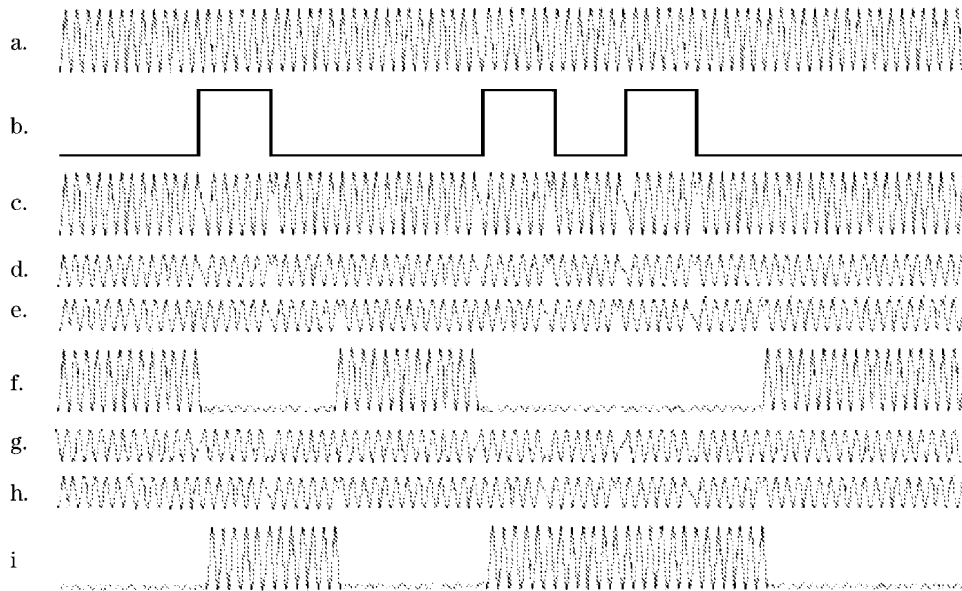


Fig. 3. The light waveforms of NMD-PSK.

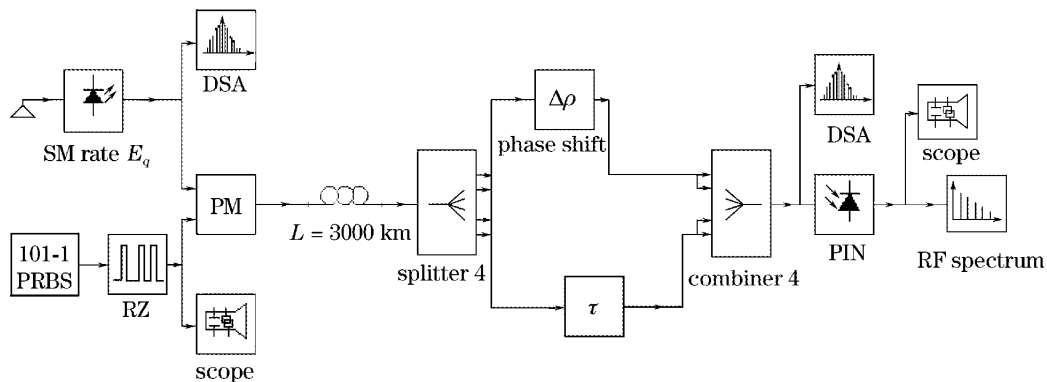


Fig. 4. The simulation setup of NMD-PSK.

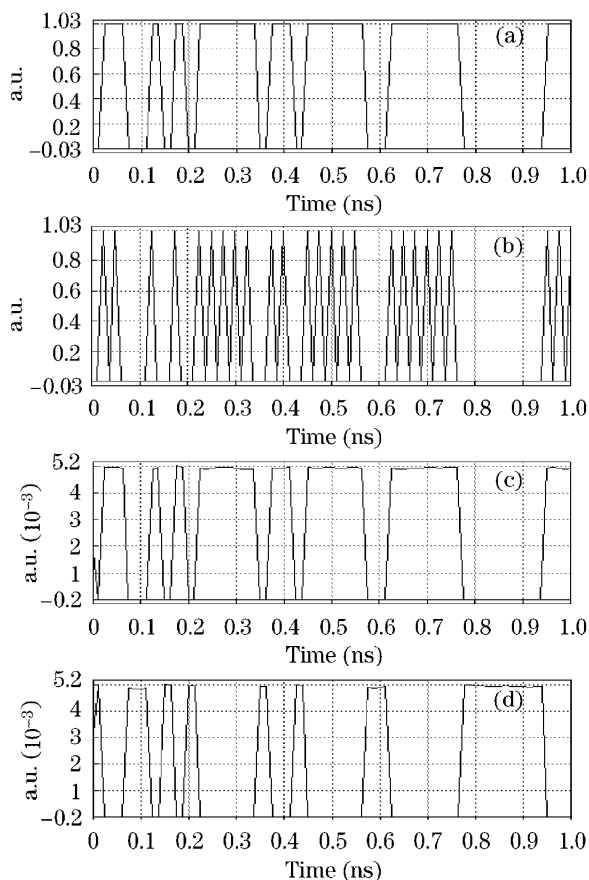


Fig. 5. The simulation results. (a) "RZ" Input waveform; (b) "RZ" output waveform; (c) "PIN" output waveform when $\Delta\rho = 180$; (d) "PIN" output waveform when $\Delta\rho = 0$.

by using the other intensity modulator which remodulates the signal to suppress such waveform degradation^[4].

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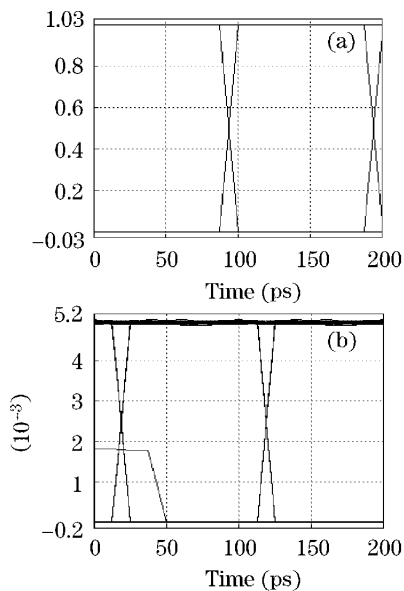


Fig. 6. The eye diagrams of input (a) and output (b) signal.

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References

1. J. Leibrich, C. Wree, and W. Rosenkranz, *IEEE Photon. Technol. Lett.* **14**, 155 (2002).
2. C. Xu, X. Liu, L. F. Mollenauer, and X. Wei, *IEEE Photon. Technol. Lett.* **15**, 617 (2003).
3. D. Penninckx, H. Bissessur, P. Brindel, E. Gohin, and F. Bakhti, in *Proceedings of ECOC'01* 456 (2001).
4. T. Hoshida, O. Vassilieva, K. Yamada, S. Chhouchary, R. Pecqueur, and H. Kuwahara, *J. Lightwave Technol.* **20**, 1989 (2002).