

# Ca<sup>17+</sup> 和 Mn<sup>22+</sup> 的辐射跃迁几率

朱顺人 潘守甫

(吉林大学原子与分子物理所, 长春 130023)

**提要:** 上海光机所徐至展等的研究<sup>[1]</sup>预言, 采用类锂复合机制, 有可能在他们现有的激光驱动装置上将软 X 射线激光推进到“水窗”(4.376~2.332 nm) 波段。本文的计算表明, Ca<sup>17+</sup> 和 Mn<sup>22+</sup> 的 5f-3d 和 5d-3p 跃迁波长处于水窗两端。进而, 详尽地计算了这两个元素类锂离子的精细能级 ( $n \leq 12, l \leq 5$ ) 及它们间的辐射跃迁几率。

**关键词:** 类锂离子, 水窗 X 射线激光, 精细能级, 辐射跃迁几率

## Radiative transition probabilities for Ca<sup>17+</sup> and Mn<sup>22+</sup>

Zhu Qiren, Pan Shoufu

(Institute of Atomic and Molecular Physics, Jilin University, Changchun 130023)

**Abstract:** The investigation by Zhizhan Xu *et al.* of SIOM predicted<sup>[1]</sup> that it is possible that the lasing in the water window (4.376~2.332 nm) will be realized with the Li-like recombination scheme using their high power laser facility.

Our calculations show that the wavelengths of the transitions 5f-3d and 5d-3p in Ca<sup>17+</sup> and Mn<sup>22+</sup> lie at both ends of the water window. The fine levels ( $n \leq 12, l \leq 5$ ) for these two Li-like ions and the radiative transition probabilities between them are calculated.

**Key words:** water window lasers of Li-like ions, fine levels, radiative transition probabilities

以简单的类锂复合方案实现“水窗”(4.376~2.332 nm) 激光的前景<sup>[1]</sup>令人鼓舞。本文首次详尽地计算了其 5f-3d 和 5d-3p 跃迁波长居于水窗两端的 Ca<sup>17+</sup> 和 Mn<sup>22+</sup> 的精细能级 ( $n \leq 12, l \leq 5$ ) 和它们间的辐射跃迁几率。人们可以由这些数据以及它们表现出的确定规律获得从理论上求解动力学方程组所需的全部辐射过程的信息。

## 一、计算方法

本文对于辐射过程的计算, 是运行 MODF 程序包<sup>[2]</sup>, 连同其横向 Breit 修正和量子电动力学修正程序<sup>[3]</sup>, 以及我们自编的计算相对论辐射跃迁几率的后续程序<sup>[4]</sup>完成的。对于每对能级, 均分别在 Coulomb 规范和长度规范下求得两个跃迁几率值, 它们的相对偏差非常灵敏地反映了所得波函数的准确度。对于本文所涉及的大部分跃迁, 这种偏差均在 1% 之内; 对于

**Table 1 Fine levels(eV) of Ca<sup>17+</sup> and Mn<sup>22+</sup>. The upper data are for Ca<sup>17+</sup> and the lower ones for Mn<sup>22+</sup> in every level**

Level	Energy	Level	Energy	Level	Energy	Level	Energy
2s	0 0	6p <sub>3/2</sub>	1034.248 1678.535	8f <sub>5/2</sub>	1088.386 1766.876	10g <sub>9/2</sub>	1113.209 1807.431
2p <sub>1/2</sub>	35.961 46.449	6d <sub>3/2</sub>	1034.689 1679.111	8f <sub>7/2</sub>	1088.399 1766.909	10h <sub>9/2</sub>	1113.209 1807.431
2p <sub>3/2</sub>	41.014 59.886	6d <sub>5/2</sub>	1034.748 1679.268	8g <sub>7/2</sub>	1088.399 1766.910	10h <sub>11/2</sub>	1113.212 1807.438
3s	651.475 1055.928	6f <sub>5/2</sub>	1034.776 1679.306	8g <sub>9/2</sub>	1088.407 1766.929	11s	1120.545 1819.451
3p <sub>1/2</sub>	661.445 1068.830	6f <sub>7/2</sub>	1034.806 1679.385	8h <sub>9/2</sub>	1088.407 1766.929	11p <sub>1/2</sub>	1120.747 1819.712
3p <sub>3/2</sub>	662.938 1072.805	6g <sub>7/2</sub>	1034.806 1679.386	8h <sub>11/2</sub>	1088.412 1766.943	11p <sub>3/2</sub>	1120.777 1819.792
3d <sub>3/2</sub>	666.649 1077.641	6g <sub>9/2</sub>	1034.824 1679.432	9s	1102.287 1789.671	11d <sub>3/2</sub>	1120.839 1819.874
3d <sub>5/2</sub>	667.118 1078.896	6h <sub>9/2</sub>	1034.824 1679.433	9p <sub>1/2</sub>	1102.648 1790.138	11d <sub>5/2</sub>	1120.848 1819.899
4s	875.058 1419.493	6h <sub>11/2</sub>	1034.836 1679.464	9p <sub>3/2</sub>	1102.703 1790.284	11f <sub>5/2</sub>	1120.854 1819.907
4p <sub>1/2</sub>	879.193 1424.808	7s	1066.082 1730.636	9d <sub>3/2</sub>	1102.825 1790.444	11f <sub>7/2</sub>	1120.859 1819.920
4p <sub>3/2</sub>	879.792 1426.482	7p <sub>1/2</sub>	1066.841 1731.618	9d <sub>5/2</sub>	1102.843 1790.491	11g <sub>7/2</sub>	1120.859 1819.920
4d <sub>3/2</sub>	881.335 1428.492	7p <sub>3/2</sub>	1066.958 1731.930	9f <sub>5/2</sub>	1102.852 1790.504	11g <sub>9/2</sub>	1120.862 1819.928
4d <sub>5/2</sub>	881.533 1429.022	7d <sub>3/2</sub>	1067.231 1732.286	9f <sub>7/2</sub>	1102.861 1790.527	11h <sub>9/2</sub>	1120.862 1819.928
4f <sub>5/2</sub>	881.613 1429.129	7d <sub>5/2</sub>	1037.268 1732.385	9g <sub>7/2</sub>	1102.861 1790.528	11h <sub>11/2</sub>	1120.864 1819.933
4f <sub>7/2</sub>	881.712 1429.394	7f <sub>5/2</sub>	1067.287 1732.410	9g <sub>9/2</sub>	1102.866 1790.542	12s	1126.438 1829.065
5s	977.531 1586.337	7f <sub>7/2</sub>	1067.305 1732.460	9h <sub>9/2</sub>	1102.866 1790.542	12p <sub>1/2</sub>	1126.596 1829.268
5p <sub>1/2</sub>	979.608 1589.027	7g <sub>7/2</sub>	1067.305 1732.461	9h <sub>11/2</sub>	1102.870 1790.551	12p <sub>3/2</sub>	1126.619 1829.330
5p <sub>3/2</sub>	979.929 1589.883	7g <sub>9/2</sub>	1067.317 1732.490	10s	1112.787 1803.797	12d <sub>3/2</sub>	1126.664 1829.390
5d <sub>3/2</sub>	980.713 1590.904	7h <sub>9/2</sub>	1067.317 1732.490	10p <sub>1/2</sub>	1113.053 1807.140	12d <sub>5/2</sub>	1126.671 1829.410
5d <sub>5/2</sub>	980.815 1591.175	7h <sub>11/2</sub>	1067.324 1732.510	10p <sub>3/2</sub>	1113.093 1807.246	12f <sub>5/2</sub>	1126.676 1829.416
5f <sub>5/2</sub>	980.360 1591.236	8s	1087.581 1765.689	10d <sub>3/2</sub>	1113.179 1807.360	12f <sub>7/2</sub>	1126.680 1829.426
5f <sub>7/2</sub>	980.911 1591.371	8p <sub>1/2</sub>	1088.092 1766.349	10d <sub>5/2</sub>	1113.192 1807.394	12g <sub>7/2</sub>	1126.680 1829.426
5g <sub>7/2</sub>	980.911 1591.373	8p <sub>3/2</sub>	1088.170 1766.558	10f <sub>5/2</sub>	1113.199 1807.404	12g <sub>9/2</sub>	1126.682 1829.432
5g <sub>9/2</sub>	980.942 1591.454	8d <sub>3/2</sub>	1088.349 1766.792	10f <sub>7/2</sub>	1113.205 1807.421	12h <sub>9/2</sub>	1126.682 1829.432
6s	1032.858 1676.482	8d <sub>5/2</sub>	1088.374 1766.858	10g <sub>7/2</sub>	1113.205 1807.421	12h <sub>11/2</sub>	1126.684 1829.436
6p <sub>1/2</sub>	1034.063 1678.041						

**Table 2** Transition probabilities  $A(s^{-1})$  between fine levels in Ca<sup>17+</sup> and Mn<sup>22+</sup>. The upper date are for Ca<sup>17+</sup> and the lower ones for Mn<sup>22+</sup> in every transition. Here X(Y) means  $X \times 10^Y$ .

Transition	Probability <i>A</i>	Transition	Probability <i>A</i>	Transition	Probability <i>A</i>	Transition	Probability <i>A</i>
2s-3p <sub>1/2</sub>	2.321(12) 6.285(12)	2p <sub>1/2</sub> -9s	9.950(9) 2.527(10)	2p <sub>3/2</sub> -5d <sub>3/2</sub>	1.702(11) 4.493(11)	3s-12p <sub>1/2</sub>	1.241(10) 3.339(10)
4p <sub>1/2</sub>	1.021(12) 2.747(12)	10s	7.222(9) 1.834(10)	6d <sub>3/2</sub>	9.290(10) 2.451(11)	3s-4p <sub>3/2</sub>	2.972(11) 7.993(11)
5p <sub>1/2</sub>	5.257(11) 1.411(12)	11s	5.408(9) 1.375(10)	7d <sub>3/2</sub>	5.653(10) 1.491(11)	5p <sub>3/2</sub>	1.639(11) 4.395(11)
6p <sub>1/2</sub>	3.045(11) 8.160(11)	12s	4.155(9) 1.056(10)	8d <sub>3/2</sub>	3.706(10) 9.772(10)	6p <sub>3/2</sub>	9.664(10) 2.590(11)
7p <sub>1/2</sub>	1.917(11) 5.133(11)	2p <sub>1/2</sub> -3d <sub>3/2</sub>	5.887(12) 1.567(13)	9d <sub>3/2</sub>	2.465(10) 6.761(10)	7p <sub>3/2</sub>	6.130(10) 1.642(11)
8p <sub>1/2</sub>	1.283(11) 3.434(11)	4d <sub>3/2</sub>	1.892(12) 5.048(12)	10d <sub>3/2</sub>	1.850(10) 4.877(10)	8p <sub>3/2</sub>	4.121(10) 1.103(11)
9p <sub>1/2</sub>	9.007(10) 2.410(11)	5d <sub>3/2</sub>	8.669(11) 2.315(12)	11d <sub>3/2</sub>	1.380(10) 3.636(10)	9p <sub>3/2</sub>	2.900(10) 7.760(10)
10p <sub>1/2</sub>	6.563(10) 1.756(11)	6d <sub>3/2</sub>	4.739(11) 1.266(12)	12d <sub>3/2</sub>	1.057(10) 2.785(10)	10p <sub>3/2</sub>	2.116(10) 5.663(10)
11p <sub>1/2</sub>	4.930(10) 1.319(11)	7d <sub>3/2</sub>	2.886(11) 7.711(11)	2p <sub>3/2</sub> -3d <sub>5/2</sub>	7.006(12) 1.855(13)	11p <sub>3/2</sub>	1.591(10) 4.257(10)
12p <sub>1/2</sub>	3.796(10) 1.015(11)	8d <sub>3/2</sub>	1.893(11) 5.057(11)	4d <sub>5/2</sub>	2.242(12) 5.936(12)	12p <sub>3/2</sub>	1.227(10) 3.281(10)
2s-3p <sub>3/2</sub>	2.274(12) 6.086(12)	9d <sub>3/2</sub>	1.310(11) 3.501(11)	5d <sub>5/2</sub>	1.026(12) 2.718(12)	3p <sub>1/2</sub> -4s	8.362(10) 2.133(11)
4p <sub>3/2</sub>	1.007(12) 2.688(12)	10d <sub>3/2</sub>	9.456(10) 2.526(11)	6d <sub>5/2</sub>	5.602(11) 1.483(12)	5s	4.050(10) 1.036(11)
5p <sub>3/2</sub>	5.198(11) 1.387(12)	11d <sub>3/2</sub>	7.052(10) 1.884(11)	7d <sub>5/2</sub>	3.411(11) 9.029(11)	6s	2.255(10) 5.775(10)
6p <sub>3/2</sub>	3.015(11) 8.037(11)	12d <sub>3/2</sub>	5.402(10) 1.443(11)	8d <sub>5/2</sub>	2.236(11) 5.919(11)	7s	1.386(10) 3.550(10)
7p <sub>3/2</sub>	1.899(11) 5.063(11)	2p <sub>3/2</sub> -3s	6.349(11) 1.635(12)	9d <sub>5/2</sub>	1.548(11) 4.097(11)	8s	9.131(9) 2.340(10)
8p <sub>3/2</sub>	1.273(11) 3.391(11)	4s	2.530(11) 6.532(11)	10d <sub>5/2</sub>	1.117(11) 2.956(11)	9s	6.340(9) 1.626(10)
9p <sub>3/2</sub>	8.935(10) 2.381(11)	5s	1.252(11) 3.236(11)	11d <sub>5/2</sub>	8.329(10) 2.204(11)	10s	4.584(9) 1.176(10)
10p <sub>3/2</sub>	6.513(10) 1.736(11)	6s	7.102(10) 1.837(11)	12d <sub>5/2</sub>	6.380(10) 1.688(11)	11s	3.423(9) 8.775(9)
11p <sub>3/2</sub>	4.893(10) 1.304(11)	7s	4.415(10) 1.142(11)	3s-4p <sub>1/2</sub>	3.044(11) 8.302(11)	12s	2.624(9) 6.728(9)
12p <sub>3/2</sub>	3.769(10) 1.004(11)	8s	2.933(10) 7.587(10)	5p <sub>1/2</sub>	1.669(11) 4.520(11)	3p <sub>1/2</sub> -4d <sub>3/2</sub>	6.249(11) 1.660(12)
2p <sub>1/2</sub> -3s	3.077(11) 7.762(11)	9s	2.047(10) 5.296(10)	6p <sub>1/2</sub>	9.813(10) 2.652(11)	5d <sub>3/2</sub>	3.037(11) 8.090(11)
4s	1.229(11) 3.112(11)	10s	1.486(10) 3.844(10)	7p <sub>1/2</sub>	6.216(10) 1.677(11)	6d <sub>3/2</sub>	1.687(11) 4.500(11)
5s	6.085(10) 1.543(11)	11s	1.113(10) 2.879(10)	8p <sub>1/2</sub>	4.175(10) 1.126(11)	7d <sub>3/2</sub>	1.035(11) 2.761(11)
6s	3.452(10) 8.759(10)	12s	8.547(9) 2.212(10)	9p <sub>1/2</sub>	2.936(10) 7.910(10)	8d <sub>3/2</sub>	6.809(10) 1.818(11)
7s	2.146(10) 5.448(10)	2p <sub>3/2</sub> -3d <sub>5/2</sub>	1.167(12) 3.090(12)	10p <sub>1/2</sub>	2.141(10) 5.768(10)	9d <sub>3/2</sub>	4.724(10) 1.262(11)
8s	1.426(10) 3.620(10)	4d <sub>5/2</sub>	3.724(11) 9.840(11)	11p <sub>1/2</sub>	1.610(10) 4.234(10)	10d <sub>3/2</sub>	3.414(10) 9.116(10)

(续表)

Transition	Probability <i>A</i>	Transition	Probability <i>A</i>	Transition	Probability <i>A</i>	Transition	Probability <i>A</i>
$3p_{1/2}-11d_{3/2}$	2.549(10) 6.806(10)	$3p_{1/2}-11d_{5/2}$	3.034(10) 8.063(10)	$3d_{3/2}-11f_{5/2}$	2.580(10) 6.893(10)	$3d_{5/2}-11f_{7/2}$	2.751(10) 7.331(10)
$12d_{3/2}$	1.954(10) 5.217(10)	$12d_{5/2}$	2.325(10) 6.180(10)	$12f_{5/2}$	1.952(10) 5.216(10)	$12f_{7/2}$	2.082(10) 5.547(10)
$3p_{3/2}-4s$	1.722(11) 4.478(11)	$3d_{3/2}-4p_{1/2}$	4.081(10) 1.113(11)	$3d_{5/2}-4p_{3/2}$	3.538(10) 9.439(10)	$4s-5p_{1/2}$	7.151(10) 1.957(11)
$5s$	8.320(10) 2.167(11)	$5p_{1/2}$	1.761(10) 4.797(10)	$5p_{3/2}$	1.529(10) 4.074(10)	$6p_{1/2}$	4.440(10) 1.207(11)
$6s$	4.630(10) 1.206(11)	$6p_{1/2}$	9.229(9) 2.514(10)	$6p_{3/2}$	8.011(9) 2.135(10)	$7p_{1/2}$	2.845(10) 7.715(10)
$7s$	2.844(10) 7.413(10)	$7p_{1/2}$	5.474(9) 1.490(10)	$7p_{3/2}$	4.751(9) 1.266(10)	$8p_{1/2}$	1.919(10) 5.194(10)
$8s$	1.874(10) 4.885(10)	$8p_{1/2}$	3.527(9) 9.604(9)	$8p_{3/2}$	3.002(9) 8.159(9)	$9p_{1/2}$	1.351(10) 3.655(10)
$9s$	1.301(10) 3.392(10)	$9p_{1/2}$	2.412(9) 6.568(9)	$9d_{3/2}$	2.094(9) 5.581(9)	$10p_{1/2}$	9.863(9) 2.667(10)
$10s$	9.406(9) 2.453(10)	$10p_{1/2}$	1.726(9) 4.699(9)	$10p_{3/2}$	1.498(9) 3.992(9)	$11p_{1/2}$	7.416(9) 2.004(10)
$11s$	7.023(9) 1.832(10)	$11p_{1/2}$	1.179(9) 3.481(9)	$11p_{3/2}$	1.110(9) 2.958(9)	$12p_{1/2}$	5.715(9) 1.544(10)
$12s$	5.384(9) 1.404(10)	$12p_{1/2}$	9.747(8) 2.653(9)	$12p_{3/2}$	8.462(8) 2.255(9)	$4s-5p_{3/2}$	6.968(10) 1.879(11)
$3p_{3/2}-4d_{3/2}$	1.254(11) 3.337(11)	$3d_{3/2}-4p_{3/2}$	3.877(9) 1.025(10)	$3d_{5/2}-4f_{5/2}$	9.655(10) 2.572(11)	$6p_{3/2}$	4.352(10) 1.170(11)
$5d_{3/2}$	6.048(10) 1.608(11)	$5p_{3/2}$	1.675(9) 4.427(9)	$5f_{5/2}$	3.176(10) 8.453(10)	$7p_{3/2}$	2.796(10) 7.507(10)
$6d_{3/2}$	3.351(10) 8.904(10)	$6p_{3/2}$	8.779(8) 2.320(9)	$6f_{5/2}$	1.500(10) 3.989(10)	$8p_{3/2}$	1.888(10) 5.066(10)
$7d_{3/2}$	2.053(10) 5.451(10)	$7p_{3/2}$	5.207(8) 1.375(9)	$7f_{5/2}$	8.432(9) 2.242(10)	$9p_{3/2}$	1.331(10) 3.570(10)
$8d_{3/2}$	1.350(10) 3.584(10)	$8p_{3/2}$	3.355(8) 8.863(8)	$8f_{5/2}$	5.265(9) 1.400(10)	$10p_{3/2}$	9.720(9) 2.607(10)
$9d_{3/2}$	9.359(9) 2.485(10)	$9p_{3/2}$	2.295(8) 6.061(8)	$9f_{5/2}$	3.529(9) 9.378(9)	$11p_{3/2}$	7.312(9) 1.961(10)
$10d_{3/2}$	6.761(9) 1.795(10)	$10p_{3/2}$	1.642(8) 4.336(8)	$10f_{5/2}$	2.489(9) 6.615(9)	$12p_{3/2}$	5.637(9) 1.512(10)
$11d_{3/2}$	5.046(9) 1.339(10)	$11p_{3/2}$	1.216(8) 3.213(8)	$11f_{5/2}$	1.826(9) 4.852(9)	$4p_{1/2}-5s$	2.850(10) 7.302(10)
$12d_{3/2}$	3.867(9) 1.027(10)	$12p_{3/2}$	9.271(7) 2.449(8)	$12f_{5/2}$	1.381(9) 3.671(9)	$6s$	1.556(10) 3.999(10)
$3p_{3/2}-4d_{5/2}$	7.500(11) 1.993(12)	$3d_{3/2}-4f_{5/2}$	1.356(12) 3.618(12)	$3d_{5/2}-4f_{7/2}$	1.449(12) 3.862(12)	$7s$	9.383(9) 2.414(10)
$5d_{5/2}$	3.627(11) 9.642(11)	$5f_{5/2}$	4.473(11) 1.195(12)	$5f_{7/2}$	4.777(11) 1.273(12)	$8s$	6.107(9) 1.572(10)
$6d_{5/2}$	2.012(11) 5.348(11)	$6f_{5/2}$	2.115(11) 5.650(11)	$6f_{7/2}$	2.257(11) 6.015(11)	$9s$	4.205(9) 1.083(10)
$7d_{5/2}$	1.233(11) 3.277(11)	$7f_{5/2}$	1.190(11) 3.179(11)	$7f_{7/2}$	1.269(11) 3.384(11)	$10s$	3.022(9) 7.781(9)
$8d_{5/2}$	8.111(10) 2.156(11)	$8f_{5/2}$	7.433(10) 1.986(11)	$8f_{7/2}$	7.930(10) 2.113(11)	$11s$	2.247(9) 5.786(9)
$9d_{5/2}$	5.626(10) 1.496(11)	$9f_{5/2}$	4.983(10) 1.331(11)	$9f_{7/2}$	5.315(10) 1.416(11)	$12s$	1.717(9) 4.421(9)
$10d_{5/2}$	4.065(10) 1.080(11)	$10f_{5/2}$	3.516(10) 9.395(10)	$10f_{7/2}$	3.750(10) 9.993(10)	$4p_{1/2}-5d_{3/2}$	1.301(11) 3.449(11)

(续表)

Transition	Probability A	Transition	Probability A	Transition	Probability A	Transition	Probability A
4p <sub>1/2</sub> -6d <sub>3/2</sub>	7.607(10) 2.025(11)	4p <sub>3/2</sub> -9d <sub>5/2</sub>	2.603(10) 6.929(10)	4d <sub>3/2</sub> -12f <sub>5/2</sub>	1.200(10) 3.208(10)	4f <sub>5/2</sub> -7d <sub>3/2</sub>	1.209(9) 3.264(9)
7d <sub>3/2</sub>	4.727(10) 1.260(11)	10d <sub>5/2</sub>	1.883(10) 5.013(10)	4d <sub>5/2</sub> -5p <sub>3/2</sub>	1.900(10) 5.070(10)	8d <sub>3/2</sub>	7.221(8) 1.949(9)
8d <sub>3/2</sub>	3.218(10) 8.337(10)	11d <sub>5/2</sub>	1.407(10) 3.744(10)	6p <sub>3/2</sub>	9.521(9) 2.539(10)	9d <sub>3/2</sub>	4.695(8) 1.267(9)
9d <sub>3/2</sub>	2.176(10) 5.802(10)	12d <sub>5/2</sub>	1.079(10) 2.872(10)	7p <sub>3/2</sub>	5.459(9) 1.455(10)	10d <sub>3/2</sub>	3.242(8) 8.754(8)
10d <sub>3/2</sub>	1.575(10) 4.199(10)	4d <sub>3/2</sub> -5p <sub>1/2</sub>	2.182(10) 5.937(10)	8p <sub>3/2</sub>	3.441(9) 9.171(9)	11d <sub>3/2</sub>	2.342(8) 6.323(8)
11d <sub>3/2</sub>	1.176(10) 3.138(10)	6p <sub>1/2</sub>	1.092(10) 2.967(10)	9p <sub>3/2</sub>	2.319(9) 6.181(9)	12d <sub>3/2</sub>	1.751(8) 4.728(8)
12d <sub>3/2</sub>	9.024(9) 2.408(10)	7p <sub>1/2</sub>	6.259(9) 1.700(10)	10p <sub>3/2</sub>	1.642(9) 4.377(9)	4f <sub>5/2</sub> -5d <sub>5/2</sub>	2.536(8) 6.765(8)
4p <sub>3/2</sub> -5s	5.862(10) 1.530(11)	8p <sub>1/2</sub>	3.94(59) 1.071(10)	11p <sub>3/2</sub>	1.208(9) 3.219(9)	6d <sub>5/2</sub>	1.079(8) 2.878(8)
6s	3.192(10) 8.342(10)	9p <sub>1/2</sub>	2.659(9) 7.220(9)	12p <sub>3/2</sub>	9.156(8) 2.440(9)	7d <sub>5/2</sub>	5.656(7) 1.509(8)
7s	1.924(10) 5.030(10)	10p <sub>1/2</sub>	1.883(9) 5.112(9)	4d <sub>5/2</sub> -5f <sub>5/2</sub>	1.812(10) 4.832(10)	8d <sub>5/2</sub>	3.376(7) 9.010(7)
8s	1.252(10) 3.274(10)	11p <sub>1/2</sub>	1.385(9) 3.760(9)	6f <sub>5/2</sub>	9.020(9) 2.404(10)	9d <sub>5/2</sub>	2.195(7) 5.858(7)
9s	8.615(9) 2.254(10)	12p <sub>1/2</sub>	1.050(9) 2.849(9)	7f <sub>5/2</sub>	5.142(9) 1.370(10)	10d <sub>5/2</sub>	1.515(7) 4.045(7)
10s	6.191(9) 1.620(10)	4d <sub>3/2</sub> -5p <sub>3/2</sub>	2.085(9) 5.518(9)	8f <sub>5/2</sub>	3.229(9) 8.601(9)	11d <sub>5/2</sub>	1.094(7) 2.921(7)
11s	4.602(9) 1.204(10)	6p <sub>3/2</sub>	1.045(9) 2.765(9)	9f <sub>5/2</sub>	2.171(9) 5.780(9)	12d <sub>5/2</sub>	8.184(6) 2.184(7)
12s	3.516(9) 9.202(9)	7p <sub>3/2</sub>	5.992(8) 1.584(9)	10f <sub>5/2</sub>	1.534(9) 4.084(9)	4f <sub>5/2</sub> -5g <sub>7/2</sub>	4.313(11) 1.150(12)
4p <sub>3/2</sub> -5d <sub>3/2</sub>	2.625(10) 7.000(10)	8p <sub>3/2</sub>	3.777(8) 9.988(8)	11f <sub>5/2</sub>	1.126(9) 2.999(9)	6g <sub>7/2</sub>	1.393(11) 3.716(11)
6d <sub>3/2</sub>	1.525(10) 4.065(10)	9p <sub>3/2</sub>	2.546(8) 6.731(8)	12f <sub>5/2</sub>	8.529(8) 2.270(9)	7g <sub>7/2</sub>	6.553(10) 1.749(11)
7d <sub>3/2</sub>	9.452(9) 2.518(10)	10p <sub>3/2</sub>	1.802(8) 4.765(8)	4d <sub>5/2</sub> -5f <sub>7/2</sub>	2.717(11) 7.242(11)	8g <sub>7/2</sub>	3.696(10) 9.865(10)
8d <sub>3/2</sub>	6.245(9) 1.663(10)	11p <sub>3/2</sub>	1.326(8) 3.505(8)	6f <sub>7/2</sub>	1.354(11) 3.610(11)	9g <sub>7/2</sub>	2.323(10) 6.198(10)
9d <sub>3/2</sub>	4.340(9) 1.156(10)	12p <sub>3/2</sub>	1.005(8) 2.656(8)	7f <sub>7/2</sub>	7.724(10) 2.060(11)	10g <sub>7/2</sub>	1.568(10) 4.185(10)
10d <sub>3/2</sub>	3.139(9) 8.355(9)	4d <sub>3/2</sub> -5f <sub>5/2</sub>	2.538(11) 6.768(11)	8f <sub>7/2</sub>	4.853(10) 1.294(11)	11g <sub>7/2</sub>	1.115(10) 2.975(10)
11d <sub>3/2</sub>	2.344(9) 6.239(9)	6f <sub>5/2</sub>	1.266(11) 3.380(11)	9f <sub>7/2</sub>	3.262(10) 8.700(10)	12g <sub>7/2</sub>	8.242(9) 2.199(10)
12d <sub>3/2</sub>	1.798(9) 4.783(9)	7f <sub>5/2</sub>	7.226(10) 1.930(11)	10f <sub>7/2</sub>	2.306(10) 6.149(10)	4f <sub>7/2</sub> -5d <sub>5/2</sub>	5.112(9) 1.370(10)
4p <sub>3/2</sub> -5d <sub>5/2</sub>	1.568(11) 4.170(11)	8f <sub>5/2</sub>	4.541(10) 1.213(11)	11f <sub>7/2</sub>	1.694(10) 4.516(10)	6d <sub>5/2</sub>	2.175(9) 5.832(9)
6d <sub>5/2</sub>	9.132(10) 2.431(11)	9f <sub>5/2</sub>	3.054(10) 8.157(10)	12f <sub>7/2</sub>	1.282(10) 3.420(10)	7d <sub>5/2</sub>	1.141(9) 3.059(9)
7d <sub>5/2</sub>	5.664(10) 1.508(11)	10f <sub>5/2</sub>	2.159(10) 5.766(10)	4f <sub>5/2</sub> -5d <sub>3/2</sub>	5.419(9) 1.461(10)	8d <sub>5/2</sub>	6.810(8) 1.827(9)
8d <sub>5/2</sub>	3.744(10) 9.967(10)	11f <sub>5/2</sub>	1.585(10) 4.236(10)	6d <sub>3/2</sub>	2.305(9) 6.220(9)	9d <sub>5/2</sub>	4.427(8) 1.188(9)

(续表)

Transition	Probability <i>A</i>	Transition	Probability <i>A</i>	Transition	Probability <i>A</i>	Transition	Probability <i>A</i>
$4f_{7/2}-10d_{5/2}$	3.057(8) 8.204(8)	$5s-7p_{3/2}$	1.529(10) 4.116(10)	$5p_{3/2}-6d_{3/2}$	7.895(9) 2.108(10)	$5d_{3/2}-12p_{3/2}$	9.072(7) 2.400(8)
$11d_{5/2}$	2.208(8) 5.925(8)	$8p_{3/2}$	1.043(10) 2.803(10)	$7d_{3/2}$	5.107(9) 1.363(10)	$5d_{3/2}-6f_{5/2}$	7.092(10) 1.890(11)
$12d_{5/2}$	1.651(8) 4.430(8)	$9p_{3/2}$	7.370(9) 1.981(10)	$8d_{3/2}$	3.406(9) 9.083(9)	$7f_{5/2}$	4.255(10) 1.135(11)
$4f_{7/2}-5g_{7/2}$	1.595(10) 4.249(10)	$10p_{3/2}$	5.388(9) 1.447(10)	$9d_{3/2}$	2.374(9) 6.330(9)	$8f_{5/2}$	2.707(10) 7.227(10)
$6g_{7/2}$	5.141(9) 1.369(10)	$11p_{3/2}$	4.054(9) 1.089(10)	$10d_{5/2}$	1.719(9) 4.583(9)	$9f_{5/2}$	1.829(10) 4.884(10)
$7g_{7/2}$	2.417(9) 6.433(9)	$12p_{3/2}$	3.125(9) 8.388(9)	$11d_{3/2}$	1.285(9) 3.424(9)	$10f_{5/2}$	1.296(10) 3.461(10)
$8g_{7/2}$	1.363(9) 3.626(9)	$5p_{1/2}-6s$	1.164(10) 2.989(10)	$12d_{3/2}$	9.853(8) 2.626(9)	$11f_{5/2}$	9.534(9) 2.546(10)
$9g_{7/2}$	8.560(8) 2.277(9)	$7s$	6.898(9) 1.777(10)	$5p_{3/2}-6d_{5/2}$	4.713(10) 1.255(11)	$12f_{5/2}$	7.225(9) 1.929(10)
$10g_{7/2}$	5.779(8) 1.537(9)	$8s$	4.410(9) 1.137(10)	$7d_{5/2}$	3.054(10) 8.134(10)	$5d_{5/2}-6p_{3/2}$	9.609(9) 2.565(10)
$11g_{7/2}$	4.108(8) 1.093(9)	$9s$	2.998(9) 7.739(9)	$8d_{5/2}$	2.039(10) 5.430(10)	$7p_{3/2}$	5.330(9) 1.421(10)
$12g_{7/2}$	3.036(8) 8.075(8)	$10s$	2.136(9) 5.516(9)	$9d_{5/2}$	1.422(10) 3.788(10)	$8p_{3/2}$	3.264(9) 8.700(9)
$4f_{7/2}-5g_{9/2}$	4.468(11) 1.191(12)	$11s$	1.578(9) 4.076(9)	$10d_{5/2}$	1.030(10) 2.743(10)	$9p_{3/2}$	2.157(9) 5.749(9)
$6g_{9/2}$	1.442(11) 3.844(11)	$12s$	1.201(9) 3.101(9)	$11d_{5/2}$	7.698(9) 2.051(10)	$10p_{3/2}$	1.507(9) 4.015(9)
$7g_{9/2}$	6.784(10) 1.808(11)	$5p_{1/2}-6d_{3/2}$	3.898(10) 1.033(11)	$12d_{5/2}$	5.906(9) 1.573(10)	$11p_{3/2}$	1.097(9) 2.924(9)
$8g_{9/2}$	3.826(10) 1.020(11)	$7d_{3/2}$	2.537(10) 6.743(10)	$5d_{3/2}-6p_{1/2}$	1.101(10) 2.991(10)	$12p_{3/2}$	8.259(8) 2.201(9)
$9g_{9/2}$	2.404(10) 6.048(10)	$8d_{3/2}$	1.697(10) 4.514(10)	$7p_{1/2}$	6.095(9) 1.653(10)	$5d_{5/2}-6f_{5/2}$	5.073(9) 1.353(10)
$10g_{9/2}$	1.623(10) 4.326(10)	$9d_{3/2}$	1.184(10) 3.153(10)	$8p_{1/2}$	3.731(9) 1.011(10)	$7f_{5/2}$	3.037(9) 8.098(9)
$11g_{9/2}$	1.154(10) 3.075(10)	$10d_{3/2}$	8.584(9) 2.287(10)	$9p_{1/2}$	2.465(9) 6.683(9)	$8f_{5/2}$	1.930(9) 5.147(9)
$12g_{9/2}$	8.530(9) 2.273(10)	$11d_{3/2}$	6.419(9) 1.710(10)	$10p_{1/2}$	1.722(9) 4.667(9)	$9f_{5/2}$	1.304(9) 3.475(9)
$5s-6p_{1/2}$	2.321(10) 6.365(10)	$12d_{3/2}$	4.925(9) 1.312(10)	$11p_{1/2}$	1.254(9) 3.399(9)	$10f_{5/2}$	9.233(8) 2.461(9)
$7p_{1/2}$	1.562(10) 4.256(10)	$5p_{3/2}-6s$	2.391(10) 6.254(10)	$12p_{1/2}$	9.440(8) 2.558(9)	$11f_{5/2}$	6.789(8) 1.809(9)
$8p_{1/2}$	1.063(10) 2.883(10)	$7s$	1.414(10) 3.702(10)	$5d_{3/2}-6p_{3/2}$	1.055(9) 2.796(9)	$12f_{5/2}$	5.144(8) 1.371(9)
$9p_{1/2}$	7.500(9) 2.036(10)	$8s$	9.029(9) 2.366(10)	$7p_{3/2}$	5.857(8) 1.550(9)	$5d_{5/2}-6f_{7/2}$	7.600(10) 2.025(11)
$10p_{1/2}$	5.478(9) 1.485(10)	$9s$	6.138(9) 1.609(10)	$8p_{3/2}$	3.586(8) 9.491(8)	$7f_{7/2}$	4.555(10) 1.213(11)
$11p_{1/2}$	4.119(9) 1.116(10)	$10s$	4.372(9) 1.146(10)	$9p_{3/2}$	2.370(8) 6.271(8)	$8f_{7/2}$	2.897(10) 7.725(10)
$12p_{1/2}$	3.173(9) 8.594(9)	$11s$	3.230(9) 8.468(9)	$10p_{3/2}$	1.655(8) 4.380(8)	$9f_{7/2}$	1.956(10) 5.218(10)
$5s-6p_{3/2}$	2.259(10) 6.098(10)	$12s$	2.457(9) 6.441(9)	$11p_{3/2}$	1.205(8) 3.189(8)	$10f_{7/2}$	1.386(10) 3.697(10)

(续表)

Transition	Probability <i>A</i>	Transition	Probability <i>A</i>	Transition	Probability <i>A</i>	Transition	Probability <i>A</i>
5d <sub>5/2</sub> -11f <sub>7/2</sub>	1.019(10) 2.719(10)	5f <sub>7/2</sub> -12g <sub>7/2</sub>	7.173(9) 1.914(10)	5g <sub>7/2</sub> -6f <sub>5/2</sub>	1.206(9) 3.237(9)	5g <sub>9/2</sub> -6f <sub>7/2</sub>	1.168(9) 3.127(9)
12f <sub>7/2</sub>	7.726(9) 2.060(10)	5f <sub>6/2</sub> -6d <sub>5/2</sub>	3.952(9) 1.059(10)	7f <sub>6/2</sub>	4.939(8) 1.325(9)	7f <sub>7/2</sub>	4.782(8) 1.280(9)
5f <sub>6/2</sub> -6d <sub>3/2</sub>	4.186(9) 1.127(10)	7d <sub>5/2</sub>	1.936(9) 5.186(9)	8f <sub>5/2</sub>	2.538(8) 6.815(8)	8f <sub>7/2</sub>	2.457(8) 6.580(8)
7d <sub>3/2</sub>	2.050(9) 5.520(9)	8d <sub>5/2</sub>	1.103(9) 2.955(9)	9f <sub>5/2</sub>	1.500(8) 4.028(8)	9f <sub>7/2</sub>	1.452(8) 3.888(8)
8d <sub>3/2</sub>	1.168(9) 3.146(9)	9d <sub>5/2</sub>	6.957(8) 1.864(9)	10f <sub>5/2</sub>	9.705(7) 2.607(8)	10f <sub>7/2</sub>	9.395(7) 2.517(8)
9d <sub>3/2</sub>	7.367(8) 1.985(9)	10d <sub>5/2</sub>	4.707(8) 1.262(9)	11f <sub>5/2</sub>	6.693(7) 1.798(8)	11f <sub>7/2</sub>	6.477(7) 1.735(8)
10d <sub>3/2</sub>	4.985(8) 1.343(9)	11d <sub>5/2</sub>	3.351(8) 8.982(8)	12f <sub>5/2</sub>	4.835(7) 1.299(8)	12f <sub>7/2</sub>	4.680(7) 1.254(8)
11d <sub>3/2</sub>	3.549(8) 9.565(8)	12d <sub>5/2</sub>	2.479(8) 6.645(8)	5g <sub>7/2</sub> -6f <sub>7/2</sub>	3.322(7) 8.861(7)	5g <sub>9/2</sub> -6h <sub>9/2</sub>	3.837(9) 1.023(10)
12d <sub>3/2</sub>	2.626(8) 7.077(8)	5f <sub>7/2</sub> -6g <sub>7/2</sub>	4.148(9) 1.106(10)	7f <sub>7/2</sub>	1.359(7) 3.627(7)	7h <sub>9/2</sub>	1.186(9) 3.158(9)
5f <sub>6/2</sub> -6d <sub>5/2</sub>	1.963(8) 5.234(8)	7g <sub>7/2</sub>	2.055(9) 5.477(9)	8f <sub>7/2</sub>	6.983(6) 1.863(7)	8h <sub>9/2</sub>	5.448(8) 1.451(9)
7d <sub>5/2</sub>	9.610(7) 2.563(8)	8g <sub>7/2</sub>	1.175(9) 3.131(9)	9f <sub>7/2</sub>	4.124(6) 1.101(7)	9h <sub>9/2</sub>	3.033(8) 8.074(8)
8d <sub>5/2</sub>	5.474(7) 1.460(8)	9g <sub>7/2</sub>	7.422(8) 1.977(9)	10f <sub>7/2</sub>	2.668(6) 7.122(6)	10h <sub>9/2</sub>	1.893(8) 5.037(8)
9d <sub>5/2</sub>	3.452(7) 9.210(7)	10g <sub>7/2</sub>	5.025(8) 1.338(9)	11f <sub>7/2</sub>	1.839(6) 4.910(6)	11h <sub>9/2</sub>	1.274(8) 3.390(8)
10d <sub>5/2</sub>	2.335(7) 6.231(7)	11g <sub>7/2</sub>	3.578(8) 9.528(8)	12f <sub>7/2</sub>	1.329(6) 3.547(6)	12h <sub>9/2</sub>	9.049(7) 2.048(8)
11d <sub>5/2</sub>	1.662(7) 4.435(7)	12g <sub>7/2</sub>	2.647(8) 7.049(8)	5g <sub>7/2</sub> -6h <sub>9/2</sub>	1.690(11) 4.506(11)	5g <sub>9/2</sub> -6h <sub>11/2</sub>	1.728(11) 4.605(11)
12d <sub>5/2</sub>	1.230(7) 3.281(7)	5f <sub>7/2</sub> -6g <sub>9/2</sub>	1.161(11) 3.096(11)	7h <sub>9/2</sub>	5.229(10) 1.395(11)	7h <sub>11/2</sub>	5.343(10) 1.424(11)
5f <sub>6/2</sub> -6g <sub>7/2</sub>	1.120(11) 2.988(11)	7g <sub>9/2</sub>	5.760(10) 1.536(11)	8h <sub>9/2</sub>	2.403(10) 6.411(10)	8h <sub>11/2</sub>	2.456(10) 6.547(10)
7g <sub>7/2</sub>	5.560(10) 1.483(11)	8g <sub>9/2</sub>	3.294(10) 8.784(10)	9h <sub>9/2</sub>	1.339(10) 3.570(10)	9h <sub>11/2</sub>	1.368(10) 3.646(10)
8g <sub>7/2</sub>	3.180(10) 8.487(10)	9g <sub>9/2</sub>	2.081(10) 5.550(10)	10h <sub>9/2</sub>	8.355(9) 2.228(10)	10h <sub>11/2</sub>	8.536(9) 2.275(10)
9g <sub>7/2</sub>	2.010(10) 5.364(10)	10g <sub>9/2</sub>	1.409(10) 3.758(10)	11h <sub>9/2</sub>	5.624(9) 1.500(10)	11h <sub>11/2</sub>	5.746(9) 1.531(10)
10g <sub>7/2</sub>	1.361(10) 3.632(10)	11g <sub>9/2</sub>	1.004(10) 2.676(10)	12h <sub>9/2</sub>	3.996(9) 1.066(10)	12h <sub>11/2</sub>	4.082(9) 1.088(10)
11g <sub>7/2</sub>	9.693(9) 2.587(10)	12g <sub>9/2</sub>	7.427(9) 1.980(10)				

少数由于径向相消效应<sup>[5]</sup>所造成的弱跃迁, 其相对偏差亦在 5% 之内。我们取它们的算术平均值作为该对能级间跃迁几率的理论值。

表 1 一并列出了 Ca<sup>17+</sup> 和 Mn<sup>22+</sup> 的  $n \leq 12$ ,  $l \leq 5$  的全部精细能级值。对于  $n, l$  都很大的能级, 由于它们应有很好的非相对论的类氢行为, 可由表列的数据方便地推出。

表 2 一并列出了 Ca<sup>17+</sup> 和 Mn<sup>22+</sup> 的辐射跃迁几率值。注意到, 对于  $\Delta n = 0$  的跃迁, 由于其跃迁能甚小, 在每一里德伯系之内, 其跃迁几率均明显小于其它成员, 故而未列。另外, 为省篇

幅计,表中未列跃迁波长,读者可由表 1 数据依下式方便求得:

$$\lambda = \frac{12398.52}{\Delta E(\text{eV})} \text{ \AA}, \quad (1)$$

式中  $\Delta E$  为相应两能级的能量差(eV 单位),  $\lambda$  即为该跃迁波长( $\text{\AA}$  单位)。

另外,由表 2 所列数据,依下式可得  $n \leq 6$  所有精细能级的辐射衰变速率  $\Gamma_k$ :

$$\Gamma_k = \sum_i A_{(nl)k \rightarrow (n'l')}, \quad (2)$$

## 二、结果与讨论

正如我们在  $\text{Si}^{11+}$  的计算<sup>[6]</sup>中已经发现的那样,由表 2 仍可看到,对于所有里德伯系,当跃迁上能级的主量数  $n_k$  足够大之后,其跃迁几率仅与  $n_k^3$  成反比。

另外,由表 2 可以看到,对于每组跃迁,上下两层数据几乎均保持着一个共同的比值: 0.375。这是高电离类锂离子的类氢行为的又一生动反映: 对于  $\text{Ca}^{17+}$ , 其光学电子所感受到的有效核电荷  $z_{\text{eff}} \cong 20 - 2 = 18$ ; 对于  $\text{Mn}^{22+}$ ,  $z_{\text{eff}} \cong 25 - 2 = 23$ 。所以,其跃迁几率比应为它们有效核电荷比的 4 次方。

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## 用半导体激光泵浦的 YAG 激光器获得绿光输出

中国科学院上海光机所激光技术开放研究实验室在外腔型“半导体激光泵浦 YAG 激光器”获得运转的基础上,于 1991 年 8 月 22 日实现了腔内倍频,获得了绿光输出。

半外腔的 Nd:YAG 激光腔,腔镜由两个凹面镜组成,5 mm 长的 YAG 棒的一个端面为腔镜之一,涂双色膜,对 1064 nm 全反射,对 808 nm 透过 90%,另一个腔镜也是双色膜,对 1064 nm 全反射,对 532 nm 透过 90%。激光腔的设计使得腔模与泵浦光束匹配,同时有利于增加倍频光的输出。

激光器采用端面纵向泵浦,由半导体温度控制器把泵浦激光波长稳定在 YAG 的吸收峰上,实现光谱匹配。

半导体激光器是本所研制的一维 10 单元锁相阵列的 GaAlAs/GaAs 双异质结激光器,连续波工作时,空间积分功率为 50 mW,脉冲工作时,空间积分峰值功率为 100 mW,重复频率 1 kHz,脉冲宽度 0.1 ms。

腔内倍频用 II 类相位匹配的 KTP 晶体,在连续和脉冲两种工作方式下都获得了 532 nm 的绿光输出。除了能获得稳定的 TEM<sub>00</sub> 模外,也可以得到 TEM<sub>m,n</sub> 模的绿光, $m, n$  可以从 0 到 7 之间变化。

(中国科学院上海光机所激光技术开发实验室 何慧娟 赵庆春 陆雨田

半导体电子学实验室 方祖捷 金志良 屠玉珍 顾德英

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