

基于泵浦分束的波长可调谐 1  $\mu\text{m}$  超短脉冲光纤激光器

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**摘要** 利用啁啾脉冲增益饱和放大特性, 搭建了一台基于泵浦分束结构的波长可调谐 1  $\mu\text{m}$  全保偏光纤超短脉冲激光器。该激光器由超短脉冲激光振荡器和超短脉冲激光放大器组成, 控制注入到放大器的啁啾脉冲能量, 使放大器处于增益饱和或非饱和状态, 从而实现激光中心波长的精确调节。实验中, 激光器可产生 1030.0~1034.5 nm 波长可调谐的超短脉冲激光, 光谱带宽大于 13.1 nm。在整个波长调谐范围内, 放大脉冲激光的信噪比均大于 55 dB, 时域脉宽为 7.1~7.5 ps。此外, 得益于全保偏光纤架构, 该 1  $\mu\text{m}$  超短脉冲光源表现出良好的长期稳定性, 平均功率的相对抖动低至 0.1%。该激光器产生的波长可调谐超短脉冲激光, 能够精准匹配 Yb:YAG、Yb:CaF<sub>2</sub>、Yb:Lu<sub>2</sub>O<sub>3</sub> 等晶体的发射峰, 可为后续 Yb:YAG、Yb:CaF<sub>2</sub>、Yb:Lu<sub>2</sub>O<sub>3</sub> 等大能量超短脉冲固体激光器提供紧凑、便捷、稳定的种子光源。

**关键词** 激光器; 光纤激光器; 超短脉冲; 泵浦分束; 波长可调谐

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## 1 引言

1  $\mu\text{m}$  波长可调谐超短脉冲光纤激光器不仅可应用在激光光谱学、光学测量、生物医学等领域<sup>[1-5]</sup>, 还可用作超短脉冲固体激光器的种子源<sup>[6-7]</sup>, 可精准匹配不同增益介质的发射峰。目前超短脉冲光纤激光器主要依赖锁模技术, 包括非线性偏振演化(NPE)<sup>[8-9]</sup>、非线性光纤放大环形镜(NALM)<sup>[10-11]</sup>、半导体可饱和吸收镜(SESAM)<sup>[12-14]</sup>等。波长可调谐 1  $\mu\text{m}$  超短脉冲激光器基于这些锁模技术, 添加了相应的波长可调谐技术, 例如干涉效应、光栅、带通可调谐滤波器等。2011年, Zhu等<sup>[15]</sup>利用相移长周期光纤光栅, 搭建了基于NPE锁模机制的掺镱光纤激光器, 基于弯曲的光纤光栅, 实现了波长为 1028.28~1039.1 nm 的窄带脉冲激光输出。2012年, Agnesi等<sup>[16]</sup>搭建了工作在正色散区域的锁模掺镱光纤激光器, 通过在腔内引入 Littrow 结构的光栅, 实现了光谱滤波, 从而获得了波长在 1015~1085 nm 范围内的窄带锁模脉冲输出。2012年, 白扬博等<sup>[17]</sup>利用反射型体光栅搭建了基于 SESAM 锁模结构的 1  $\mu\text{m}$  波段光纤激光器, 实现了中心波长在 1011.9~1050.6 nm 范围内的连续可调谐, 中心波长 1030 nm 处的谱宽为 0.32 nm。2013年, 苟斗斗等<sup>[18]</sup>搭建了波长为 1  $\mu\text{m}$  的环形光纤激光器, 通过结合 SESAM 被动锁模技术和可调谐滤波器, 实现了波长为 1033~1069 nm 的宽带可调谐激光输出, 整个调谐范围内的谱宽均小于 2.7 nm。2017年, Zou等<sup>[19]</sup>提出

了一种基于 SESAM 锁模结构的全光纤锁模激光器, 采用基于薄膜腔技术的可调谐带通滤波器调节波长, 通过调节滤波器和偏振控制器, 获得了波长为 1023~1060 nm 的皮秒脉冲激光。2022年, 林加强等<sup>[20]</sup>利用基于双段保偏光纤的 Sagnac 滤波器, 搭建了全光纤掺镱锁模激光器, 当激光器处于单波长锁模状态时, 通过调节腔内的偏振控制器, 可以获得波长连续可调谐的脉冲输出, 其调谐范围为 1031~1040 nm。虽然以上方式可以实现输出波长可调谐的脉冲激光, 但整体系统结构相对复杂、成本较高, 且很难实现宽光谱脉冲激光直接输出。

此外, 目前超短脉冲锁模光纤激光振荡器的直接输出功率几乎为数十毫瓦甚至更低, 要想获得百毫瓦量级的激光脉冲输出, 须在其后搭建一级超短脉冲激光放大器。当前主流技术方案需要两台半导体激光器分别泵浦振荡器和放大器。为了降低激光器的复杂性和成本, 2017年, 李平雪等<sup>[21]</sup>利用泵浦分束方式实现了皮秒光纤振荡器和放大器的同步泵浦(仅需一台半导体激光器)。一些商用脉冲光纤激光器厂家也采用这一方法。然而, 上述激光器无法实现特定波长的激光输出, 很难精准匹配 Yb:YAG、Yb:CaF<sub>2</sub>、Yb:Lu<sub>2</sub>O<sub>3</sub> 等超短脉冲固体激光器的发射波长。

本文在泵浦分束结构的基础上引入了波长可调谐机制, 即利用啁啾脉冲增益饱和放大特性实现可调谐激光输出, 通过调节注入到放大器的啁啾脉冲能量, 控制放大器的增益饱和状态, 最终获得了 1030.0~

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1034.5 nm 波长可调谐超短脉冲激光,相应的平均功率为 50~156 mW,最大泵光转换效率为 42.8%,谱宽大于 13.1 nm,可支持时域宽度约为 100 fs 的超短脉冲激光输出。该激光器产生的可调谐超短脉冲激光,可精确匹配 Yb:YAG、Yb:CaF<sub>2</sub>、Yb:Lu<sub>2</sub>O<sub>3</sub> 等晶体的发射波长,因此该激光系统能较好满足 Yb:YAG、Yb:CaF<sub>2</sub>、Yb:Lu<sub>2</sub>O<sub>3</sub> 等超短脉冲固体激光器的需求,对后续宽带脉冲可调谐激光器的设计具有一定的指导意义。

## 2 实验方案

基于泵浦分束结构的波长可调谐 1 μm 超短脉冲光纤激光器的实验装置如图 1 所示,整个激光器采用全光纤结构,主要包括超短脉冲激光振荡器和超短脉冲激光放大器两部分。首先利用两台独立的激光二极管(LD)分别泵浦超短脉冲激光振荡器和超短脉冲激光放大器,从而确定振荡器以及放大器所需的泵浦功率。在此基础上,为了简化激光器结构,利用非保偏分束器(coupler)将 976 nm 单模 LD 的激光分成两束(分束比为 20:80),分别充当超短脉冲激光振荡器和超短脉冲激光放大器的泵浦源,此时,20% 端口输出的泵浦功率为 72.6 mW,80% 端口输出的泵浦功率为 291.9 mW。该结构既实现了超短脉冲激光振荡器的锁模输出,又同步提供了超短脉冲激光放大器所需的泵浦功率。单模

LD 之后的泵浦保护器(pump protector)用于防止回返光损坏 LD。

超短脉冲激光振荡器是全保偏线形腔结构,其采用 6 μm/125 μm 掺镱保偏光纤(PM-YSF)作为增益介质,该增益光纤长度为 0.7 m,在 976 nm 处的吸收系数为 250 dB/m。SESAM 作为高反镜,其反射效率取决于可饱和吸收特性,是实现锁模脉冲激光输出的核心器件。值得一提的是,SESAM 与波分复用器(WDM)集成在同一光纤器件中,这种集成结构是在传统的 SESAM 外部增加了二向色镜,所以 976 nm 的泵浦光会被二向色镜反射,而 1 μm 波段的信号光可通过二向色镜进入 SESAM,该集成结构进一步简化了实验装置,如图 1 所示。光纤啁啾布拉格光栅(CFBG)为输出镜,其工作波长为(1030±3) nm,带宽为 25 nm,透过率为 80%,色散量为 -0.1407 ps<sup>2</sup>。除了作为输出镜外,CFBG 还起到色散管理的作用,其宽带特性也为宽带超短脉冲激光的产生提供了可能。众所周知,为了实现宽带锁模脉冲激光输出,振荡器须工作在净零色散附近<sup>[22]</sup>。实验所使用的单模保偏光纤在波长 1030 nm 处的单位长度色散量约为 0.026 ps<sup>2</sup>/m,为了尽可能补偿 CFBG 的负色散,本实验将振荡器的腔长设为 2.86 m,其中无源光纤长度为 2.16 m。通过计算,腔内的光纤提供的总色散量约为 0.149 ps<sup>2</sup>,根据 CFBG 所提供的色散补偿量,可估算出激光振荡器的总色散量约为 0.008 ps<sup>2</sup>。

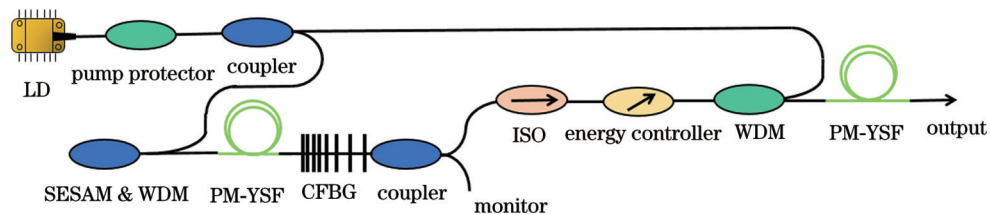


图 1 基于泵浦分束的波长可调谐 1 μm 超短脉冲光纤激光器装置图

Fig. 1 Device diagram of wavelength-tunable 1 μm ultrashort pulse fiber laser based on pump beam splitting

振荡器产生的超短脉冲激光在进入超短脉冲激光放大器之前,采用分束比为 20:80 的保偏分束器进行分束,其 20% 端口输出的激光用于锁模脉冲的实时监测,80% 端口输出的激光被注入到超短脉冲激光放大器中。

超短脉冲激光放大器为全保偏光纤结构,包括光纤隔离器(ISO)、能量控制器(energy controller)、WDM 和 PM-YSF。其中,ISO 用于防止放大过程中的回返光对超短脉冲振荡器产生影响。能量控制器可对注入到超短脉冲激光放大器的啁啾脉冲能量进行调节。泵浦激光通过 980 μm/1030 μm 的 WDM 耦合进 PM-YSF,该增益光纤参数与超短脉冲激光振荡器相同,长度为 1.4 m,放大后的脉冲激光最后跳线输出。

## 3 分析与讨论

利用超短脉冲光纤激光器可实现振荡器和放大器的同步泵浦。当 LD 功率增加到 364.5 mW 时(相应的振荡器泵浦功率为 72.6 mW,放大器泵浦功率为 291.9 mW),该激光器可实现稳定的超短脉冲激光输出。超短脉冲激光振荡器会依次经历量子噪声、调 Q、锁模这三个阶段,在锁模条件下,超短脉冲激光振荡器的输出功率为 12.1 mW。

图 2(a)为示波器测量的脉冲序列,可见其重复频率( $f_r$ )为 36.23 MHz,与腔长匹配,说明此时锁模激光器还未产生谐波,处于单脉冲锁模状态。图 2(b)为相应的输出光谱,可见激光中心波长为 1034.2 nm,3 dB 光谱宽度为 17.4 nm,相应的傅里叶变换极限(FTL)脉冲宽度为 100 fs。在本实验装置中,LD 发出的抽运光

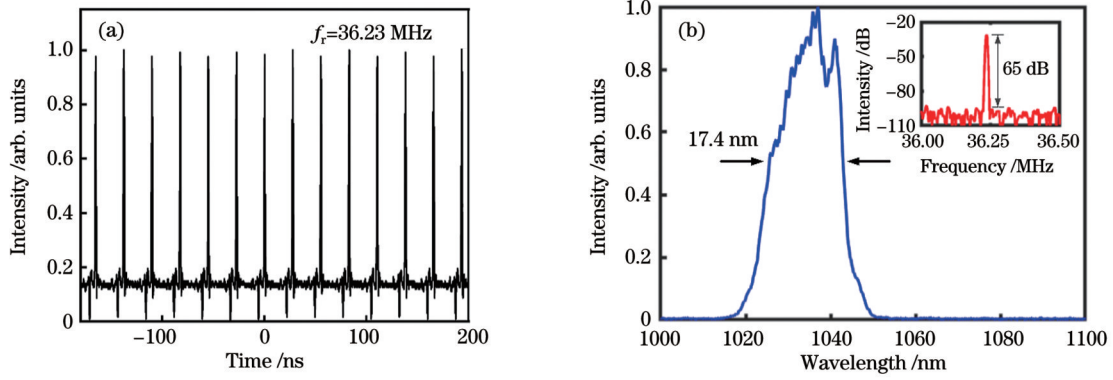


图2 实验结果。(a)超短脉冲激光振荡器脉冲序列;(b)超短脉冲激光振荡器输出光谱(插图:为振荡器频谱)

Fig. 2 Experimental results. (a) Pulse train of ultrashort pulse laser oscillator; (b) output spectrum of ultrashort pulse laser oscillator with frequency spectrum of oscillator shown in inset

泵浦 PM-YSF, PM-YSF 作为增益介质表现出正常色散特性,光脉冲经 PM-YSF 传输后得到放大和展宽,展宽后的光脉冲进入 CFBG,此时 CFBG 仅对反射回腔内的脉冲提供负色散,因此,CFBG 透射端输出的锁模脉冲带有一定的正啁啾,脉冲宽度应该为 ps 量级。这在后续实验放大器中,利用啁啾脉冲增益饱和放大特性<sup>[23-24]</sup>实现光谱的可调谐提供了可能性。此外,也测量了锁模激光的频谱特性,如图 2(b)插图所示,其信噪比高达 65 dB,表明其具有较好的脉冲稳定性。

对于超短脉冲激光放大器,利用能量控制器可以控制放大器增益饱和状态,并实时监测放大器的输出功率、输出光谱的变化。根据前文可知,放大器增益光纤采用的是高掺杂 PM-YSF,所以放大器输出的脉冲激光几乎没有残余泵浦。通过调节能量控制器,放大器最大可产生平均功率为 156 mW 的超短脉冲激光。当输出功率低于 50 mW 时,会出现放大自发辐射(ASE),并在一定程度上影响输出脉冲的信噪比。因此,本文仅对输出功率大于 50 mW 时的波长可调谐特性进行研究。图 3 是输出功率为 50~156 mW 时的光

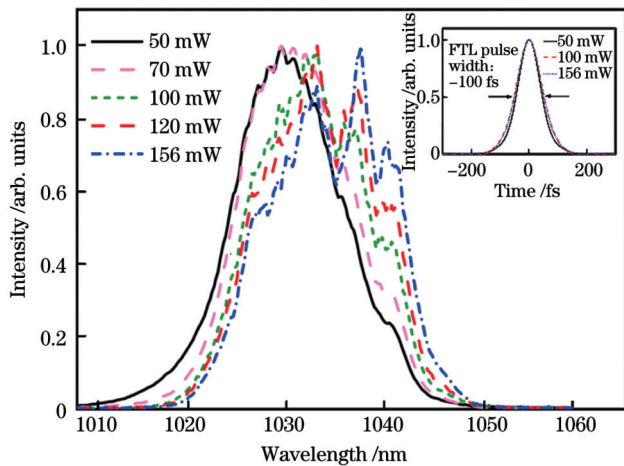


图3 不同输出功率下的光谱(插图:不同功率下的FTL脉宽)  
Fig. 3 Spectra under different output powers with FTL pulse widths under different powers shown in inset

谱,可见随着输出功率的增加,输出的中心波长由 1030.0 nm 逐渐被调谐到 1034.5 nm。研究发现,调谐范围内的部分波长小于超短脉冲激光振荡器直接输出的中心波长,原因是注入到放大器的啁啾脉冲能量较低,此时激光器处于增益未饱和状态,粒子能级跃迁辐射出的中心波长主要由掺镱光纤的增益决定(发射峰位于 1030 nm 处)。随着注入能量的继续增加,脉冲中心波长逐渐向长波方向移动,这是由于注入到放大器的脉冲带有正啁啾,长波部分(红光)处在脉冲的前沿,相应的短波在后沿,且放大器使用的光纤都是正色散光纤,因此当种子注入能量达到放大器增益饱和阈值时,脉冲前沿(长波)比后沿(短波)获得了更高的增益,出现了光谱红移现象<sup>[25]</sup>。而对于无啁啾种子脉冲,由于脉冲所有的频谱成分同时出现的,因此当放大器处于增益饱和状态时,输出激光的中心波长几乎与种子脉冲保持一致。

此外,从图 3 可观测到,在波长调谐范围内,随着输出功率的增加,光谱出现调制现象,这是由光纤中典型的自相位调制(SPM)导致的。当输出功率为 50 mW 时,输出光谱的中心波长恰好位于 1030 nm 附近,可以精准匹配 Yb:YAG、Yb:CaF<sub>2</sub> 固体激光器的发射峰;当输出功率为 100 mW 时,放大光谱的中心波长恰好位于 1032 nm 附近,与 Yb:Lu<sub>2</sub>O<sub>3</sub> 固体激光器的发射峰相吻合<sup>[6]</sup>。根据放大后的光谱形状计算出相应的 FTL 脉冲宽度,当输出功率分别为 50、100、156 mW 时,相应的 FTL 脉冲宽度为 92、104、103 fs,如图 3 插图所示。该方式实现的波长可调谐超短脉冲激光输出为后端固体放大器实现较高的能量提取效率提供了可能。

随后测试了波长调谐范围内脉冲的频谱特性,如图 4(a)所示,可见随着超短脉冲激光放大器输出功率的增加,脉冲激光信噪比逐渐增大,并且波长调谐范围内脉冲信噪比均大于 55 dB,证明放大器具有极高的稳定性。此外,使用自相关仪测得了不同功率下的自相关曲线,如图 4(b)所示。当输出功率分别为 50、

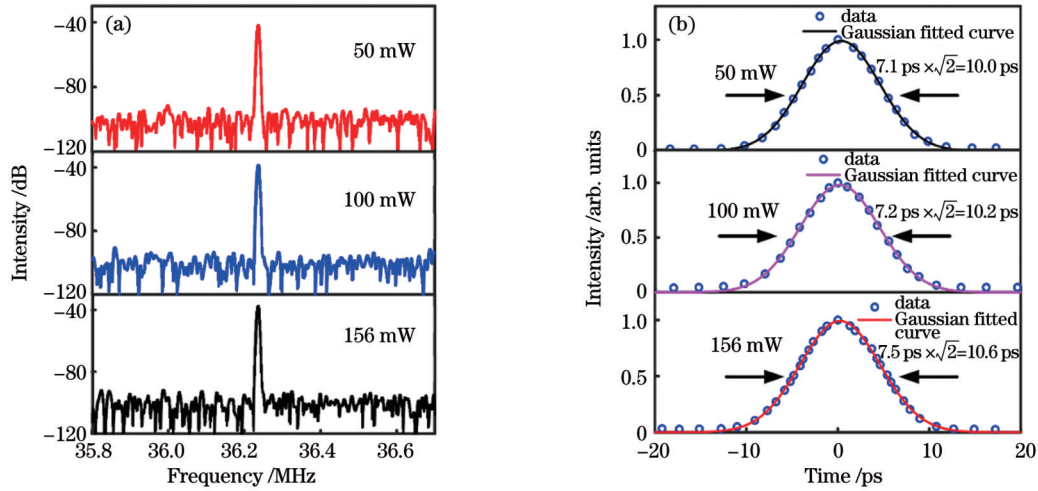


图 4 实验结果。(a)不同输出功率下频谱;(b)不同输出功率下脉宽

Fig. 4 Experimental results. (a) Frequency spectra under different output powers; (b) pulse widths under different output powers

100、156 mW 时,相应的脉冲宽度分别为 7.1、7.2、7.5 ps (假设为高斯脉冲)。脉冲宽度逐渐增大的主要原因有以下两个:一个是随着输出功率的提高,SPM 效应增强,引入了一定的正啁啾;另一个是输出光谱变宽,在色散量(由振荡器输出脉冲的啁啾量以及光纤色散决定)一定的情况下,脉宽进一步变大。

得益于稳定的被动锁模以及全保偏的光纤结构,所获得的  $1\ \mu\text{m}$  超短脉冲光源表现出良好的功率稳定性,如图 5 所示,在输出功率为 156 mW 的条件下,5 h 时间内的相对抖动( $\sigma$ )低至 0.1%。

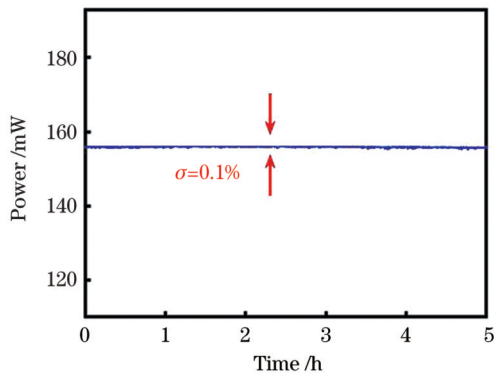


图 5 156 mW 输出功率下超短脉冲光源的稳定性

Fig. 5 Stability of ultrashort pulse light source at 156 mW output power

## 4 结 论

报道了一台波长可调谐  $1\ \mu\text{m}$  超短脉冲光纤激光器。基于泵浦分束结构,利用啁啾脉冲增益饱和放大效应实现了波长可调的超短脉冲激光输出。调节注入到放大器的啁啾脉冲能量,使放大器处于增益饱和或非饱和状态,可获得  $1030.0\sim 1034.5\ \text{nm}$  波长范围内可调的宽带脉冲激光输出,平均功率为  $50\sim 156\ \text{mW}$ ,谱宽大于  $13.1\ \text{nm}$ 。该激光器可支持时域宽度约为 100 fs

的超短脉冲激光输出,其波长连续可调的能力可精确匹配 Yb:YAG、Yb:CaF<sub>2</sub>、Yb:Lu<sub>2</sub>O<sub>3</sub> 等晶体的发射峰,相比于目前单波长光纤激光器,能更好满足 Yb:YAG、Yb:CaF<sub>2</sub>、Yb:Lu<sub>2</sub>O<sub>3</sub> 等大能量超短脉冲固体激光器的需求。

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## Wavelength-Tunable 1- $\mu\text{m}$ Ultrashort-Pulse Fiber Laser Based on Pump Beam Splitting

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### Abstract

**Objective** A wavelength-tunable 1- $\mu\text{m}$  ultrashort-pulse fiber laser can be used not only in laser spectroscopy, optical measurements, biomedicine, and other fields, but also as a seed source in the field of ultrashort-pulse solid-state lasers to accurately match the emission peaks of different gain media. Currently, ultrashort-pulse fiber lasers mainly rely on mode-locking techniques such as nonlinear polarization evolution (NPE), nonlinear amplifying loop mirrors (NALMs), and semiconductor saturable absorption mirrors (SESAMs). Wavelength-tunable 1- $\mu\text{m}$  ultrashort-pulse lasers can be constructed by adding corresponding wavelength-tunable items such as interference items, gratings, and bandpass tunable filters. However, these add complexity and cost to the system. This study utilizes the characteristics of gain saturation amplification related to chirp pulses to realize a wavelength-tunable 1- $\mu\text{m}$  polarization-maintaining (PM) ultrashort-pulse fiber laser based on a pump beam splitting structure. The wavelength-tunable 1- $\mu\text{m}$  ultrashort-pulse fiber laser is relatively simple in structure and has the ability to adjust the central wavelength continuously and accurately, which can match the emission peaks of gain crystals such as Yb: YAG, Yb: CaF<sub>2</sub>, and Yb: Lu<sub>2</sub>O<sub>3</sub>. The proposed laser is expected to provide a more compact, portable, and stable seed light source for ultrashort-pulse solid-state lasers.

**Methods** Based on the pump beam splitting structure, an innovative wavelength-tunable ultrashort-pulse fiber laser is realized using the gain saturation amplification effect of chirp pulses. The laser consists of an ultrashort-pulse fiber oscillator, energy controller, and ultrashort-pulse fiber amplifier, which is driven by a semiconductor laser based on a beam-splitting structure. Controlling the chirp

pulse energy injected into the amplifier enables the amplifier to operate in a gain-saturation or non-saturation state, and the central wavelength of the laser can be accurately adjusted.

**Results and Discussions** When the laser diode (LD) power is increased to 364.5 mW, which corresponds to pump power of 72.6 mW and 291.9 mW for the oscillator and amplifier, respectively, stable ultrashort pulses are obtained at a repetition rate of 36.23 MHz for the ultrashort-pulse fiber laser. When the energy controller is adjusted, the center wavelength of the ultrashort-pulse laser can tune from 1030.0 nm to 1034.5 nm with a spectral width of  $>13.1$  nm. The corresponding output power changes from 50 mW to 156 mW, and the Fourier transform limited (FTL) pulse widths over the entire wavelength tuning range are approximately 100 fs (Fig. 3). When the output power is 50 mW, the central wavelength of the output spectrum is exactly 1030 nm, which accurately matches the emission peaks of Yb:YAG and Yb:CaF<sub>2</sub>. When the output power is 100 mW, the central wavelength is exactly 1032 nm, which is consistent with the emission peak of Yb:Lu<sub>2</sub>O<sub>3</sub>. Notably, the signal-to-noise ratio (SNR) of the ultrashort pulses at each wavelength is greater than 55 dB, indicating that the ultrashort-pulse fiber laser has very high stability. In addition, when the output power is 50, 100, and 156 mW, the corresponding pulse width is 7.1, 7.2, and 7.5 ps, respectively (Fig. 4). Because of the stable passive mode-locking and PM fiber structure, the obtained 1- $\mu$ m ultrashort-pulse laser exhibits good power stability. When the output power is 156 mW, the relative jitter is as low as 0.1% within 5 h (Fig. 5).

**Conclusions** This study utilizes the characteristics of gain saturation amplification related to chirp pulses to report a wavelength-tunable 1- $\mu$ m PM ultrashort-pulse fiber laser based on a pump beam splitting structure. Adjustments to the chirp pulse energy injected into the amplifier enable the amplifier to operate in a gain-saturated or non-saturated state, whereby the laser produces wavelength-tunable pulses from 1030.0 nm to 1034.5 nm at a spectral bandwidth of  $>13.1$  nm. Over the entire tuning range, the SNR of the amplified pulses exceeds 55 dB and the pulse width changes from 7.1 ps to 7.5 ps. In addition, because of the PM architecture, the 1- $\mu$ m ultrashort-pulse laser source exhibits good long-term power stability of as low as 0.1%. The output wavelength of the laser can accurately match the emission peaks of gain crystals such as Yb:YAG, Yb:CaF<sub>2</sub>, and Yb:Lu<sub>2</sub>O<sub>3</sub>. This laser system can serve as a more compact, portable, and stable seed source for ultrashort-pulse solid-state lasers based on various gain crystals such as Yb:YAG, Yb:CaF<sub>2</sub>, and Yb:Lu<sub>2</sub>O<sub>3</sub>.

**Key words** lasers; fiber laser; ultrashort pulse; pump splitting; wavelength tunable