

全保偏掺铒光纤皮秒脉冲及高效率倍频技术研究

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摘要 实验搭建了基于全保偏掺铒光纤激光器的高效率倍频光源。采用可饱和吸收镜进行锁模,并通过两级掺铒光纤放大器实现了高重复频率、窄光谱的线偏振皮秒脉冲输出。在 PPLN 晶体中对该脉冲进行倍频处理,获得了光谱宽度为 0.68 nm、中心波长为 774.8 nm 的皮秒脉冲,平均功率为 613 mW,最大转换效率为 55.7%,倍频脉冲在 3 h 内平均功率的相对抖动低至 0.6%。该光源具有结构紧凑、稳定性高的优势,可应用于超快光谱学、半导体测试等领域。

关键词 激光器; 光纤激光器; 倍频; 全保偏; 皮秒脉冲

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脉冲宽度在皮秒量级的 780 nm 波段激光在太赫兹时域光谱^[1]、材料微加工^[2]和相干反斯托克斯拉曼散射(CARS)成像^[3-4]等多个领域中有着重要的应用。钛宝石激光器可直接产生 780 nm 波段皮秒脉冲^[5],但其光路为空间结构,对环境敏感,需要配置隔振平台及恒温实验室。与钛宝石激光器相比,光纤激光器具有结构紧凑、光束质量好、抗干扰能力强等优点。特别是掺铒光纤激光器的发射波长为 1.5~1.6 μm,通过光学倍频可产生 780 nm 波段^[6-8]脉冲。基于准相位匹配技术^[9-10]的周期性极化晶体可有效规避基频光和倍频光的波矢失配,实现高效率的倍频激光(SHG)输出,因此受到研究人员的青睐。Zhang 等^[11]采用腔内主动锁模,产生了脉宽为 60 ps、重复频率为 6.12 GHz 的 1550 nm 脉冲;并通过 10 mm 长度的 PPLN 晶体,倍频输出了 150 mW 的 775 nm 皮秒脉冲,转换效率为 23.4%。Hu 等^[12]采用马赫-曾德尔调制器对 1560 nm 连续光进行调制,获得了脉宽为 430 ps、重复频率为 50 MHz 的脉冲光;并通过 35 mm 长度的 PPLN 晶体,倍频获得了 3.5 W 的 780 nm 脉冲。由于该系统采用非保偏光纤结构,转换效率仅为 22.4%,且

易受环境干扰,功率稳定性欠佳。Hansknecht 等^[13]通过增益开关调制分布式反馈(DFB)激光器,产生了脉宽为 40 ps、重复频率为 499 MHz 的 1560 nm 脉冲;该系统基于全保偏光纤结构,利用 10 mm 长的 PPLN 晶体,倍频获得了 2 W 的 780 nm 脉冲,转换效率为 40%。Lecourt 等^[14]采用可饱和吸收镜进行锁模,并以 Sagnac 环作为端镜,经光学滤波后获得了脉宽为 15.5 ps、重复频率为 55 MHz 的 1560 nm 皮秒脉冲;通过 MgO-PPLN 晶体输出了 700 mW 的倍频光,转换效率为 35%。本文搭建了基于全保偏掺铒光纤激光器的倍频装置,采用可饱和吸收镜进行锁模,并以光纤布拉格光栅作为滤波反射镜,经两级光纤放大后,获得了高重复频率、窄光谱的近红外皮秒脉冲。该脉冲在 PPLN 晶体中,通过倍频产生了最大功率为 613 mW 的 775 nm 脉冲,转换效率高达 55.7%。

实验装置如图 1 所示,包括掺铒光纤激光器和光学倍频两部分结构。掺铒光纤激光器如图 1(a)所示,SESAM 为可饱和吸收镜,中心波长为 1550 nm,带宽为 20 nm;WDM 为波分复用器;ESF 为长度为 0.9 m 的单模保偏掺铒光纤;光纤

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布拉格光栅 (FBG) 的中心波长和带宽分别为 1550 nm 和 1 nm。LD 为中心波长为 974 nm 的激光二极管, 最大输出功率为 400 mW。实验使用的保偏光纤为波长为 1550 nm 的单模光纤, 纤芯直径为 8.5 μm 。振荡器为线性腔结构, 通过 SESAM 锁模^[15] 实现了种子脉冲输出。种子脉冲经单模掺铒光纤放大器 (EDFA) 提升功率后注入主放大器中, 为后续倍频提供基频光。为了防止后向传输光影响锁模状态, 在振荡器和放大器之间插入光纤隔离器 (ISO)。主放大器的泵浦源为高功率激

光二极管 (HP-LD), 最大输出功率为 9 W。倍频装置如图 1(b) 所示, 基频光经 L1 透镜准直后, 利用半波片 (HWP) 将其调节为竖直偏振状态以满足准相位匹配条件; L2 透镜的焦距为 19 mm, 将基频光聚焦至周期极化铌酸锂 (PPLN) 晶体内; PPLN 的反转周期为 19.34 μm , 尺寸为 10 mm \times 3 mm \times 1 mm。为了避免环境温度的干扰, 晶体放置于控温精度为 0.1 $^{\circ}\text{C}$ 的温控炉 (Oven) 中。倍频光和剩余基频光经透镜 L3 准直后被两面二向色镜 (DM1、DM2) 分束。

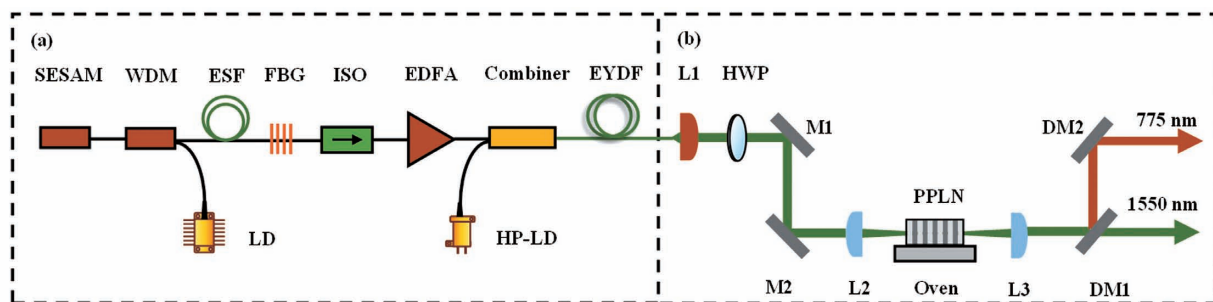


图 1 实验装置。(a) 掺铒光纤激光器; (b) 倍频装置

Fig. 1 Experimental setup. (a) Er-doped fiber laser; (b) SHG device

在实验中, 当激光二极管 (LD) 的功率达到 298 mW 后, 振荡器实现锁模自启动, 产生的激光脉冲的重复频率为 100 MHz、平均功率为 30 mW。输出脉冲经 EDFA 后, 平均功率被提升至百毫瓦量级。主放大器采用长度为 2 m 的双包层铒镱共掺 (EYDF) 光纤作为增益介质, 有效提高了光-光转换效率并抑制了光纤中的非线性效应。当 HP-LD 的功率为 7 W 时, 输出脉冲的平均功率为 1.3 W。如图 2(a)、(b) 所示, 基频光的中心波长为 1549.6 nm,

光谱宽度为 1.01 nm, 相应的脉冲宽度为 11.6 ps (假定为高斯脉冲)。由于脉冲的产生和放大均采用保偏光纤, 基频光的偏振对比度可达 13 dB。为了降低高功率泵浦导致的晶体损伤风险, 后续倍频时基频光的最大入射功率为 1.1 W。

基频光通过 PPLN 晶体实现频率转换, 产生的倍频光的中心波长为 774.8 nm、光谱宽度为 0.68 nm, 相应的脉冲宽度为 11.4 ps, 如图 2(c)、(d) 所示。

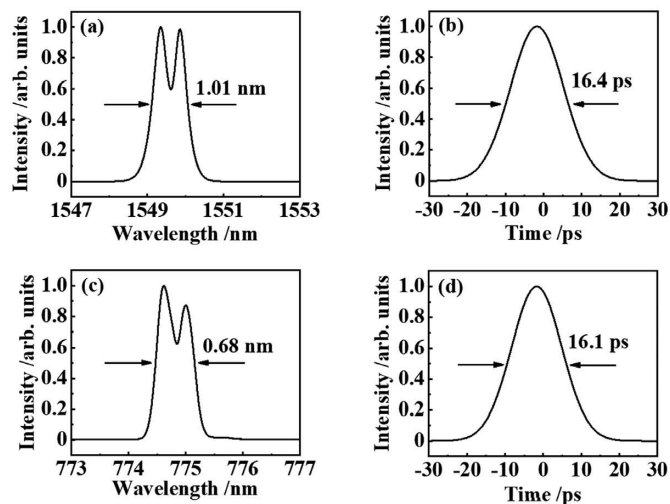


图 2 光谱和脉宽。(a) 基频光光谱; (b) 基频光脉宽; (c) 倍频光光谱; (d) 倍频光脉宽

Fig. 2 Spectrum and pulse duration. (a) Spectrum of fundamental wave; (b) pulse duration of fundamental wave; (c) spectrum of SHG; (d) pulse duration of SHG

在倍频光路中,通过微调光路确定出基频光斑在 PPLN 晶体内的最佳位置,而短焦距的聚焦透镜有效提高了入射脉冲的峰值功率密度。PPLN 晶体的长度为 10 mm,既保证基频光与晶体有足够长的作用距离,又避免了基频光光谱的损失。之后通过温控炉调节晶体温度,获得了高转换效率的倍频光。此外,基频光的高偏振对比度也对转换效率的提高起到了关键性的作用。图 3(a)展示了倍频光的输出功率和转换效率随基频光功率的变化。实验发现,倍频光的功率随基频光功率的增加而单调增加。当基频光功率大于 700 mW 时,转换效率表现出一定的饱和效应。当基频光功率为 1.1 W 时,转换效率达到最高,为 55.7%,此时倍频光的输出功率为 613 mW。由于非线性频率转换对偏

振极为敏感,倍频光的偏振对比度达 27 dB。此外,实验测量了倍频光的功率与晶体温度的关系,如图 3(b)所示,当晶体温度达到 34 °C 时,倍频光的转换效率最高。当倍频光的输出功率为 613 mW 时,通过光斑分析仪在准直透镜 L3 后 1 m 处测量了倍频光的光斑,如图 3(b)中插图所示,倍频光的光斑直径为 0.92 mm,圆度为 97%。得益于稳定的锁模机制和全保偏的光纤结构,倍频脉冲表现出良好的功率稳定性。如图 3(c)所示,倍频脉冲在 3 h 测量时间内平均功率的相对抖动 σ 低至 0.6%,短时间内的峰峰值波动为 2 mW。为了进一步拓展应用,将系统集成于尺寸为 330 mm×250 mm×110 mm 的机箱中,实现了小型化封装,如图 3(d)所示。

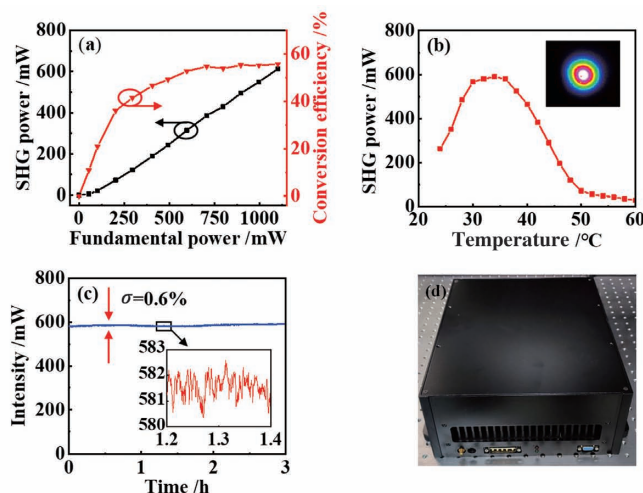


图 3 实验结果。(a)倍频光功率和相应的转换效率随基频光功率的变化;(b)倍频光功率与晶体温度的关系及光斑(插图);(c)倍频光功率稳定性;(d)实物图

Fig. 3 Experimental results. (a) SHG power and corresponding conversion efficiency versus fundamental-wave power; (b) SHG power versus crystal temperature and facula (inset); (c) SHG power stability; (d) photo of product

综上所述,实验验证了基于全保偏掺铒光纤激光器的高效率倍频方案,利用 PPLN 晶体获得了中心波长为 774.8 nm 的皮秒脉冲,转换效率高达 55.7%。所提方案基于全保偏光纤结构,具有紧凑性、便捷性、稳定性等优点,可替代部分钛宝石激光器。

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Picosecond Pulse and High Efficiency Frequency Doubling Based on All-Polarization-Maintaining Er-Doped Fibers

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Abstract

Objective A picosecond pulse at 780 nm has played an important role in practical applications and scientific researches. A Ti: sapphire laser is a famous light source at this wavelength range. However, due to its bulk design and complex architecture, the Ti: sapphire laser is sensitive to its environment. Compared with Ti: sapphire lasers, fiber lasers have the advantages of compact structure, high beam quality, and high stability. An alternative way to generate a picosecond pulse at 780 nm is to utilize frequency doubling of the pulse output from an Er-doped fiber laser. In this study, we experimentally demonstrated a frequency doubling efficiency as high as 55.7% based on an all-polarization-maintaining Er-doped fiber laser. Moreover, this scheme favors the advantages such as compact

structure and good stability, and can be further applied in many fields such as ultrafast spectroscopy and semiconductor testing.

Methods In this study, a passively mode-locked fiber oscillator and a cascaded fiber amplifier, including a single mode fiber pre-amplifier and a double-cladding fiber amplifier, were used to produce a picosecond pulse at 1550 nm. The fiber oscillator was mode-locked by a semiconductor saturable absorber mirror (SESAM). A segment of Er-Yb co-doped double-cladding fiber with a 12 μm fiber core was used in the main amplifier to provide a laser gain and suppress nonlinear effects at a watt-level average power. The frequency conversion was achieved in a periodically poled lithium niobate (PPLN) crystal with 10 mm \times 3 mm \times 1 mm size and a 19.34 μm poling period. The fundamental-wave was focused on the PPLN crystal by a lens with a 19 mm focal length. A temperature-controlled oven was used to achieve the thermal phase matching condition for frequency doubling. A collimating lens and two dichroic mirrors were used for splitting the two beams at 775 nm and 1550 nm.

Results and Discussions The average power from the oscillator was 30 mW at a 100-MHz repetition rate. Subsequently, the pulsed laser was amplified to 1.3 W by the cascaded Er-doped fiber amplifiers. The amplified pulse had a spectral bandwidth of 1.01 nm centered at 1549.6 nm, and a pulse duration of 11.6 ps [Fig. 2(a) and Fig. 2(b)]. The polarization extinction ratio of the pulse was measured to be 13 dB. In order to avoid optical damage on the end facet of the crystal, the maximum incident power of the fundamental-wave was controlled below 1.1-W average power. The optimum temperature of this PPLN crystal was 34 $^{\circ}\text{C}$. In our experiment, the second harmonic average power increases monotonically with the fundamental-wave power. With an incident average power of 1.1 W, the second harmonic laser achieves a power as high as 613 mW, yielding a conversion efficiency of 55.7% [Fig. 3(a)]. The spectral bandwidth and pulse duration of the frequency doubled pulse are 0.68 nm and 11.4 ps, respectively [Fig. 2(c) and Fig. 2(d)]. Benefiting from the all-polarization-maintaining fiber architecture, the frequency doubled pulse exhibits an excellent long-term stability. As shown in Fig. 3(c), the average power instability is as low as 0.6% within 3 h.

Conclusions A picosecond laser architecture for 780-nm spectral range was demonstrated by using an all-polarization-maintaining Er-doped fiber laser and a PPLN frequency doubling crystal. As high as 613-mW average power and 55.7% conversion efficiency were achieved. The proposed laser scheme has the characteristics of compact structure and high stability, which is a good candidate to replace Ti:sapphire lasers in some circumstances.

Key words lasers; fiber lasers; second harmonic generation; all polarization-maintaining; picosecond pulse

OCIS codes 140.3510; 140.3515; 320.7090; 060.2420