

部分相干调制方形平顶脉冲电磁光束在自由空间的传输特性

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摘要 基于广义惠更斯-菲涅耳衍射积分和相干偏振统一理论,研究了有振幅和相位调制的部分相干方形平顶脉冲电磁光束在自由空间的传输特性,推导出了有振幅和相位调制的部分相干方形平顶脉冲电磁光束在自由空间传输的交叉谱密度矩阵解析式,通过数值计算分析了有振幅和相位调制的部分相干方形平顶脉冲电磁光束在自由空间传输的光谱强度分布。研究表明振幅和相位调制半径、调制深度都会对部分相干方形平顶脉冲电磁光束的光谱强度分布产生影响,有振幅和相位调制的部分相干方形平顶脉冲电磁光束在自由空间传输的光谱强度分布与相干长度、脉冲时间相干长度和传输距离有关。

关键词 物理光学;振幅和相位调制;惠更斯-菲涅耳衍射积分;相干偏振统一理论;光谱强度分布

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Propagation Properties of Partially Coherent Modulated Electromagnetic Square Flat-Topped Pulsed Beams in Free Space

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Abstract Based on the generalized Huygens-Fresnel diffraction integral and the unified theory of coherence and polarization, propagation properties of partially coherent electromagnetic square flat-topped pulsed beams with amplitude and phase modulations in free space are analyzed. The analytical expressions for the cross-spectral density matrix of partially coherent electromagnetic square flat-topped pulsed beams with amplitude and phase modulations in free space are derived, and the numerical calculations are also given. It is shown that the spectral intensity distribution of partially coherent electromagnetic square flat-topped pulsed beams is influenced by size of the modulation zone, the depth of amplitude and phase modulations, the coherence length and temporal coherence length of the beams, and transmission distance.

Key words physical optics; amplitude and phase modulation; Huygens-Fresnel diffraction integral; unified theory of coherence and polarization; spectral intensity distribution

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1 引言

在高功率激光装置系统中,除了需要解决提升功率、能量的技术方案外,必须研究光束质量和光束

控制问题,以能满足实际应用要求。实际中传输的激光光束通常都有振幅调制和相位畸变,对调制光束传输的研究引起了许多研究者的兴趣。Wolf^[1]

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于2003年建立了随机电磁光束的相干偏振统一理论,该理论有效地将光束的相干和偏振两个重要特性有效地统一结合,方便了对光束的传输特性的研究。随后研究者采用该理论作了大量的研究,例如随机电磁光束在大气湍流中的传输特性^[2~5]、随机电磁光束在增益或吸收介质中的传输特性^[6],光束的传输特性通过相干偏振统一理论得到了很好的描述。以上的研究都是基于光束稳态场的情况,但是光束的各频率成分之间存在部分相干性^[7,8],因此研究者提出了部分相干脉冲光束的概念,并提供了获得部分相干脉冲光束的方法^[9,10]。由此,研究者们开始了对非稳态的部分相干光束的研究,如林强等^[11,12]研究了部分相干脉冲的传输和时空耦合效应,丁超亮等^[13~17]研究了部分相干脉冲的光谱、相干及偏振特性。本文构建了部分相干方形平顶脉冲光束,研究了有振幅和相位调制的部分相干方形平顶脉冲电磁光束在自由空间的传输特性,分析了有振幅和相位调制的部分相干方形平顶脉冲电磁光束在自由空间传输的光谱强度分布,着重研究了振幅和相位调制半径、调制深度、相干长度、脉冲时间相干长度和传输距离对光谱强度分布的影响。本研究对于光束在实际光路中传输具有基础研究意义和参考价值。

2 理论分析

在时间-空间域内, $z=0$ 平面处的部分相干电磁脉冲光束的 2×2 相干偏振矩阵为

$$\vec{\Gamma}^{(0)}(\boldsymbol{\rho}_1, \boldsymbol{\rho}_2, t_1, t_2) = \begin{bmatrix} \Gamma_{xx}^{(0)}(\boldsymbol{\rho}_1, \boldsymbol{\rho}_2, t_1, t_2) & \Gamma_{xy}^{(0)}(\boldsymbol{\rho}_1, \boldsymbol{\rho}_2, t_1, t_2) \\ \Gamma_{yx}^{(0)}(\boldsymbol{\rho}_1, \boldsymbol{\rho}_2, t_1, t_2) & \Gamma_{yy}^{(0)}(\boldsymbol{\rho}_1, \boldsymbol{\rho}_2, t_1, t_2) \end{bmatrix}, \quad (1)$$

其中相干偏振矩阵元

$$\Gamma_{ij}^{(0)}(\boldsymbol{\rho}_1, \boldsymbol{\rho}_2, t_1, t_2) = \langle E_i^*(\boldsymbol{\rho}_1, t_1) E_j(\boldsymbol{\rho}_2, t_2) \rangle = \sqrt{I_i^{(0)}(\boldsymbol{\rho}_1, t_1)} \sqrt{I_j^{(0)}(\boldsymbol{\rho}_2, t_2)} \eta_{ij}^{(0)}(\boldsymbol{\rho}_1 - \boldsymbol{\rho}_2, t_1 - t_2) \quad (i = x, y; j = x, y), \quad (2)$$

式中 $I^{(0)}(\boldsymbol{\rho}_1, t_1)$ 表示随机电磁脉冲光束的空间和时间振幅分布, $\eta^{(0)}(\boldsymbol{\rho}_1 - \boldsymbol{\rho}_2, t_1 - t_2)$ 表示随机电磁脉冲光束的空间和时间的相干性。 ρ 表示垂直于光轴 z 的横向空间柱坐标, t 表示时间。通常情况下, $I^{(0)}(\boldsymbol{\rho}_1, t_1)$ 分别用高斯空间分布函数和高斯时间分布函数来描述,而 $\eta^{(0)}(\boldsymbol{\rho}_1 - \boldsymbol{\rho}_2, t_1 - t_2)$ 则用谢尔模型来表示

空间域和时间域的相关性。在高功率激光装置中,脉冲光束的空间分布采用的都是平顶模型即超高斯模型来描述,但这给获得传输场中光束解析表达式带来了困难。因此,为了更好地了解光场性质,这里将引用Li^[18,19]所提出的基模叠加的方式来描述随机电磁脉冲光束的空间分布,而时间分布采用高斯函数描述。具体形式如下

$$I_i^{(0)}(\boldsymbol{\rho}, t) = A_i \exp\left\{-\frac{t^2}{T_0^2}\right\} \sum_{m=1}^N \alpha_m \exp\left\{-m\beta_m \frac{\boldsymbol{\rho}^2}{2\sigma^2}\right\}, \quad (3)$$

式中

$$\begin{cases} \alpha_m = (-1)^{m+1} \frac{N!}{m!(N-m)!} \\ \beta_m = \sum_{m=1}^N \frac{\alpha_m}{m} \end{cases}. \quad (4)$$

脉冲光束的空间相关性和时间相关性则采用谢尔模型来描述为

$$\eta_{ij}^{(0)}(\boldsymbol{\rho}_1 - \boldsymbol{\rho}_2, t_1 - t_2) = B_{ij} \exp\left\{-\frac{(\boldsymbol{\rho}_1 - \boldsymbol{\rho}_2)^2}{2\delta_{ij}^2}\right\} \times \exp\left\{-\frac{(t_1 - t_2)^2}{2T_{ci}^2}\right\} \exp\{i\omega_0(t_1 - t_2)\}, \quad (5)$$

式中

$$\begin{cases} B_{ij} \equiv 1 & i = j \\ |B_{ij}| \leq 1 & i \neq j \end{cases}. \quad (6)$$

(3)式和(5)式中,参数 A_i, B_{ij}, σ 和 δ_{ij} 分别表示振幅强度常数、相关性常数、光斑半径以及相关长度,这些参数与载波频率 ω_0 有关。 T_0 表示脉冲时间长度, T_{ci} 表示光束电场 i 方向的脉冲时间相关长度。 N 表示电磁光束空间分布基模叠加阶数,当 $N=1$ 时,表示普通的高斯空间分布,当 $N>2$ 时,则表示平顶空间分布, N 越大,光束空间轮廓越趋于平顶。

为了简单起见,假设 $z=0$ 平面随机电磁脉冲光束的电场在 x 与 y 方向不关联,则有

$$\Gamma_{xy}^{(0)}(\boldsymbol{\rho}_1, \boldsymbol{\rho}_2, t_1, t_2) = \Gamma_{yx}^{(0)}(\boldsymbol{\rho}_1, \boldsymbol{\rho}_2, t_1, t_2) = 0. \quad (7)$$

对(1)式中各矩阵元作如下傅里叶变换

$$W_{ii}^{(0)}(\boldsymbol{\rho}_1, \boldsymbol{\rho}_2, \omega_1, \omega_2) = \frac{1}{(2\pi)^2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \Gamma_{ii}^{(0)}(\boldsymbol{\rho}_1, \boldsymbol{\rho}_2, t_1, t_2) \times \exp[-i(\omega_1 t_1 - \omega_2 t_2)] dt_1 dt_2, \quad (8)$$

则在空间-频率域,随机电磁脉冲光束 $z=0$ 平面的交叉谱密度函数表示为

$$W_{ii}^{(0)}(\boldsymbol{\rho}_1, \boldsymbol{\rho}_2, \omega_1, \omega_2) = \frac{T_0 A_i}{2\pi\Omega_i} \sum_{m_1=1}^N \sum_{m_2=1}^N \alpha_{m_1} \alpha_{m_2} \exp\left(-m_1\beta_1 \frac{\boldsymbol{\rho}_1^2}{4\sigma^2}\right) \exp\left(-m_2\beta_2 \frac{\boldsymbol{\rho}_2^2}{4\sigma^2}\right) \times$$

$$\exp\left[-\frac{(\boldsymbol{\rho}_1 - \boldsymbol{\rho}_2)^2}{2\delta_{ii}^2}\right] \exp\left[-\frac{(\omega_1 - \omega_0)^2 + (\omega_2 - \omega_0)^2}{2\Omega_{0i}^2}\right] \exp\left[-\frac{(\omega_1 - \omega_2)^2}{2\Omega_{ci}^2}\right], \quad (9)$$

$$\Omega_{0i} = \sqrt{\frac{1}{T_0^2} + \frac{2}{T_{ci}^2}}, \quad (10a)$$

$$\Omega_{ci} = \frac{T_{ci}}{T_0} \Omega_{0i}, \quad (10b)$$

式中 Ω_{0i} 表示光束电场 i 方向的光谱宽度, Ω_{ci} 表示光束电场 i 方向的光谱相关长度, 是衡量不同频率成分之间相关性的量。直接采用(9)式进行模拟, 得出光源初始场的空间分布为圆形平顶分布。而高功率激光系统通常采用方形平顶分布。所以将(9)式作如下分解, 可得到方形平顶空间分布的随机电磁脉冲光束的交叉谱密度函数

$$\begin{aligned} W_{ii}^{(0)}(x'_1, y'_1, x'_2, y'_2, \omega_1, \omega_2) &= \frac{T_0 A_i}{2\pi\Omega_{0i}} \exp\left[-\frac{(\omega_1 - \omega_0)^2 + (\omega_2 - \omega_0)^2}{2\Omega_{0i}^2}\right] \exp\left[-\frac{(\omega_1 - \omega_2)^2}{2\Omega_{ci}^2}\right] \times \\ &\sum_{m_1=1}^N \sum_{m_2=1}^N \sum_{n_1=1}^N \sum_{n_2=1}^N \alpha_{m_1} \alpha_{m_2} \alpha_{n_1} \alpha_{n_2} \exp\left[-\left(m_1\beta_{m_1} \frac{x_1'^2}{4\sigma^2} + m_2\beta_{m_1} \frac{x_2'^2}{4\sigma^2} + n_1\beta_{n_1} \frac{y_1'^2}{4\sigma^2} + n_2\beta_{n_2} \frac{y_2'^2}{4\sigma^2}\right)\right] \times \\ &\exp\left\{-\frac{(x'_1 - x'_2)^2 + (y'_1 - y'_2)^2}{2\delta_{ii}^2}\right\}. \end{aligned} \quad (11)$$

实际中传输的激光光束通常都有振幅调制和相位畸变, 当光束经过振幅和相位调制时, 根据菲涅耳衍射积分公式, 则有

$$\begin{aligned} W_{ii}(x_1, y_1, x_2, y_2, z; \omega_1, \omega_2) &= \frac{\omega_1 \omega_2}{4\pi^2 c^2 z^2} \exp\left\{\frac{i(\omega_2 - \omega_1)z}{c}\right\} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} W_{ii}^{(0)}(x'_1, y'_1, x'_2, y'_2, \omega_1, \omega_2) \times \\ &T(x'_1, y'_1, x'_2, y'_2, \omega_1, \omega_2) \exp\left\{\frac{i\omega_2}{2cz} [(x_2 - x_2')^2 + (y_2 - y_2')^2] - \right. \\ &\left. \frac{i\omega_1}{2cz} [(x_1 - x_1')^2 + (y_1 - y_1')^2]\right\} dx'_1 dy'_1 dx'_2 dy'_2, \end{aligned} \quad (12)$$

式中 c 表示真空中的光速。 $T(x'_1, y'_1, x'_2, y'_2, \omega_1, \omega_2)$ 表示振幅和相位调制函数。通常情况下, 振幅和相位调制函数可表示为

$$\begin{aligned} T(x'_1, y'_1, x'_2, y'_2, \omega_1, \omega_2) &= \left\{1 - B\xi \exp\left[\frac{(x'_1 - x_0)^2 + (y'_1 - y_0)^2}{r_0^2}\right]\right\} \exp\left[i\Lambda \frac{\omega_1 \phi}{c} \frac{(x'_1 - x_0)^2 + (y'_1 - y_0)^2}{r_0^2}\right] \times \\ &\left\{1 - B\xi \exp\left[\frac{(x'_2 - x_0)^2 + (y'_2 - y_0)^2}{r_0^2}\right]\right\} \exp\left[-i\Lambda \frac{\omega_2 \phi}{c} \frac{(x'_2 - x_0)^2 + (y'_2 - y_0)^2}{r_0^2}\right], \end{aligned} \quad (13)$$

式中 B 为振幅调制透射率大小; ξ 表示振幅调制方向, Λ 表示相位调制方向, 取 $+1$ 和 -1 分别代表正、反方向调制; ϕ 表示相位调制深度; (x_0, y_0) 表示振幅和相位调制中心位置坐标。将(11)式和(13)式代入(12)式中作积分推导运算, 可得交叉谱密度矩阵元解析式为

$$\begin{aligned} W_{ii}(x_1, y_1, x_2, y_2, z; \omega_1, \omega_2) &= W_{ii}^{(1)}(x_1, y_1, x_2, y_2, z; \omega_1, \omega_2) + W_{ii}^{(2)}(x_1, y_1, x_2, y_2, z; \omega_1, \omega_2) + \\ &W_{ii}^{(3)}(x_1, y_1, x_2, y_2, z; \omega_1, \omega_2) + W_{ii}^{(4)}(x_1, y_1, x_2, y_2, z; \omega_1, \omega_2), \end{aligned} \quad (14)$$

式中

$$\begin{aligned} W_{ii}^{(1)}(x_1, y_1, x_2, y_2, z; \omega_1, \omega_2) &= W_0(x_1, y_1, x_2, y_2, z; \omega_1, \omega_2) \sum_{m_1=1}^N \sum_{m_2=1}^N \sum_{n_1=1}^N \sum_{n_2=1}^N \frac{\alpha_{m_1} \alpha_{m_2} \alpha_{n_1} \alpha_{n_2}}{\sqrt{p_{m_1} p_{m_1, m_2} p_{n_1} p_{n_1, n_2}}} \times \\ &\exp\left[\left(-\frac{1}{4z^2 c^2 p_{m_1}} - \frac{1}{16z^2 c^2 \delta_{ii}^4 (p_{m_1})^2 p_{m_1, m_2}}\right) \omega_1^2 x_1^2 + \frac{\omega_1 \omega_2 x_1 x_2}{4z^2 c^2 \delta_{ii}^2 p_{m_1} p_{m_1, m_2}} - \frac{\omega_2^2 x_2^2}{4z^2 c^2 p_{m_1, m_2}}\right] \times \\ &\exp\left[\left(-\frac{1}{4z^2 c^2 p_{n_1}} - \frac{1}{16z^2 c^2 \delta_{ii}^4 (p_{n_1})^2 p_{n_1, n_2}}\right) \omega_1^2 y_1^2 + \frac{\omega_1 \omega_2 y_1 y_2}{4z^2 c^2 \delta_{ii}^2 p_{n_1} p_{n_1, n_2}} - \frac{\omega_2^2 y_2^2}{4z^2 c^2 p_{n_1, n_2}}\right], \\ W_{ii}^{(2)}(x_1, y_1, x_2, y_2, z; \omega_1, \omega_2) &= \\ &-BW_0(x_1, y_1, x_2, y_2, z; \omega_1, \omega_2) \sum_{m_1=1}^N \sum_{m_2=1}^N \sum_{n_1=1}^N \sum_{n_2=1}^N \frac{\alpha_{m_1} \alpha_{m_2} \alpha_{n_1} \alpha_{n_2}}{\sqrt{p_{m_1} (p_{m_1, m_2} - M) p_{n_1} (p_{n_1, n_2} - M)}} \times \end{aligned}$$

$$\begin{aligned}
 & \exp \left\{ \left(\frac{1}{16z^2 c^2 \delta_{ii}^4 (p_{m_1})^2 (M - p_{m_1, m_2})} - \frac{1}{4z^2 c^2 p_{m_1}} \right) \omega_1^2 x_1^2 - \frac{\omega_1 \omega_2 x_1 x_2}{4z^2 c^2 \delta_{ii}^2 p_{m_1} (M - p_{m_1, m_2})} + \frac{\omega_2^2 x_2^2}{4z^2 c^2 (M - p_{m_1, m_2})} + \right. \\
 & \left. \left[\frac{x_1 M \omega_1 i}{2z c \delta_{ii}^2 p_{m_1} (M - p_{m_1, m_2})} - \frac{x_2 M \omega_2 i}{z c (M - p_{m_1, m_2})} \right] x_0 + \left(M - \frac{M^2}{M - p_{m_1, m_2}} \right) x_0^2 \right\} \frac{\omega_2^2 y_2^2}{4z^2 c^2 (M - p_{n_1, n_2})} + \\
 & \exp \left\{ \left(\frac{1}{16z^2 c^2 \delta_{ii}^4 (p_{n_1})^2 (M - p_{n_1, n_2})} - \frac{1}{4z^2 c^2 p_{n_1}} \right) \omega_1^2 y_1^2 - \frac{\omega_1 \omega_2 y_1 y_2}{4z^2 c^2 \delta_{ii}^2 p_{n_1} (M - p_{n_1, n_2})} + \right. \\
 & \left. \left[\frac{y_1 M \omega_1 i}{2z c \delta_{ii}^2 p_{n_1} (M - p_{n_1, n_2})} - \frac{y_2 M \omega_2 i}{z c (M - p_{n_1, n_2})} \right] y_0 + \left(M - \frac{M^2}{M - p_{n_1, n_2}} \right) y_0^2 \right\}, \\
 & W_{ii}^{(3)}(x_1, y_1, x_2, y_2, z; \omega_1, \omega_2) = \\
 & - B W_0(x_1, y_1, x_2, y_2, z; \omega_1, \omega_2) \sum_{m_1=1}^N \sum_{m_2=1}^N \sum_{n_1=1}^N \sum_{n_2=1}^N \frac{\alpha_{m_1} \alpha_{m_2} \alpha_{n_1} \alpha_{n_2}}{\sqrt{(p_{m_1} - M^*)(p_{n_1} - M^*) q_{m_1, m_2} q_{n_1, n_2}}} \times \\
 & \exp \left\{ \left(\frac{1}{4z^2 c^2 (M^* - p_{m_1})} - \frac{1}{16z^2 c^2 \delta_{ii}^4 q_{m_1, m_2} (M^* - p_{m_1})^2} \right) \omega_1^2 x_1^2 - \frac{\omega_1 \omega_2 x_1 x_2}{4z^2 c^2 \delta_{ii}^2 q_{m_1, m_2} (M^* - p_{m_1})} - \frac{\omega_2^2 x_2^2}{4z^2 c^2 q_{m_1, m_2}} + \right. \\
 & \left. \left\{ \frac{M^* \omega_1 i}{z c (M^* - p_{m_1})} - \frac{M^* \omega_1 i}{4z c \delta_{ii}^4 q_{m_1, m_2} (M^* - p_{m_1})^2} \right\} x_1 - \frac{M^* \omega_2 x_2 i}{2z c \delta_{ii}^2 q_{m_1, m_2} (M^* - p_{m_1})} \right\} x_0 + \\
 & \left(M^* - \frac{M^{*2}}{M^* - p_{m_1}} + \frac{M^{*2}}{4\delta_{ii}^4 q_{m_1, m_2} (M^* - p_{m_1})^2} \right) x_0^2 \times \\
 & \exp \left\{ \left(\frac{1}{4z^2 c^2 (M^* - p_{n_1})} - \frac{1}{16z^2 c^2 \delta_{ii}^4 q_{n_1, n_2} (M^* - p_{n_1})^2} \right) \omega_1^2 y_1^2 - \right. \\
 & \left. \frac{\omega_1 \omega_2 y_1 y_2}{4z^2 c^2 \delta_{ii}^2 q_{n_1, n_2} (M^* - p_{n_1})} - \frac{\omega_2^2 y_2^2}{4z^2 c^2 q_{n_1, n_2}} + \left\{ \frac{M^* \omega_1 i}{z c (M^* - p_{n_1})} - \frac{M^* \omega_1 i}{4z c \delta_{ii}^4 q_{n_1, n_2} (M^* - p_{n_1})^2} \right\} y_1 - \right. \\
 & \left. \frac{M^* \omega_2 x_2 i}{2z c \delta_{ii}^2 q_{n_1, n_2} (M^* - p_{n_1})} \right\} y_0 + \left(M^* - \frac{M^{*2}}{M^* - p_{n_1}} + \frac{M^{*2}}{4\delta_{ii}^4 q_{n_1, n_2} (M^* - p_{n_1})^2} \right) y_0^2 \Big\}, \\
 & W_{ii}^{(4)}(x_1, y_1, x_2, y_2, z; \omega_1, \omega_2) = \\
 & B^2 W_0(x_1, y_1, x_2, y_2, z; \omega_1, \omega_2) \sum_{m_1=1}^N \sum_{m_2=1}^N \sum_{n_1=1}^N \sum_{n_2=1}^N \frac{\alpha_{m_1} \alpha_{m_2} \alpha_{n_1} \alpha_{n_2}}{\sqrt{(p_{m_1} - M^*)(p_{n_1} - M^*)(q_{m_1, m_2} - M)(q_{n_1, n_2} - M)}} \times \\
 & \exp \left\{ \left(\frac{1}{4z^2 c^2 (M^* - p_{m_1})} + \frac{1}{16z^2 c^2 \delta_{ii}^4 (M - q_{m_1, m_2}) (M^* - p_{m_1})^2} \right) \omega_1^2 x_1^2 + \frac{\omega_1 \omega_2 x_1 x_2}{4z^2 c^2 \delta_{ii}^2 (M - q_{m_1, m_2}) (M^* - p_{m_1})} + \right. \\
 & \left. \frac{\omega_2^2 x_2^2}{4z^2 c^2 (M - q_{m_1, m_2})} + \left[\frac{M^* \omega_1 i}{z c (M^* - p_{m_1})} + \frac{(M^* - 2MM^* \delta_{ii}^2 + 2Mp_{m_1} \delta_{ii}^2) \omega_1 i}{4z c \delta_{ii}^4 (M - q_{m_1, m_2}) (M^* - p_{m_1})^2} \right] x_1 + \right. \\
 & \left. \frac{x_2 (M^* - 2MM^* \delta_{ii}^2 + 2Mp_{m_1} \delta_{ii}^2) \omega_2 i}{2z c \delta_{ii}^2 (M - q_{m_1, m_2}) (M^* - p_{m_1})} \right] x_0 + \left(M + M^* - \frac{M^{*2}}{M^* - p_{m_1}} - \frac{(M^* - 2MM^* \delta_{ii}^2 + 2Mp_{m_1} \delta_{ii}^2)^2}{4\delta_{ii}^4 (M - q_{m_1, m_2}) (M^* - p_{m_1})^2} \right) x_0^2 \Big\} \times \\
 & \exp \left\{ \left(\frac{1}{4z^2 c^2 (M^* - p_{n_1})} + \frac{1}{16z^2 c^2 \delta_{ii}^4 (M - q_{n_1, n_2}) (M^* - p_{n_1})^2} \right) \omega_1^2 y_1^2 + \frac{\omega_1 \omega_2 y_1 y_2}{4z^2 c^2 \delta_{ii}^2 (M - q_{n_1, n_2}) (M^* - p_{n_1})} + \right. \\
 & \left. \frac{\omega_2^2 y_2^2}{4z^2 c^2 (M - q_{n_1, n_2})} + \left[\frac{M^* \omega_1 i}{z c (M^* - p_{n_1})} + \frac{(M^* - 2MM^* \delta_{ii}^2 + 2Mp_{n_1} \delta_{ii}^2) \omega_1 i}{4z c \delta_{ii}^4 (M - q_{n_1, n_2}) (M^* - p_{n_1})^2} \right] y_1 + \right. \\
 & \left. \frac{y_2 (M^* - 2MM^* \delta_{ii}^2 + 2Mp_{n_1} \delta_{ii}^2) \omega_2 i}{2z c \delta_{ii}^2 (M - q_{n_1, n_2}) (M^* - p_{n_1})} \right] y_0 + \left(M + M^* - \frac{M^{*2}}{M^* - p_{n_1}} - \frac{(M^* - 2MM^* \delta_{ii}^2 + 2Mp_{n_1} \delta_{ii}^2)^2}{4\delta_{ii}^4 (M - q_{n_1, n_2}) (M^* - p_{n_1})^2} \right) y_0^2 \Big\}, \tag{15}
 \end{aligned}$$

$$\begin{aligned}
 W_0(x_1, y_1, x_2, y_2, z; \omega_1, \omega_2) &= A_i \frac{T_0 \omega_1 \omega_2}{8\pi c^2 z^2 \Omega_{0i}} \exp \left[-\frac{(\omega_1 - \omega_0)^2 + (\omega_2 - \omega_0)^2}{2\Omega_{0i}^2} \right] \exp \left[-\frac{(\omega_1 - \omega_2)^2}{2\Omega_{ci}^2} \right] \times \\
 \exp \left[\frac{-i\omega_1}{2zc} (x_1^2 + y_1^2) + \frac{i\omega_2}{2zc} (x_2^2 - y_2^2) \right], \quad M &= \left(\xi - i\Lambda \frac{\omega_2 \phi}{c} \right) \frac{1}{r_0^2}, \quad M^* = \left(\xi + i\Lambda \frac{\omega_1 \phi}{c} \right) \frac{1}{r_0^2},
 \end{aligned}$$

$$\begin{aligned}
p_{m_1} &= \frac{1}{2\delta_{ii}^2} + \frac{m_1\beta_{m_1}}{4\sigma^2} + \frac{\omega_1 i}{2zc}, & p_{n_1} &= \frac{1}{2\delta_{ii}^2} + \frac{n_1\beta_{n_1}}{4\sigma^2} + \frac{\omega_1 i}{2zc}, & p_{m_1, m_2} &= \frac{1}{2\delta_{ii}^2} + \frac{m_2\beta_{m_2}}{4\sigma^2} - \frac{\omega_2 i}{2zc} - \frac{1}{4\delta_{ii}^4 p_{m_1}}, \\
p_{n_1, n_2} &= \frac{1}{2\delta_{ii}^2} + \frac{n_2\beta_{n_2}}{4\sigma^2} - \frac{\omega_2 i}{2zc} - \frac{1}{4\delta_{ii}^4 p_{n_1}}, & q_{m_1, m_2} &= \frac{1}{2\delta_{ii}^2} + \frac{m_2\beta_{m_2}}{4\sigma^2} - \frac{\omega_2 i}{2zc} + \frac{1}{\delta_{ii}^4 (4M^* - p_{m_1})}, \\
q_{n_1, n_2} &= \frac{1}{2\delta_{ii}^2} + \frac{n_2\beta_{n_2}}{4\sigma^2} - \frac{\omega_2 i}{2zc} + \frac{1}{\delta_{ii}^4 (4M^* - p_{n_1})}.
\end{aligned} \tag{16}$$

令 $x_1 = x_2 = x, y_1 = y_2 = y$, 根据相干偏振统一理论, 有振幅和相位调制的部分相干方形平顶脉冲电磁光束在自由空间传输的光谱强度为

$$S(x, y, z; \omega) = W_{xx}(x, y, x, y, z; \omega, \omega) + W_{yy}(x, y, x, y, z; \omega, \omega). \tag{17}$$

将(14)式代入(17)式, 即得到部分相干方形平顶脉冲光束某一频率成分在传输空间的光谱强度。采用傅里叶变换的方法, 将空间频率域的光谱强度变为空间时间域的光强,

$$I(x, y, z; t_1, t_2) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} S(x, y, z; \omega_1, \omega_2) \times \exp[i(\omega_1 t_1 - \omega_2 t_2)] d\omega_1 d\omega_2. \tag{18}$$

3 数值计算结果及分析

通过一系列数值算例来说明有振幅和相位调制的部分相干方形平顶脉冲电磁光束在自由空间的传输特性。在下列的数值计算中, 选取脉冲光束载波频率为 $\omega_0 = 3.106 \text{ rad/fs}$ 。图 1 为振幅调制半径 r_0 不同情况下的 xy 面的三维光强分布, 图中参数选取为 $T_0 = 70 \text{ fs}, T_{ci} = 4 \text{ fs}, x_0 = y_0 = 0 \text{ mm}, \sigma = 5 \text{ mm}, \delta = 1 \text{ mm}, N = 7, \epsilon = 1, \Lambda = 0, \phi = 1, B = 1$, 可以看出振幅调制的部分相干方形平顶脉冲电磁光束中心存在一个缺陷, 并且调制半径 r_0 越大, 缺陷越大。

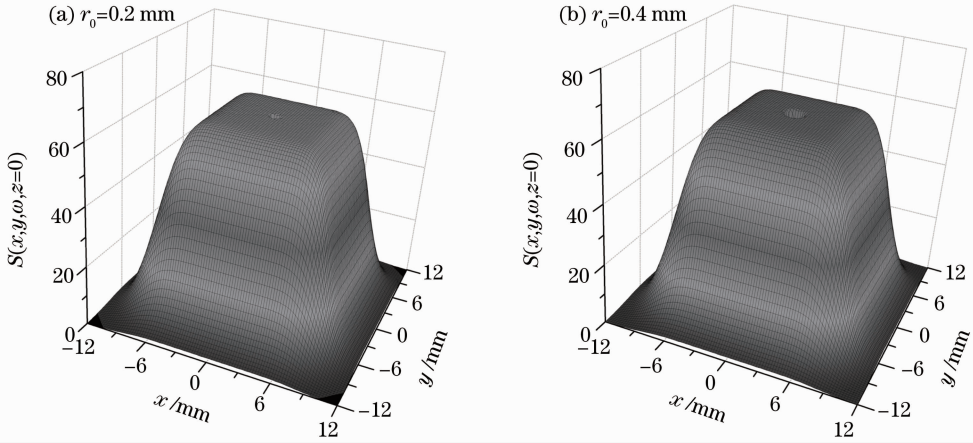


图 1 振幅调制半径 r_0 不同情况下的 xy 面的三维光谱强度分布

Fig. 1 3D irradiance distribution of spectral density in the xy plane for different radii r_0 of amplitude modulation

图 2 为振幅调制的部分相干方形平顶脉冲电磁光束在不同传输距离时的光强分布, 图中参数选取为 $T_0 = 70 \text{ fs}, T_{ci} = 4 \text{ fs}, \sigma = 5 \text{ mm}, x_0 = y_0 = 0 \text{ mm}, \delta = 1 \text{ mm}, N = 7, \epsilon = 1, \Lambda = 0, \phi = 1, r_0 = 0.2 \text{ mm}$, 图 2(a) 中振幅调制深度 $B = 0.5$, 相干长度 $\delta = 1 \text{ mm}$, 图 2(b) 中振幅调制深度 $B = 1$, 相干长度 $\delta = 1 \text{ mm}$, 图 2(c) 中振幅调制深度 $B = 1$, 相干长度 $\delta = 10 \text{ mm}$, 从这 3 幅图对比可以看出, 振幅调制深度越大, 缺陷恢复得越慢, 相干长度越大, 对部分相干方形平顶脉冲电磁光束的波面影响越大, 光强缺陷随着传输距离的增大会得到修复。

图 3 和图 4 为相位调制半径 r_0 不同情况下的 xy 面的三维光强分布, 图中参数选取为 $T_0 = 70 \text{ fs}, T_{ci} = 4 \text{ fs}, \sigma = 5 \text{ mm}, x_0 = y_0 = 0 \text{ mm}, \delta = 1 \text{ mm}, N = 7, \epsilon = 0, \phi = 1, B = 1$, 图 3 中调制方向 $\Lambda = 1$, 图 4 中调制方向 $\Lambda = -1$, 可以看出相位调制与振幅调制相比, 对光强分布的影响更大, 相位调制的部分相干方形平顶脉冲电磁光束产生了许多毛刺, 调制半径 r_0 越大, 对部分相干方形平顶脉冲电磁光束的波面影响越大, 而且调制方向不同, 对部分相干方形平顶脉冲电磁光束的光强影响也不同。

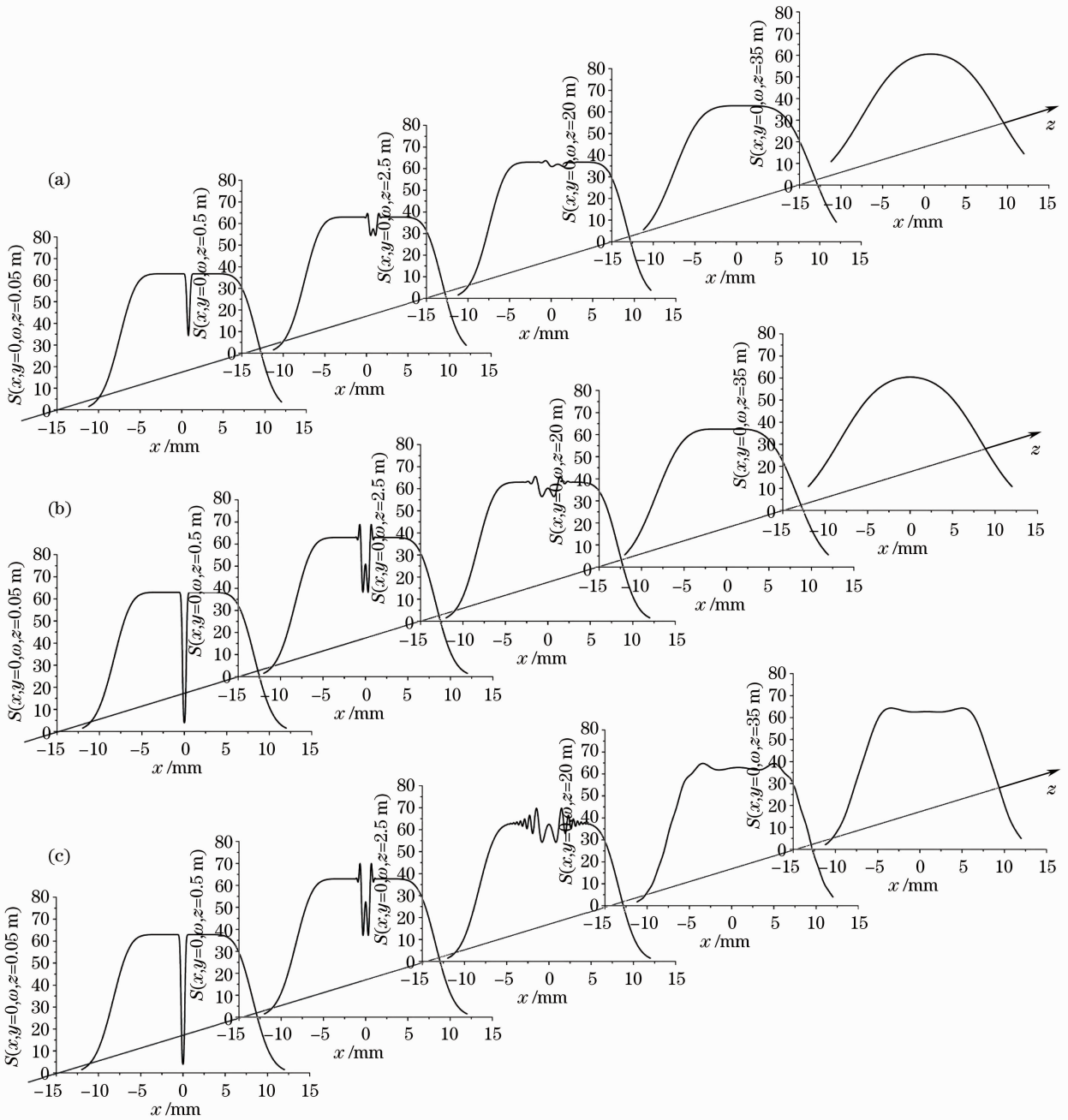


图 2 振幅调制的部分相干方形平顶脉冲电磁光束在不同传输距离时的光谱强度分布

Fig. 2 Distribution of the spectral density of the partially coherent electromagnetic square flat-topped pulsed beam modulated by amplitude in different propagation distances

图 5 为不同相位调制半径 r_0 情况下传输空间的轴上光谱强度,图中参数选取为 $T_0 = 70$ fs, $T_{ci} = 4$ fs, $\sigma = 5$ mm, $x_0 = y_0 = 0$ mm, $\delta = 0.2$ mm, $N = 5$, $\epsilon = 0$, $\phi = \pi$, $B = 1$,图 5(a)中调制方向 $\Lambda = 1$,图 5(b)中调制方向 $\Lambda = -1$,可以看出在存在相位调制的情况下,部分相干方形平顶脉冲电磁光束的传输空间会产生一个光强峰值,并且存在一个相位调制半径 r_0 ,使得传输空间某处存在一个最大值光强峰值,相位调制半径 r_0 越大,光强峰值越远离原场平面,光

强峰值最大值越大,峰值宽度越小。调制方向的不同也会对部分相干方形平顶脉冲电磁光束的传输空间的光强分布产生影响。

图 6 为不同相干长度 δ 和相位调制深度 ϕ 情况下传输空间的轴上光谱强度,图 6(a)中相调制深度 $\phi = \pi$,图 6(b)中相干长度 $\delta = 0.2$ mm,其他参数选取为 $T_0 = 70$ fs, $T_{ci} = 4$ fs, $\sigma = 5$ mm, $x_0 = y_0 = 0$ mm, $N = 5$, $\epsilon = 0$, $B = 1$, $r_0 = 0.6$ mm, $\Lambda = 1$,可以看出相干长度 δ 越大,传输空间产生的光强峰值数

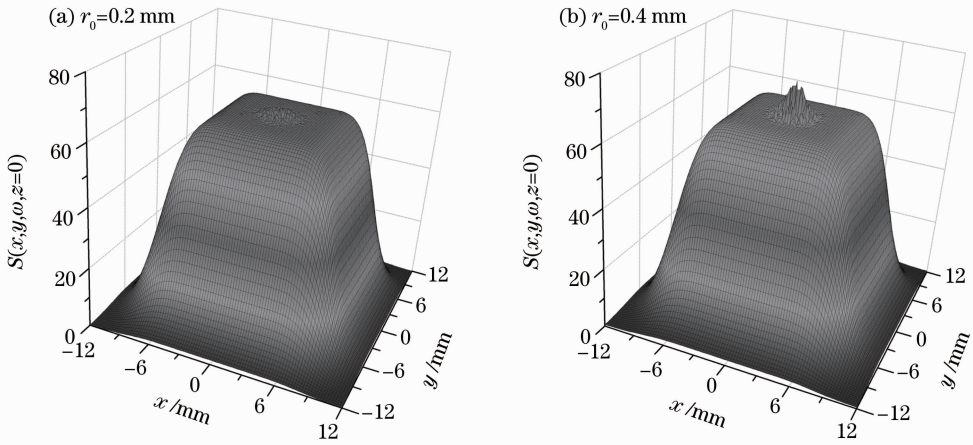
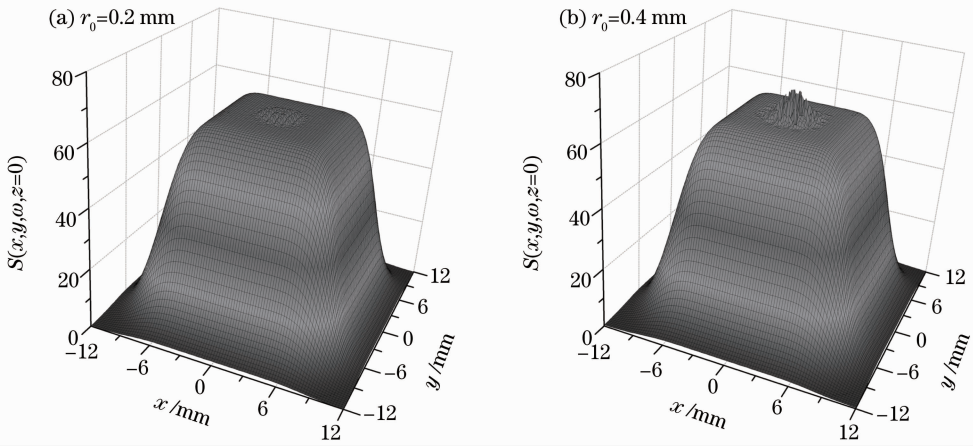
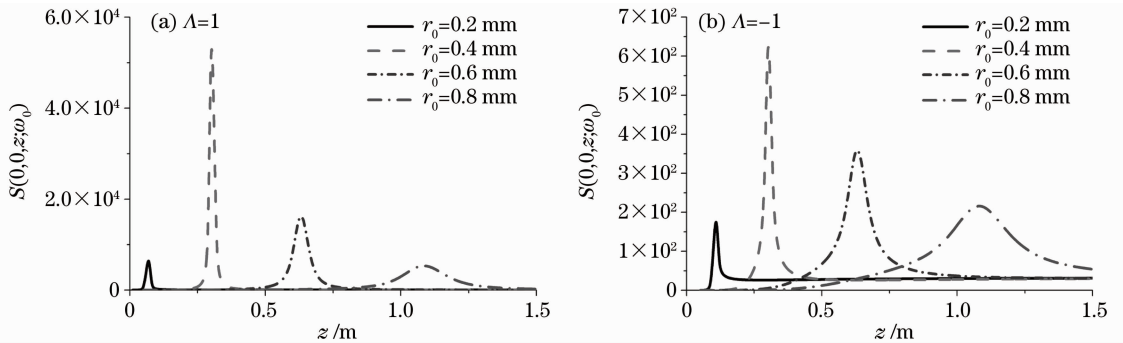
图 3 相位调制半径 r_0 不同情况下的 xy 面的三维光谱强度分布 ($\Lambda=1$)Fig. 3 3D irradiance distribution of spectral density in the xy plane for different radii r_0 of phase modulation ($\Lambda=1$)图 4 相位调制半径 r_0 不同情况下的 xy 面的三维光谱强度分布 ($\Lambda=-1$)Fig. 4 3D irradiance distribution of spectral density in the xy plane for different radii r_0 of phase modulation ($\Lambda=-1$)图 5 不同相位调制半径 r_0 情况下传输空间的轴上光谱强度

Fig. 5 Longitudinal spectral density for different radii of phase modulation in propagation space

值越大；随着相位调制深度 ϕ 的增大，传输空间产生的光强峰值越靠近原场平面，并且光强峰值数值变大，峰值宽度变小。

图 7 为不同光源参数 N 和脉冲时间相关长度 T_{ci} 情况下传输空间的轴上光谱强度，图 7(a) 中脉冲时间相关长度 $T_{ci}=4$ fs，图 7(b) 中光源参数 $N=5$ ，其他参数选取为 $T_0=70$ fs， $\sigma=5$ mm， $x_0=y_0=$

0 mm， $\delta=0.2$ mm， $\epsilon=0$ ， $B=1$ ， $r_0=0.6$ mm， $\phi=\pi$ ， $\Lambda=1$ ，可以看出光源参数 N 越大，传输空间产生的光强峰值数值越大；脉冲时间相关长度 T_{ci} 越大，传输空间产生的光强峰值数值越大。

4 结 论

通过广义惠更斯-菲涅耳衍射积分和相干偏振

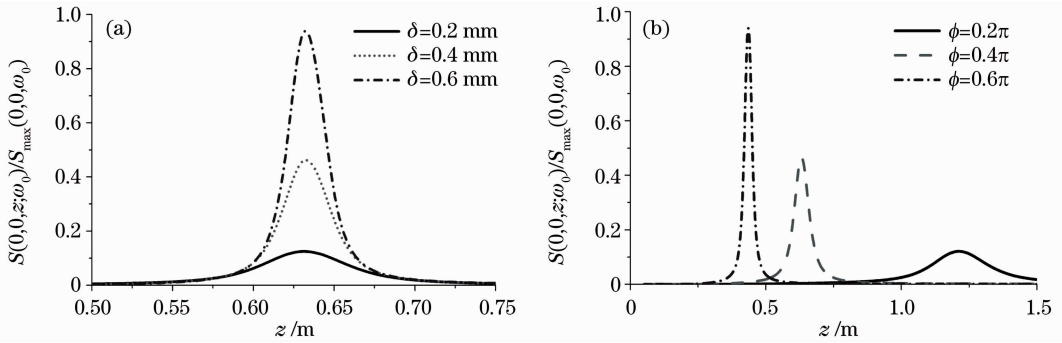


图 6 不同相干长度 δ 和相位调制深度 ϕ 情况下传输空间的轴上光谱强度

Fig. 6 Longitudinal spectral density for different coherence lengths and phase modulation depth in propagation space

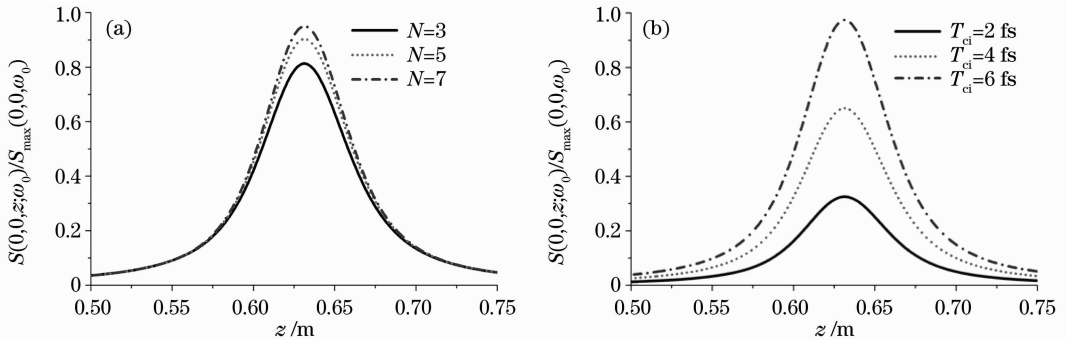


图 7 不同光源参数 N 和脉冲时间相关长度 T_{ci} 情况下传输空间的轴上光谱强度

Fig. 7 Longitudinal spectral density for different values of N and T_{ci} in propagation space

统一理论,研究了有振幅和相位调制的部分相干方形平顶脉冲电磁光束在自由空间传输的光强分布。研究表明振幅和相位调制半径、调制深度都会对部分相干方形平顶脉冲电磁光束的光强分布产生影响,有振幅和相位调制的部分相干方形平顶脉冲电磁光束在自由空间传输的光强分布与相干长度、脉冲时间相干长度和传输距离有关。在局域振幅调制的情况下,振幅调制深度越大,缺陷恢复得越慢,相干长度越大,对部分相干方形平顶脉冲电磁光束的波面影响越大,光强缺陷随着传输距离的增大会得到修复。与振幅调制相比,相位调制对光强分布的影响更大,相位调制的部分相干方形平顶脉冲电磁光束产生了许多毛刺,调制半径越大,对部分相干方形平顶脉冲电磁光束的波面影响越大,而且调制方向不同,对部分相干方形平顶脉冲电磁光束的光强影响也不同。在存在相位调制的情况下,部分相干方形平顶脉冲电磁光束的传输空间会产生一个光强峰值,并且存在一个相位调制半径,使得传输空间某处存在一个最大值光强峰值,相位调制半径越大,光强峰值越远离原场平面,光强峰值最大值越大,峰值宽度越小。调制方向的不同也会对部分相干方形平顶脉冲电磁光束的传输空间的光强分布产生影响。相干长度越大,传输空间产生的光强峰值数值

越大;随着相位调制深度的增大,传输空间产生的光强峰值越靠近原场平面,并且光强峰值数值变大,峰值宽度变小。光源参数 N 和脉冲时间相关长度越大,传输空间产生的光强峰值数值越大。

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